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THE GENERATION, RADIATION AND PREDICTION OF SUPERSONIC JET NOISE--ETC(U)

OCT 78 B J TESTER, P J MORRIS, H K TANNA

F33615-76-C-2021

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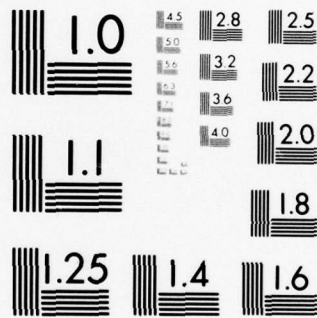
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Volume II

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LEVEL II

**THE GENERATION, RADIATION AND PREDICTION
OF SUPERSONIC JET NOISE
VOLUME II - APPENDIX-COMPUTER PROGRAM LISTING**

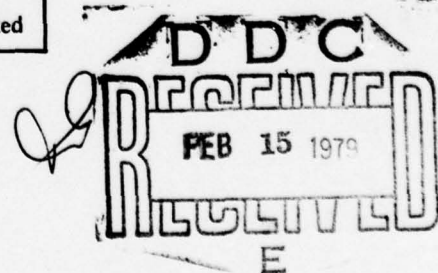
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OCTOBER 1978

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WRIGHT-PATTERSON AIR FORCE BASE, OHIO 45433



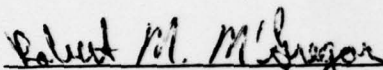
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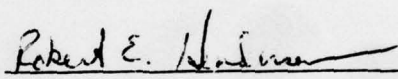
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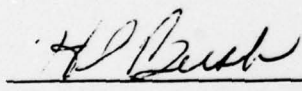
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This technical report has been reviewed and is approved for publication.


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PREFACE

This report was prepared by the Lockheed-Georgia Company, Marietta, Georgia, for the Air Force Aero Propulsion Laboratory, Wright-Patterson Air Force Base under Contract F33615-76-C-2021 (Project 3066, Task 14). The report covers work done in the period 1 December 1975 through 1 September 1978. The work described herein is part of the Air Force Aero Propulsion Laboratory's program to define and control the noise emission of aircraft propulsion systems, and forms a continuation of the studies conducted at Lockheed under two previous contracts (F33615-71-C-1663 and F33615-73-C-2032), which were reported in technical reports AFAPL-TR-72-53 (six volumes) and AFAPL-TR-76-65 (four volumes), respectively.

Mr. Paul Shahady was the Air Force Aero Propulsion Laboratory's Project Engineer for the first two contracts, and he also initiated the third (i.e. the present) contract. Lt. Robert McGregor was the AFAPL's Program Manager for the present contract. Lockheed's Program Manager for all three contracts was Dr. Harry E. Plumblee, Jr.

This Volume II - appendix volume - presents a complete listing of two computer programs. The first program, called UNIJET, is developed to predict the total noise from a subsonic or supersonic jet under static conditions using the results of the present contract together with the knowledge gained in the two previous contracts. The second computer program, called INTEG, is designed to predict absolute values of turbulent mixing noise at 90° to the jet axis, based on laser velocimeter turbulence measurements. A detailed description of these two programs in the form of a User's Guide is given in the main volume of this report.

The authors gratefully acknowledge the efforts of Mr. Robert H. Burrin in preparing this report and Mrs. Barbara C. Reagan in typing the manuscript.

This report was submitted by the authors on 15 September 1978.

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```

*DECK UNIMAIN
PROGRAM UNIMAIN(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE2)
C .....
C *
C *   UNIFIED JET NOISE PREDICTION PROGRAM
C *   -----
C *
C *   PACKAGE A = NOISE FROM LARGE-SCALE TURBULENCE STRUCTURE
C *   PACKAGE B = TURBULENT MIXING NOISE
C *   PACKAGE C = SHOCK ASSOCIATED NOISE
C *
C *   OPNO = OPTION NUMBER
C *
C *   OPNO 1 = A
C *   OPNO 2 = B
C *   OPNO 3 = C
C *   OPNO 4 = A, B, AND A+B
C *   OPNO 5 = B, C, AND B+C
C *   OPNO 6 = A, C, AND A+C
C *   OPNO 7 = A, B, C, AND A+B+C
C *
C *   BOPNO 1 = HIGH-FREQUENCY LILLEY EQUATION SOLUTION
C *   BOPNO 2 = NUMERIC LILLEY EQUATION SOLUTION
C *
C .....
C
C   DIMENSION TM(20),FREQ(30)
C   DIMENSION SPLA(30),SPLB(30),SPLC(30),SPLT(30)
C   DIMENSION SPLLS(30,20)
C   DIMENSION SPLM(33,12)
C   DIMENSION THDOCT(33)
C
C
C   INTEGER TP,OPNO,BOPNO
C   INTEGER OPPE
C   REAL MJ
C
C   INTEGER OC
C   REAL K0,K1,L0,L1,MC
C
C   DATA IC,OC/2HIC,2H /
C
C   DATA NU /1/
C
C   DATA THDOCT /
C   1  50. , 63. , 80. , 100. , 125. , 160. , 200. ,
C   2  250. , 315. , 400. , 500. , 630. , 800. , 1000. ,
C   3  1250. , 1600. , 2000. , 2500. , 3150. , 4000. , 5000. ,
C   4  6300. , 8000. , 10000. , 12500. , 16000. , 20000. , 25000. ,
C   5  31500. , 40000. , 50000. , 63000. , 80000. /
C   WRITE EXPLANATIONS FOR FAILURES
C
C   CALL DATE (DATED)
C   CALL TIME (TIMED)
C   WRITE (6,640) DATED,TIMED
C
C   WRITE (6,650)
C
C   WRITE (6,660)

```

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A 10
A 20
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A 550
A 560
A 570
A 580

```


C		A 590
C	NOVEMBER 15 77. PREDICTION FOR VJ/A0 GT 1 INSIDE CONE OF	A 600
C	SILENCE(IC) ALLOWED	A 610
C		A 620
	WRITE (6,670)	A 630*
C		A 640
C	NOVEMBER 15 77. PREDICTION FOR VJ/A0 GT 1 INSIDE CONE OF	A 650
C	SILENCE(IC) ALLOWED	A 660
C		A 670
	WRITE (6,680)	A 680*
C		A 690
C	READ STATEMENTS	A 700
C		A 710
	READ (5,690) DIA,R	A 720*
	DFT=DIA/12.0	A 730
	ROD=R/DFT	A 740
C		A 750
C	NFREQ = 0 INPUT STARTING 1/3 O.B. NUMBER IN ISTART AND	A 760
C	ENDING 1/3 O.B. NUMBER IN ISTOP	A 770
C	NO FREQUENCIES ARE READ IN .	A 780
C	NFREQ NE 0 NFREQ IS THE NUMBER OF FREQUENCIES TO BE READ IN	A 790
C	ISTART AND ISTOP ARE NOT USED.	A 800
C		A 810
	READ (5,700) NANG,NFREQ,ISTART,ISTOP	A 820*
C		A 830
	IF (NFREQ.EQ.0) GO TO 10	A 840
	READ (5,690) (FREQ(I),I=1,NFREQ)	A 850*
	GO TO 30	A 860
C		A 870
	10 NFREQ=(ISTOP-ISTART)+1	A 880
	J=ISTART-1	A 890
	DO 20 I=1,NFREQ	A 900
	J=J+1	A 910
	20 FREQ(I)=THDOCT(J)	A 920
	30 CONTINUE	A 930
C		A 940
	READ (5,690) (TM(J),J=1,NANG)	A 950*
C		A 960
C		A 970
	READ (5,700) NS	A 980*
	READ (5,690) C,K0,K1,BC	A 990*
C		A1000
C	READ JET OPERATING CONDITIONS AND CALCULATE ALL BASIC PARAMETERS	A1010
C	*	A1020
C	* OPPEP 0 = FLOW PARAMETERS INPUT ARE P0,T0F,VJA0,TJTO	A1030
C	* OPPEP 1 = FLOW PARAMETERS INPUT ARE P0,T0F,PRG,TRF	A1040
C	*	A1050
C		A1060
	READ (5,700) OPNO,OPPER,ICODE,IFLG,BOPNO,ISS,IOPF,ILWR	A1070*
	IF (OPNO.EQ.2.OR.OPNO.EQ.4.OR.OPNO.EQ.5.OR.OPNO.EQ.7) CALL SELECT	A1080S
	1(NU,ISS)	A1090
	40 READ (5,700) TP	A1100*
C		A1110
C		A1120
	IF (TP.EQ.0) GO TO 630	A1130
C		A1140
	IF (OPPER.EQ.1) GO TO 50	A1150
	READ (5,690) P0,T0F,VJA0,TJTO	A1160*
	GO TO 60	A1170

50	READ (5,690) P0,T0F,PRG,TRF	A1180*
60	CONTINUE	A1190
	IF (IOPT,EQ.2) READ (5,690) RSW	A1200*
	IF (IOPT,EQ.3) READ (5,690) RSW,ALTB,BLTB	A1210*
C		A1220
C		A1230
	ICOMP=1	A1240
	IF (ICODE,EQ.0) GO TO 100	A1250
	IF (ICODE,EQ.2) GO TO 90	A1260
	READ (5,700) IVEL,IANG,INCANG	A1270*
	ICOMP=0	A1280
	IF (IVEL,EQ.0.OR.ISTART,EQ.0.OR.OPPER,EQ.0) ICOMP=1	A1290
	IF (ICOMP,EQ.1) GO TO 100	A1300
	REWIND 2	A1310*
	DO 80 IV=1,IVEL	A1320
	DO 70 J=1,12	A1330
	READ (2,710) (SPLM(I,J),I=7,30)	A1340*
70	CONTINUE	A1350
80	CONTINUE	A1360
	IOFF=ISTART-1	A1370
	GO TO 100	A1380
C		A1390
90	IOFF=ISTART-1	A1400
	ICOMP=0	A1410
	IANG=1	A1420
	INCANG=1	A1430
	READ (5,710) ((SPLM(I,J),I=7,30),J=1,NANG)	A1440*
C		A1450
100	CONTINUE	A1460
C		A1470
C	CLEAR MAIN ARRAY OF SPLS FROM LARGE SCALE NOISE PREDICTION	A1480
C		A1490
	DO 110 J=1,20	A1500
	DO 110 I=1,30	A1510
110	SPLLS(I,J)=1.0	A1520
C		A1530
	CALL CALPER (VJAO,TJT0,P0,T0F,TRF,PRG,TRK,TRT0,PRP0,PRGA,DJD0,MJ,A	A1540S
	10,VJ,GAMA,OPPER)	A1550
C		A1560
	IF (MJ,LE.1.0) GO TO 120	A1570
C		A1580
	BETA=SQRT(MJ*MJ-1.0)	A1590
	L0=K0*DIA*BETA	A1600
	L1=K1*DIA*BETA	A1610
	MC=C*VJAO	A1620
	VC=C*VJ	A1630
C		A1640
C	WRITE JET OPERATING CONDITIONS AND ALL BASIC PARAMETERS	A1650
C		A1660
120	WRITE (6,720) TP,OPNO,PRG,P0,TRF,T0F,GAMA	A1670*
C		A1680
	WRITE (6,730) PRP0,TRT0,TJT0,DJD0,VJAO,MJ,VJ	A1690*
C		A1700
	WRITE (6,740) DIA,R,ROD	A1710*
C		A1720
	IF (IOPT,GT.1) WRITE (6,750) RSW	A1730*
	IF (IOPT,EQ.3) WRITE (6,760) ALTB,BLTB	A1740*
	IF (OPNO,EQ.3) GO TO 130	A1750
	IF (OPNO,EQ.5) GO TO 130	A1760

	IF (OPNO,EQ.6) GO TO 130	A1770
	IF (OPNO,EQ.7) GO TO 130	A1780
	GO TO 140	A1790
C	130 WRITE (6,770) C,K0,K1,NS	A1800
C	IF (MJ.LE,1.0) GO TO 140	A1810*
C	WRITE (6,780) BETA,VC,MC,L0,L1	A1820
C	140 CONTINUE	A1830
C	BEGIN ANGLE LOOP	A1840
C	JJ=IANG=INCANG	A1850*
C	DO 620 J=1,NANG	A1860
C	ZM=TM(J)/57.2957795	A1870
C	JJ=JJ+INCANG	A1880
C	COMPUTE PACKAGE A IF OPTION NUMBER IS 1, 4, 6, OR 7	A1890
C	IF (OPNO,EQ.1) GO TO 150	A1900
	IF (OPNO,EQ.4) GO TO 150	A1910
	IF (OPNO,EQ.6) GO TO 150	A1920
	IF (OPNO,EQ.7) GO TO 150	A1930
	GO TO 220	A1940
C	150 CONTINUE	A1950
C	PACKAGE A -- NOISE FROM LARGE-SCALE TURBULENCE STRUCTURE*****	A1960
C	IF (ICOMP,EQ.1) GO TO 160	A1970
	WRITE (6,790) TM(J)	A1980
	GO TO 170	A1990
C	160 WRITE (6,800) TM(J)	A2000
C	BEGIN FREQUENCY LOOP (PACKAGE A)	A2010
C	170 SUMDIF=0.0	A2020
	IH=IOFF	A2030
	NF=0	A2040
C	DO 210 I=1,NFREQ	A2050
C	IF (J,NE,1) GO TO 180	A2060
	F=FREQ(I)	A2070
C	STRNO=F*DFT/VJ	A2080
C	CALL LSMIN (VJA0,TJT0,GAMA,DFT,VJ,F,I,NANG,TM,IFLG,SPLLS)	A2090*
C	180 SPLA(I)=SPLLS(I,J)	A2100
	IF (ICOMP,EQ.1) GO TO 200	A2110*
	IH=IH+1	A2120
	SPLDIF=SPLA(I)-SPLM(IH,JJ)	A2130
	IF (SPLM(IH,JJ).LE,10.0.OR.SPLA(I).LE,10.0) SPLDIF=9999999.9	A2140
	IF (SPLM(IH,JJ).LE,10.0.OR.SPLA(I).LE,10.0) GO TO 190	A2150
	SUMDIF=SUMDIF+SPLDIF**2	A2160
	NF=NF+1	A2170
		A2180
		A2190
		A2200
		A2210
		A2220
		A2230
		A2240
		A2250
		A2260S
		A2270
		A2280
		A2290
		A2300
		A2310
		A2320
		A2330
		A2340
		A2350

C		A2360
C	WRITE PREDICTED VALUES (PACKAGE A)	A2370
C		A2380
	190 WRITE (6,810) FREQ(I),SPLA(I),SPLM(IH,JJ),SPLDIF,SUMDIF	A2390*
	GO TO 210	A2400
	200 WRITE (6,820) FREQ(I),SPLA(I)	A2410*
C		A2420
	210 CONTINUE	A2430
	IF (ICOMP.EQ.1) GO TO 220	A2440
	STDEV=0.0	A2450
	IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A2460
	WRITE (6,830) STDEV	A2470*
C		A2480
C	COMPUTE PACKAGE B IF OPTION NUMBER IS 2, 4, 5, OR 7	A2490
C		A2500
	220 IF (OPNO.EQ.2) GO TO 230	A2510
	IF (OPNO.EQ.4) GO TO 230	A2520
	IF (OPNO.EQ.5) GO TO 230	A2530
	IF (OPNO.EQ.7) GO TO 230	A2540
	GO TO 290	A2550
C		A2560
	230 CONTINUE	A2570
C		A2580
C	PACKAGE B -- TURBULENT MIXING NOISE*****	A2590
C		A2600
	WRITE (6,840) BOPNO	A2610*
	IF (ISS.EQ.1) WRITE (6,850)	A2620*
	IF (NU.EQ.3) WRITE (6,860)	A2630*
	IF (ICOMP.EQ.1) GO TO 240	A2640
	WRITE (6,870) TM(J)	A2650*
	GO TO 250	A2660
	240 WRITE (6,880) TM(J)	A2670*
C		A2680
C	BEGIN FREQUENCY LOOP (PACKAGE B)	A2690
C		A2700
	250 SUMDIF=0.0	A2710
	IH=IOFF	A2720
	NF=0	A2730
C		A2740
	DO 280 I=1,NFREQ	A2750
C		A2760
	CALL MXNOISE (NU,ILWR,OPNO,BOPNO,IOPT,ROD,DFT,TOF,A0,VJ,VJA0,TJTO,	A2770S
	II,FREQ,S,ZM,SM,RSW,ALTB,BLTB,SPLB,SPLPD,SPLPQ,IND)	A2780
C		A2790
	IF (ICOMP.EQ.1) GO TO 270	A2800
	IH=IH+1	A2810
	SPLDIF=SPLB(I)-SPLM(IH,JJ)	A2820
	IF (SPLM(IH,JJ).LE.10.0.OR.SPLB(I).LE.15.0) SPLDIF=9999999.9	A2830
	IF (SPLM(IH,JJ).LE.10.0.OR.SPLB(I).LE.15.0) GO TO 260	A2840
	SUMDIF=SUMDIF+SPLDIF**2	A2850
	NF=NF+1	A2860
	260 WRITE (6,890) FREQ(I),S,SM,SPLPQ,SPLPD,SPLB(I),IND,SPLM(IH,JJ),SPL	A2870*
	DIF,SUMDIF	A2880
	GO TO 280	A2890
	270 WRITE (6,900) FREQ(I),S,SM,SPLPQ,SPLPD,SPLB(I),IND	A2900*
C		A2910
	280 CONTINUE	A2920
C		A2930
	IF (ICOMP.EQ.1) GO TO 290	A2940

	STDEV=0.0	A2950
	IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A2960
	WRITE (6,910) STDEV	A2970*
C	COMPUTE PACKAGE C IF OPTION NUMBER IS 3, 5, 6, OR 7	A2980
C		A2990
	290 IF (OPNO,EQ.3) GO TO 300	A3000
	IF (OPNO,EQ.5) GO TO 300	A3010
	IF (OPNO,EQ.6) GO TO 300	A3020
	IF (OPNO,EQ.7) GO TO 300	A3030
	GO TO 370	A3040
C		A3050
	300 CONTINUE	A3060
C		A3070
C	PACKAGE C -- SHOCK ASSOCIATED NOISE*****	A3080
C		A3090
	IF (MJ.LE.1.0) GO TO 310	A3100
C		A3110
	DF=(1.0-(MC*COS(ZM)))	A3120
	WORK2=((L1*DF)/(VC*12.0))	A3130
C		A3140
	310 WRITE (6,920) TM(J)	A3150*
	IF (ICOMP,EQ.1) GO TO 320	A3160
	WRITE (6,930)	A3170*
	GO TO 330	A3180
	320 WRITE (6,940)	A3190*
C		A3200
C	BEGIN FREQUENCY LOOP (PACKAGE C)	A3210
C		A3220
	330 SUMDIF=0.0	A3230
	IH=IOFF	A3240
	NF=0	A3250
	DO 360 I=1,NFREQ	A3260
C		A3270
	CALL SANOISE (BETA,TJTO,ROD,BC,DFT,A0,NFREQ,FREQ,I,J,TM,L0,MJ,DF,W	A3280S
	1ORK2,NS,SPLC,HXX,HYY,CYY,A3,A2)	A3290
C		A3300
C	WRITE PREDICTED VALUES (PACKAGE C)	A3310
C		A3320
	IF (ICOMP,EQ.1) GO TO 350	A3330
	IH=IH+1	A3340
	SPLDIF=SPLC(I)-SPLM(IH,JJ)	A3350
	IF (SPLM(IH,JJ).LE.10.0.OR.SPLC(I).LE.10.0) SPLDIF=9999999.9	A3360
	IF (SPLM(IH,JJ).LE.10.0.OR.SPLC(I).LE.10.0) GO TO 340	A3370
	SUMDIF=SUMDIF+SPLDIF**2	A3380
	NF=NF+1	A3390
	340 WRITE (6,950) FREQ(I),HXX,HYY,CYY,A3,A2,SPLC(I),SPLM(IH,JJ),SPLDIF	A3400*
	1,SUMDIF	A3410
	GO TO 360	A3420
	350 WRITE (6,960) FREQ(I),HXX,HYY,CYY,A3,A2,SPLC(I)	A3430*
C		A3440
	360 CONTINUE	A3450
C		A3460
	IF (ICOMP,EQ.1) GO TO 370	A3470
	STDEV=0.0	A3480
	IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A3490
	WRITE (6,970) STDEV	A3500*
	370 CONTINUE	A3510
C		A3520
C	THE FOLLOWING FOUR SECTIONS COMPUTE THE TOTAL NOISE*****	A3530

C	**FOR OPTION NUMBERS 4, 5, 6, AND 7, RESPECTIVELY*****	A3540
C		A3550
	IF (OPNO,EQ.1) GO TO 620	A3560
	IF (OPNO,EQ.2) GO TO 620	A3570
	IF (OPNO,EQ.3) GO TO 620	A3580
	IF (OPNO,EQ.4) GO TO 380	A3590
	IF (OPNO,EQ.5) GO TO 440	A3600
	IF (OPNO,EQ.6) GO TO 520	A3610
	IF (OPNO,EQ.7) GO TO 540	A3620
C		A3630
C	COMPUTATION FOR OPTION 4 -- TOTAL NOISE = A+B	A3640
C		A3650
	380 WRITE (6,980) TM(J)	A3660*
	IF (ICOMP,EQ.0) WRITE (6,990)	A3670*
	IF (ICOMP,EQ.1) WRITE (6,1000)	A3680*
C		A3690
	SUMDIF=0.0	A3700
	IH=IOFF	A3710
	NF=0	A3720
C		A3730
	DO 430 I=1,NFREQ	A3740
	SPLT(I)=10.0*ALOG10(10.0**((SPLA(I)/10.0)+10.0**((SPLB(I)/10.0)))	A3750
	IF (ICOMP,EQ.1) GO TO 420	A3760
	IH=IH+1	A3770
	SPLDIF=SPLT(I)-SPLM(IH,JJ)	A3780
	IF (SPLM(IH,JJ).LE.10.0) GO TO 390	A3790
	IF (SPLT(I).LE.15.0) GO TO 390	A3800
	GO TO 400	A3810
	390 SPLDIF=9999999.9	A3820
	GO TO 410	A3830
	400 CONTINUE	A3840
	SUMDIF=SUMDIF+SPLDIF**2	A3850
	NF=NF+1	A3860
	410 WRITE (6,1010) FREQ(I),SPLA(I),SPLB(I),SPLT(I),SPLM(IH,JJ),SPLDIF,	A3870*
	1SUMDIF	A3880
	GO TO 430	A3890
	420 WRITE (6,1020) FREQ(I),SPLA(I),SPLB(I),SPLT(I)	A3900*
	430 CONTINUE	A3910
C		A3920
	IF (ICOMP,EQ.1) GO TO 620	A3930
	STDEV=0.0	A3940
	IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A3950
	WRITE (6,1030) STDEV	A3960*
	GO TO 620	A3970
C		A3980
C	COMPUTATION FOR OPTION 5 -- TOTAL NOISE = B+C	A3990
C		A4000
	440 WRITE (6,1040) TM(J)	A4010*
	IF (ICOMP,EQ.1) GO TO 450	A4020
	WRITE (6,1050)	A4030*
	GO TO 460	A4040
	450 WRITE (6,1060)	A4050*
C		A4060
	460 CONTINUE	A4070
	SUMDIF=0.0	A4080
	IH=IOFF	A4090
	NF=0	A4100
	DO 510 I=1,NFREQ	A4110
	SPLT(I)=10.0*ALOG10(10.0**((SPLB(I)/10.0)+10.0**((SPLC(I)/10.0)))	A4120

IF (ICOMP.EQ.1) GO TO 500	A4130
IH=IH+1	A4140
SPLDIF=SPLT(I)-SPLM(IH,JJ)	A4150
IF (SPLM(IH,JJ).LE.10.0) GO TO 470	A4160
IF (SPLB(I).LE.15.0) GO TO 470	A4170
IF (SPLC(I).LT.10.0) GO TO 470	A4180
GO TO 480	A4190
470 SPLDIF=9999999.9	A4200
GO TO 490	A4210
480 CONTINUE	A4220
SUMDIF=SUMDIF+SPLDIF**2	A4230
NF=NF+1	A4240
490 WRITE (6,1070) FREQ(I),SPLB(I),SPLC(I),SPLT(I),SPLM(IH,JJ),SPLDIF,	A4250*
1SUMDIF	A4260
GO TO 510	A4270
500 CONTINUE	A4280
WRITE (6,1080) FREQ(I),SPLB(I),SPLC(I),SPLT(I)	A4290*
510 CONTINUE	A4300
C	A4310
IF (ICOMP.EQ.1) GO TO 620	A4320
STDEV=0.0	A4330
IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A4340
WRITE (6,1090) STDEV	A4350*
GO TO 620	A4360
C	A4370
C COMPUTATION FOR OPTION 6 -- TOTAL NOISE = A+C	A4380
C	A4390
520 WRITE (6,1100) TM(J)	A4400*
C	A4410
DO 530 I=1,NFREQ	A4420
SPLT(I)=10.0*ALOG10(10.0**((SPLA(I)/10.0)+10.0**((SPLC(I)/10.0)))	A4430
WRITE (6,1110) FREQ(I),SPLA(I),SPLC(I),SPLT(I)	A4440*
530 CONTINUE	A4450
C	A4460
GO TO 620	A4470
C	A4480
C COMPUTATION FOR OPTION 7 -- TOTAL NOISE = A+B+C	A4490
C	A4500
540 WRITE (6,1120) TM(J)	A4510*
IF (ICOMP.EQ.1) GO TO 550	A4520
WRITE (6,1130)	A4530*
GO TO 560	A4540
550 WRITE (6,1140)	A4550*
560 CONTINUE	A4560
C	A4570
SUMDIF=0.0	A4580
IH=IOFF	A4590
NF=0	A4600
DO 610 I=1,NFREQ	A4610
SPLT(I)=10.0*ALOG10(10.0**((SPLA(I)/10.0)+10.0**((SPLB(I)/10.0)+10.0	A4620
1**((SPLC(I)/10.0)))	A4630
IF (ICOMP.EQ.1) GO TO 600	A4640
IH=IH+1	A4650
SPLDIF=SPLT(I)-SPLM(IH,JJ)	A4660
IF (SPLM(IH,JJ).LE.10.0) GO TO 570	A4670
IF ((SPLA(I).LE.10.0.AND.SPLB(I).LE.15.0).OR.SPLC(I).LE.10.0) GO TO 5	A4680
170	A4690
GO TO 580	A4700
570 SPLDIF=9999999.9	A4710

GO TO 590	A4720
580 SUMDIF=SUMDIF+SPLDIF**2	A4730
NF=NF+1	A4740
590 WRITE (6,1150) FREQ(I),SPLA(I),SPLB(I),SPLC(I),SPLT(I),SPLM(IH,JJ)	A4750*
1,SPLDIF,SUM	A4760
GO TO 610	A4770
600 CONTINUE	A4780
WRITE (6,1160) FREQ(I),SPLA(I),SPLB(I),SPLC(I),SPLT(I)	A4790*
610 CONTINUE	A4800
C IF (ICOMP.EQ.1) GO TO 620	A4810
STDEV=0.0	A4820
IF (NF.GT.0) STDEV=SQRT(SUMDIF/NF)	A4830
WRITE (6,1170) STDEV	A4840
GO TO 620	A4850*
C	A4860
C	A4870
C END ANGLE LOOP	A4880
C	A4890
620 CONTINUE	A4900
GO TO 40	A4910
630 STOP	A4920
C	A4930
640 FORMAT (1H1,10X,"DATE ",1A10,10X,"TIME ",1A10,//)	A4940
650 FORMAT (2X,"***LARGE SCALE NOISE FAILURES ARE INDICATED BY THE ","	A4950
1FOLLOWING***",//5X,"SPLA=1.0 STABILITY CALCULATIONS FAILED TO CO	A4960
2NVERGE",/5X,"SPLA=2.0 LARGE SCALE NOISE AT THIS JET VELOCITY IS N	A4970
3EGLECTED ",/5X,"SPLA=3.0 LARGE SCALE NOISE AT THIS ANGLE IS NEGLE	A4980
4CTED",/5X,"SPLA=4.0 LARGE SCALE NOISE AT THIS FREQUENCY IS NEGLEC	A4990
5TED",/5X,"SPLA=5.0 SEARCH FOR STARTING VALUES GIVES SINGULAR MAT	A5000
6RIX",////)	A5010
660 FORMAT (2X,"***TURBULENT MIXING NOISE (BOPNO 1) FAILURES ARE INDIC	A5020
ATED BY THE FOLLOWING***",//5X,"SPLB=1.0 VELOCITY PROFILE GRADIENT	A5030
2T IS NOT AVAILABLE",/5X,"SPLB=2.0 SM IS OUTSIDE THE RANGE OF SOURCE	A5040
3CE DATA",/5X,"SPLB=3.0 SOURCE DIRECTIVITY EXPRESSION IS LESS THAN	A5050
4 ZERO",/5X,"SPLB=4.0 NUMBER OF ITERATIONS EXCEEDS 50",/5X,"SPLB=5	A5060
5.0 SM GOES NEGATIVE IN ITERATION ROUTINE",/5X,"SPLB=6.0 ARGUMENT	A5070
6 X IN DECAY FACTOR IS NEGATIVE",/5X,"SPLB=7.0 RADIATION ANGLE IS	A5080
7LESS THAN 30.0 DEGREES",/5X,"SPLB=8.0 TURBULENT MIXING NOISE AT T	A5090
8HIS ANGLE AND JET ","VELOCITY IS NEGLECTED",////)	A5100
670 FORMAT (2X,"***TURBULENT MIXING NOISE (BOPNO 2) FAILURES ARE INDIC	A5110
ATED BY THE FOLLOWING***",//5X,"SPLB=2.0 SM IS OUTSIDE THE RANGE	A5120
2OF SOURCE DATA",/5X,"SPLB=3.0 SOURCE DIRECTIVITY EXPRESSION IS LE	A5130
3SS THAN ZERO",/5X,"SPLB=4.0 NUMBER OF ITERATIONS EXCEEDS 50",/5X,	A5140
4"SPLB=5.0 SM GOES NEGATIVE IN ITERATION ROUTINE",/5X,"SPLB=8.0 T	A5150
5URBULENT MIXING NOISE AT THIS ANGLE AND JET ","VELOCITY IS NEGLECT	A5160
6ED",/5X,"SPLB=9.0 CRITICAL LAYER RADIUS TOO SMALL",/5X,"SPLB=10	A5170
7.0 BESSEL FUNCTION FAILURE",/5X,"SPLB=11.0 SOURCE AND CRITICAL	A5180
8LAYER RADIUS COINCIDE",////)	A5190
680 FORMAT (2X,"***SHOCK ASSOCIATED NOISE FAILURES ARE INDICATED BY TH	A5200
1E FOLLOWING***",//5X,"SPLC=1.0 MJ IS LESS THAN 1.0",/5X,"SPLC=2.0	A5210
2 SIGMA IS OUTSIDE THE RANGE OF MASTER SPECTRA",/5X,"SPLC=3.0 SHO	A5220
3CK NOISE CONTRIBUTION AT THIS ANGLE AND JET"," TEMPERATURE"/15X,"C	A5230
4AN BE (AND IS) NEGLECTED")	A5240
690 FORMAT (8F10.0)	A5250
700 FORMAT (16I5)	A5260
710 FORMAT (12F6.1)	A5270
720 FORMAT (1H1,//////17X,40H***** UNIFIED JET NOISE PREDICTION *****	A5280
1///32X,10HTEST POINT,14,///31X,13HOPTION NUMBER,13,///5X,20HRESERV	A5290
2OIR PRESSURE =,F6.2,28H PSI, ATMOSPHERIC PRESSURE =,F6.2,4H PSI,/1	A5300

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3X,23HRESERVOIR TEMPERATURE =,F7.1,29H DEG.F, CHAMBER TEMPERATURE = A5310
4,F7.1,5H DEG.F,/31X,7HGAMMA =,F5.2) A5320
730 FORMAT (//10X,22HPRESSURE RATIO PR/P0 =,F6.3,/10X,25HTEMPERATURE R A5330
ATIO TR/T0 =,F6.3,/10X,36HJET STATIC TEMPERATURE RATIO TJ/T0 =,F6. A5340
23,/10X,25HJET DENSITY RATIO DJ/D0 =,F6.3,/10X,26HJET VELOCITY RATI A5350
30 VJ/A0 =,F6.3,/10X,20HJET MACH NUMBER MJ =,F6.3,/10X,17HJET VELOC A5360
ITY VJ =,F7.1,4H FPS) A5370
740 FORMAT (//10X,17HNOZZLE DIAMETER =,F6.2,7H INCHES,/10X,21HMICROPHO A5380
NE DISTANCE =,F6.2,5H FEET,/10X,5HR/D =,F6.2) A5390
750 FORMAT (//,10X,"TURBULENCE INTENSITY RADIAL HALF WIDTH = ",E13.6) A5400
760 FORMAT (10X,"RADIAL COHERENCE LENGTH SCALE COEFFICIENTS (A,B) = ", A5410
E13.6," , ",E13.6) A5420
770 FORMAT (///10X,37H**SHOCK ASSOCIATED NOISE PARAMETERS**,//10X,3HC A5430
1 =,F5.2,5X,4HK0 =,F5.2,5X,4HK1 =,F5.2,/10X,21HNUMBER OF SHOCKS NS A5440
2=,I3) A5450
780 FORMAT (//10X,6HBETA =,F6.3,/10X,29HEDDY CONVECTION VELOCITY VC =, A5460
1F7.1,4H FPS,/10X,32HEDDY CONVECTION MACH NUMBER MC =,F6.3,/10X,30H A5470
2AVERAGE SHOCK CELL LENGTH L0 =,F7.3,7H INCHES,/10X,28HFIRST SHOCK A5480
3CELL LENGTH L1 =,F7.3,7H INCHES) A5490
790 FORMAT (1H1,////,5X,"NOISE FROM LARGE-SCALE TURBULENCE ","STRUCT A5500
TURE",////,5X,"OBSERVER ANGLE =",F7.2," DEGREES",///,1X,3X,"FREQ(HZ) A5510
2",4X,"SPLA(DB)",16X,"SPLM(DB)",4X,"DIFF",9X,"SUM",/) A5520
800 FORMAT (1H1,////,5X,"NOISE FROM LARGE-SCALE TURBULENCE STRUCTURE" A5530
1,///,5X,16HOBSERVER ANGLE =,F7.2,8H DEGREES,///1X,3X,"FREQ(HZ)",4X, A5540
2"SPLA(DB)",/) A5550
810 FORMAT (2X,2F10.1,14X,2(4X,F6.1),2X,F12.1) A5560
820 FORMAT (2X,F10.1,F10.1) A5570
830 FORMAT (//,40X,"STANDARD DEVIATION = ",F7.2) A5580
840 FORMAT (1H1,////,5X,"TURBULENT MIXING NOISE (BOPNO =",I2,")") A5590
850 FORMAT (/,T2,"*** ALTERNATIVE AXIAL SOURCE LOCATION MODEL ","UTILI A5600
IZED ***") A5610
860 FORMAT (/,T2,"*** DISPLACEMENT SOURCE MODEL ***") A5620
870 FORMAT (///,5X,"OBSERVER ANGLE =",F7.2," DEGREES",///,1X,3X,"FREQ( A5630
1HZ)",4X,"FD/VJ",6X,"SM",5X,"SPLPQ(DB)",1X,"SPLPD(DB)",2X,"SPLB(DB) A5640
2",16X,"SPLM(DB)",4X,"DIFF",9X,"SUM",/) A5650
880 FORMAT (///,5X,16HOBSERVER ANGLE =,F7.2,8H DEGREES,///1X,3X,"FREQ( A5660
1HZ)",4X,"FD/VJ",6X,"SM",5X,"SPLPQ(DB)",1X,"SPLPD(DB)",2X,"SPLB(DB) A5670
2"/) A5680
890 FORMAT (1X,F10.1,2F10.3,3F10.1,2X,A2,10X,2(4X,F6.1),2X,F12.1) A5690
900 FORMAT (1X,F10.1,2F10.3,3F10.1,2X,A2) A5700
910 FORMAT (//,74X,"STANDARD DEVIATION = ",F7.2) A5710
920 FORMAT (1H1,////,5X,"SHOCK ASSOCIATED NOISE",///5X,16HOBSERVER AN A5720
GLE =,F7.2,8H DEGREES,///) A5730
930 FORMAT (1X,3X,"FREQ(HZ)",3X,"SIGMA",3X,"H0(DB)",3X,"C1",3X,"ANS3(D A5740
1B)",3X,"ANS2(DB)",5X,"SPLC(DB)",16X,"SPLM(DB)",4X,"DIFF",9X,"SUM", A5750
2/) A5760
940 FORMAT (1X,3X,"FREQ(HZ)",3X,"SIGMA",3X,"H0(DB)",3X,"C1",3X,"ANS3(D A5770
1B)",3X,"ANS2(DB)",5X,"SPLC(DB)",/) A5780
950 FORMAT (2X,F10.1,3X,F5.2,3X,F6.1,2X,F4.2,2X,F7.1,4X,F7.1,5X,F7.1,1 A5790
15X,2(4X,F6.1),2X,F12.1) A5800
960 FORMAT (2X,F10.1,3X,F5.2,3X,F6.1,2X,F4.2,2X,F7.1,4X,F7.1,5X,F7.1) A5810
970 FORMAT (//,85X,"STANDARD DEVIATION = ",F7.2) A5820
980 FORMAT (1H1,////,5X,"TOTAL NOISE",///5X,16HOBSERVER ANGLE =,F7.2, A5830
18H DEGREES,///) A5840
990 FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLB(DB)",2X,"SPLT(DB)" A5850
1,19X,"SPLM(DB)",19X,"DIFF",13X,"SUMDIFF",/) A5860
1000 FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLB(DB)",2X,"SPLT(DB)" A5870
1,/) A5880
1010 FORMAT (2X,4F10.1,19X,F10.1,14X,F6.1,8X,F12.1) A5890

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1020 FORMAT (2X,4F10.1)	A5900
1030 FORMAT (///,T79,"STANDARD DEVIATION = ",F6.1)	A5910
1040 FORMAT (1H1,//////5X,"TOTAL NOISE",///5X,16HOBSERVER ANGLE =,F7.2,	A5920
18H DEGREES,///)	A5930
1050 FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLB(DB)",2X,"SPLC(DB)",2X,"SPLT(DB)"	A5940
1,16X,"SPLM(DB)",4X,"DIFF",9X,"SUM",/)	A5950
1060 FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLB(DB)",2X,"SPLC(DB)",2X,"SPLT(DB)"	A5960
1/)	A5970
1070 FORMAT (2X,4F10.1,16X,2(4X,F6.1),2X,F12.1)	A5980
1080 FORMAT (2X,4F10.1)	A5990
1090 FORMAT (///,T64,"STANDARD DEVIATION = ",F6.1)	A6000
1100 FORMAT (1H1,//////5X,"TOTAL NOISE",///5X,16HOBSERVER ANGLE =,F7.2,	A6010
18H DEGREES,///1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLC(DB)",2X,"SPL	A6020
2T(DB)"/)	A6030
1110 FORMAT (2X,4F10.1)	A6040
1120 FORMAT (1H1,//////5X,"TOTAL NOISE",///5X,16HOBSERVER ANGLE =,F7.2,	A6050
18H DEGREES,///)	A6060
1130 FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLB(DB)",2X,"SPLC(DB)"	A6070
1,2X,"SPLT(DB)",16X,"SPLM(DB)",4X,"DIFF",9X,"SUM",/)	A6080
1140 FORMAT (1X,4X,"FREQ(HZ)",3X,"SPLA(DB)",2X,"SPLB(DB)",2X,"SPLC(DB)"	A6090
1,2X,"SPLT(DB)"/)	A6100
1150 FORMAT (2X,5F10.1,15X,2(4X,F6.1),2X,F12.1)	A6110
1160 FORMAT (2X,5F10.1)	A6120
1170 FORMAT (///,T71,"STANDARD DEVIATION = ",F6.1)	A6130
END	A6140-

*DECK CALPER		
SUBROUTINE CALPER (VJA0,TJT0,P0,T0F,TRF,PRG,TRK,TRT0,PRP0,PRGA,DJD	B	10
10,MJ,A0,VJ,GAMA,OPPER)	B	20
REAL MJ	B	30
INTEGER OPFER	B	40
DIMENSION GAM(11)	B	50
IF (OPFER.EQ.1) GO TO 30	B	60
	B	70
C	B	80
C	B	90
C	B	100
CALCULATIONS FROM INPUT OF TJT0,VJA0,T0F,AND P0	B	110
TRK=5./9.*(T0F+460.0)*TJT0	B	120
TOK=(5.0*(T0F+460.0))/9.0	B	130
GAMA0=1.421-(TOK/11800.0)*(EXP(-ABS(TOK-450.0)/200.0)/80.0)	B	140
IF (TOK.LE.290.0) GAMA0=1.402	B	150
A0=SQRT(GAMA0*1716.8*(T0F+460.0))	B	160
TJK=TJT0*TOK	B	170
GAMAJ=1.421-(TJK/11800.0)*(EXP(-ABS(TJK-450.0)/200.0)/80.0)	B	180
IF (TJK.LE.290.0) GAMAJ=1.402	B	190
GJG0=GAMAJ/GAMA0	B	200
MJ=VJA0/SQRT(GJG0*TJT0)	B	210
VJ=VJA0*A0	B	220
DJD0=1.0/TJT0	B	230
GAM(1)=0.0	B	240
DO 10 I=2,11	B	250
GAM(I)=1.421-(TRK/11800.0)*(EXP(-ABS(TRK-450.0)/200.0)/80.0)	B	260
IF (TRK.LE.290.0) GAM(I)=1.402	B	270
PRGA=1.0+((GAM(I)-1.0)/2.0*MJ**2)	B	280
PRP0=PRGA**((GAM(I)/(GAM(I)-1.0))	B	290
TRT0=TJT0*PRGA	B	300
TRK=5./9.*(T0F+460.0)*TRT0	B	310
PRG=(PRP0-1.0)*P0	B	320
TRF=TRT0*(T0F+460.0)-460.0	B	330
DIFF=ABS(GAM(I)-GAM(I-1))	B	340
JJ=I	B	350
IF (DIFF.LE.0.0001) GO TO 20	B	360
10 CONTINUE	B	370
WRITE (6,40)	B	380
STOP 100	B	390
20 GAMA=GAM(JJ)	B	400
RETURN	B	410
C	B	420
C	B	430
C	B	440
CALCULATIONS FROM INPUT OF P0,T0F,PRG, AND TRF	B	450
30 PRP0=(PRG/P0)+1.0	B	460
TRT0=(TRF+460.0)/(T0F+460.0)	B	470
TRK=(5.0*(TRF+460.0))/9.0	B	480
GAMA=1.421-(TRK/11800.0)*(EXP(-ABS(TRK-450.0)/200.0)/80.0)	B	490
IF (TRK.LE.290.0) GAMA=1.402	B	500
PRGA=PRP0**((GAMA-1.0)/GAMA)	B	510
MJ=SQRT((2.0/(GAMA-1.0))*(PRGA-1.0))	B	520
TJT0=TRT0/PRGA	B	530
DJD0=1.0/TJT0	B	540
TOK=(5.0*(T0F+460.0))/9.0	B	550
GAMA0=1.421-(TOK/11800.0)*(EXP(-ABS(TOK-450.0)/200.0)/80.0)	B	560
IF (TOK.LE.290.0) GAMA0=1.402	B	570
A0=SQRT(GAMA0*1716.8*(T0F+460.0))	B	580
TJK=TJT0*TOK		
GAMAJ=1.421-(TJK/11800.0)*(EXP(-ABS(TJK-450.0)/200.0)/80.0)		
IF (TJK.LE.290.0) GAMAJ=1.402		

GJG0=GAMAJ/GAMA0	B 590
VJA0=MJ*SQRT(GJG0*JT0)	B 600
VJ=VJA0*A0	B 610
RETURN	B 620
C 40 FORMAT (///.1X,"***** THE GAMA ITERATION FAILED TO CONVERGE ", "AFT	B 630
1ER 10 TRIES. COMPUTATION STOPPED - CHECK INPUT, *****)	B 640
END	B 650
	B 660-

*DECK	LSMAIN		C 10
	SUBROUTINE LSMAIN (VJA,TJT,GAMA,DFT,VJ,F,I,NANG,TH,IFN,SPLLS)		C 20
C			C 30
C	THIS PROGRAM IS AN INTERMEDIATE STEP BETWEEN UNIMAIN AND		C 40
C	LSNOISE TO HANDLE INITIALIZATION AND ERROR PROCESSING		C 50
			C 60
	DIMENSION TM(20),PTHETA(20),PDB(20),SPLLS(30,20)		C 70
	COMPLEX ALPHA,OKDB		C 80
	REAL MACH2,MLS		C 90
	INTEGER GAMMA		C 100
	COMMON/INFO/ALPHA,OMEGA,MACH2,TJT0,NORD,GM1,OKDB,IFLG,VJA0		C 110
	TJT0=TJT		C 120
	VJA0=VJA		C 130
	IFLG=IFN		C 140
	B0=0.05		C 150
	GAMMA=8		C 160
	INF=0		C 170
	RADNF=0.		C 180
	RSTART=0.		C 190
	XLAST=0.		C 200
	FREQ=F		C 210
	IEROR=0		C 220
	SN=F*DFT/VJ		C 230
	MLS=17.2*ALOG10(10.0*SN)		C 240
	CLS=74.13*SN**(-0.136)		C 250
	CAL=MLS*10.0*ALOG10(VJA0)*CLS		C 260
	IF (VJA0.LT.1.15) GO TO 20		C 270
	IF (SN.LT.0.1.OR.SN.GT.0.5) GO TO 40		C 280
	CALL LSNOIS (FREQ,TH,NANG,GAMA,DFT,VJ,B0,GAMMA,INF,RADNF,XLAST,RST		C 290
	IART,PTHETA,PDB,IEROR)		C 300
	IF (IEROR.EQ.1) RETURN		C 310
	IF (IEROR.EQ.2) GO TO 60		C 320
	DO 10 J=1,NANG		C 330
	SPLLS(I,J)=PDB(J)*CAL		C 340
	IF (TM(J).LT.15.0.OR.TM(J).GT.45.0) SPLLS(I,J)=3.0		C 350
10	CONTINUE		C 360
	RETURN		C 370
20	DO 30 J=1,NANG		C 380
30	SPLLS(I,J)=2.0		C 390
	RETURN		C 400
40	DO 50 J=1,NANG		C 410
50	SPLLS(I,J)=4.0		C 420
	RETURN		C 430
60	DO 70 J=1,NANG		C 440
70	SPLLS(I,J)=5.0		C 450
	RETURN		C 460-
	END		


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*DECK LSNOISE
SUBROUTINE LSNOIS (FREQ,TM,NANG,GAMA,DFT,VJ,B0,GAMMA,INF,RADNF,XLA D 10
1ST,RSTART,PTheta,PDB,IEROR) D 20
DIMENSION TM(NANG),PTheta(NANG),PDB(NANG) D 30
***** D 40
C * D 50
C * THIS PROGRAM DETERMINES THE GROWTH OF PRESSURE D 60
C * FLUCTUATIONS IN A DIVERGING, COMPRESSIBLE D 70
C * AXISYMMETRIC JET. D 80
C * D 90
C ***** D 100
COMPLEX PY(3),Y(3),DY(3),P(3),Q(3),ACON(130),BB(130),ALPHA D 110
COMPLEX BB4,CSTEP,LIM(6),RADC,RAD,DIR(6) D 120
COMPLEX UVAL,DUVAL,CVAL,LAMDAM,LAMDAP,ETAC D 130
COMPLEX RHO,DRHO,AC,PP,DPP,ADAT(100),CDAT(100) D 140
COMPLEX DUDS,D2UDRS,DRDS,D2RDRS D 150
COMPLEX HSUM(2,3,2),ISUM(2,2),DUMH(3),DUM,DUM1,L1,L2 D 160
COMPLEX DKDB D 170
COMPLEX ARG,H01,H02,H11,H12,I0,I1 D 180
COMPLEX E0,E1,E2,E3,A2,A4 D 190
REAL MACH2 D 200
INTEGER GAMMA D 210
DIMENSION SDAT(100) D 220
COMMON/INFO/ALPHA,OMEGA,MACH2,TJTO,NORD,GM1,DKDB,IFLG,VJA0 D 230
COMMON/SPR/HTHETA,S,KEY1,UCENT,DUCDS,BETA1,BETA2,IFUNC D 240
COMMON/DECAY/ ID,SD D 250
SMIN1=2.5E-4 D 260
SMAX1=.05 D 270
ERMIN=.1 D 280
ERMAX=.14 D 290
ERMIN=.1 D 300
ERMAX=.14 D 310
PI=3.14159265 D 320
A=.693147 D 330
STRNO=FREQ*DFT/VJ D 340
NTT=0 D 350
ID=0 D 360
SD=1000. D 370
C D 380
C SET UP CONDITIONS FOR STABILITY CALCULATION D 390
C D 400
C STARTING RADIUS D 410
RST1=0.05 D 420
C FINISHING RADIUS D 430
RFIN=4. D 440
C DIMENSIONS OF COMPLEX CONTOUR DEFORMATION D 450
ETA11=0.5 D 460
ETA21=0.5 D 470
C NUMBER OF THICKNESSES TO BE CALCULATED D 480
NLIM=70 D 490
C 3* VARIATION IN PERCENTAGE FOR WAVENUMBER GUESSES D 500
PERCR=0.005 D 510
PERCI=0.005 D 520
C THICKNESS STEP SIZE D 530
DS=0.005/STRNO D 540
C STARTING THICKNESS FOR BOUNDARY LAYER D 550
S=0.05-DS D 560
C SET UP CALCULATED VALUE OF MODENUMBER D 570
NORD=1 D 580

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	AN=FLOAT(NORD)	D 590
	GM1=GAMA-1	D 600
	MACH2=VJA0*VJA0	D 610
	NORD1=NORD+1	D 620
10	S=S*DS	D 630
C		D 640
C	ADJUST MINIMUM AND MAXIMUM STEP SIZES TO THE LOCAL WIDTH	D 650
C		D 660
	SMIN=SMIN1*S	D 670
	SMA1=SMA1*S	D 680
	IF (SMIN.GT.SMIN1) SMIN=SMIN1	D 690
	IF (SMA1.LT.SMA1) SMA1=SMA1	D 700
	ETA1=ETA11*S	D 710
	ETA2=ETA21*S	D 720
C		D 730
C	CALCULATE THE LOCAL POTENTIAL CORE RADIUS	D 740
C	OR THE CENTERLINE VELOCITY	D 750
C		D 760
	KEY1=3	D 770
	BETA1=0.	D 780
	BETA2=0.	D 790
	UCENT=1.	D 800
	RAD=CMPLX(-.0125,0.)	D 810
	DO 20 I=1,161	D 820
	RAD=RAD*.025	D 830
	CALL UEVAL (RAD,UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	D 840
	VAL=REAL(RHO*UVAL*UVAL)	D 850
	BETA1=BETA1+VAL*.025	D 860
	BETA2=BETA2+VAL*REAL(RAD)*.025	D 870
	IF (ABS(VAL).LT.1.E-5) GO TO 30	D 880
20	CONTINUE	D 890
C		D 900
C	CALCULATION OF THE POTENTIAL CORE RADIUS	D 910
C		D 920
30	VAL=S*S*((TJT0*BETA1)**2-2.*TJT0*BETA2)+1.	D 930
	IF (VAL) 70,40,40	D 940
40	VAL=-S*BETA1*TJT0+SQRT(VAL)	D 950
	IF (VAL) 70,50,50	D 960
50	HTHETA=VAL	D 970
	KEY1=1	D 980
	IF (HTHETA.LT.RST1) GO TO 60	D 990
	RST=HTHETA+.1E-10	D1000
	GO TO 150	D1010
60	RST=RST1	D1020
	GO TO 150	D1030
C		D1040
C	CALCULATION OF THE CENTERLINE VELOCITY	D1050
C		D1060
70	KEY1=4	D1070
80	BETA2=0.	D1080
	RAD=CMPLX(-.0125,0.)	D1090
	USAVE=UCENT	D1100
	DO 90 I=1,161	D1110
	RAD=RAD*.025	D1120
	CALL UEVAL (RAD,UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	D1130
	VAL=REAL(RHO*UVAL*UVAL)	D1140
	BETA2=BETA2+VAL*REAL(RAD)*.025	D1150
	IF (ABS(VAL).LT.1.E-5) GO TO 100	D1160
90	CONTINUE	D1170

100	UCENT=1./SQRT(2.*TJT0*BETA2)/S	D1180
	IF (ABS(UCENT-USAVE).LT.1.E-4) GO TO 110	D1190
	GO TO 80	D1200
C		D1210
C	CALCULATION OF RATE OF CHANGE OF CENTERLINE VELOCITY	D1220
C	WITH LOCAL THICKNESS	D1230
C		D1240
110	AA=GM1*MACH2/2.	D1250
	BA=(1.-TJT0-AA)	D1260
	AK=SQRT(BA*BA+4.*AA)	D1270
	IF (VJA0.LT.1.E-10) GO TO 120	D1280
	DUCDS=-((AA*UCENT+BA)*UCENT-1.)*(ALOG(ABS((AA*UCENT+BA)*UCENT-1.))	D1290
	1-BA*ALOG(ABS((2.*AA*UCENT+BA-AK)*(BA+AK)/(2.*AA*UCENT+BA+AK)/(BA-A	D1300
	2K)))/AK)/UCENT/S/AA	D1310
	GO TO 140	D1320
120	BA=1.-TJT0	D1330
	IF (ABS(BA).LT.1.E-10) GO TO 130	D1340
	DUCDS=2.*(1.-BA*UCENT)*(BA*UCENT+ALOG(ABS(1.-BA*UCENT)))/S/UCENT/B	D1350
	1A/BA	D1360
	GO TO 140	D1370
130	DUCDS=-UCENT/S	D1380
140	KEY1=2	D1390
	GO TO 160	D1400
150	YMAX=RFIN*S*HMHETA	D1410
	GO TO 170	D1420
160	YMAX=RFIN*S	D1430
170	CONTINUE	D1440
C		D1450
C	READ IN OR INTERPOLATE FOR THE GUESSED VALES OF ALPHA	D1460
C		D1470
	IF (NTT.EQ.NLIM) GO TO 710	D1480
	IF (NTT.EQ.0) GO TO 190	D1490
	ALPHA=ALPHA+DKDB*DS	D1500
C		D1510
C	CONVERGENCE SEARCH FOR DAMPED SUPERSONIC WAVE	D1520
C		D1530
	IF (AIMAG(ALPHA).LT.0.) GO TO 180	D1540
	IF ((OMEGA/REAL(ALPHA)).LT.(1./VJA0)) GO TO 180	D1550
	ID=1	D1560
	SD=S-DS	D1570
	GO TO 710	D1580
180	ACON(1)=ALPHA	D1590
	ACON(2)=CMPLX((1.-PERCR)*REAL(ALPHA),(1.-PERCI)*AIMAG(ALPHA))	D1600
	ACON(3)=CMPLX((1.+PERCR)*REAL(ALPHA),(1.+PERCI)*AIMAG(ALPHA))	D1610
	NT=3	D1620
	GO TO 200	D1630
C		D1640
C	DETERMINE THE STARTING VALUES FROM TABULATION	D1650
C		D1660
190	CALL ASTART (VJA0,STRNO,TJT0,ALPHA,NORD,IEROR)	D1670s
	IF (IEROR.NE.2) GO TO 180	D1680
	RETURN	D1690
C		D1700
C	CALCULATE STROUHAL NUMBER AND RADIAN FREQUENCY	D1710
C		D1720
200	STRNO=FREQ*DFT/VJ	D1730
	OMEGA=STRNO*PI	D1740
	IF (IFLG.EQ.0) GO TO 210	D1750

	WRITE (6,740) NORD,VJA0,TJT0,STRNO,OMEGA,S	D1760*
210	IF (KEY1.EQ.2) GO TO 220	D1770
	IF (IFLG.EQ.0) GO TO 230	D1780
	WRITE (6,750) MTHETA	D1790*
	GO TO 230	D1800
220	IF (IFLG.EQ.0) GO TO 230	D1810
	WRITE (6,760) UCENT	D1820*
C		D1830
C	BEGIN THE INTEGRATION AND CALCULATE THE	D1840
C	STARTING VECTORS	D1850
C		D1860
230	KK=0	D1870
	IFUNC=1	D1880
	IF (IFLG.EQ.0) GO TO 240	D1890
	WRITE (6,830) BETA1,BETA2	D1900*
240	KK=KK+1	D1910
	ALPHA=ACON(KK)	D1920
C		D1930
C	IF KEY1 = 2 THE STARTING VECTORS ARE OBTAINED FROM A	D1940
C	SERIES SOLUTION	D1950
C		D1960
250	IF (KEY1.EQ.2) GO TO 290	D1970
	LAMDAM=CSQRT(ALPHA*ALPHA-MACH2*(ALPHA-OMEGA)*(ALPHA-OMEGA)/TJT0)	D1980
	DO 260 I=1,3	D1990
260	Y(I)=(0.,0.)	D2000
	Y(1)=CMPLX(RST,0.)	D2010
	ARG=LAMDAM*Y(1)	D2020
	PHI=ATAN2(AIMAG(ARG),REAL(ARG))	D2030
	IF (PHI.GT.=PI.AND.PHI.LE.PI/2.) GO TO 270	D2040
	ARG=ARG*(0.,-1.)	D2050
	CALL NCBRTS (ARG,H01,H02,NORD,0)	D2060S
	CALL NCBRTS (ARG,H11,H12,NORD1,0)	D2070S
	I0=CEXP((0.,1.)*AN*PI/2.)*H01	D2080
	I1=CEXP((0.,1.)*(AN+1.)*PI/2.)*H11	D2090
	GO TO 280	D2100
270	ARG=ARG*(0.,1.)	D2110
	CALL NCBRTS (ARG,H01,H02,NORD,0)	D2120S
	CALL NCBRTS (ARG,H11,H12,NORD1,0)	D2130S
	I0=CEXP((0.,-1.)*AN*PI/2.)*H01	D2140
	I1=CEXP((0.,-1.)*(AN+1.)*PI/2.)*H11	D2150
280	Y(2)=I0	D2160
	Y(3)=AN*I0/Y(1)+LAMDAM*I1	D2170
	GO TO 300	D2180
C		D2190
C	SERIES SOLUTION FOR THE STARTING VECTORS	D2200
C		D2210
290	RHO=1./(1.-(1.-TJT0)*UCENT+0.5*GM1*MACH2*UCENT*(1.-UCENT))	D2220
	DRHO=-UCENT*RHO*RHO*(1.-TJT0-0.5*GM1*MACH2*(1.-2.*UCENT))	D2230
	D2RDR2=2.*DRHO*DRHO/RHO-DRHO*GM1*MACH2*RHO*RHO*UCENT*UCENT	D2240
	DUM=ALPHA*UCENT-OMEGA	D2250
	E0=(MACH2*DUM*DUM*RHO-ALPHA*ALPHA)	D2260
	E1=(4.*ALPHA*UCENT/DUM-2.*DRHO/RHO)*A/S/S	D2270
	E2=MACH2*DUM*(DUM*DRHO-2.*ALPHA*UCENT*RHO)*A/S/S	D2280
	E3=(4.*ALPHA*UCENT*OMEGA/DUM/DUM-2.*(D2RDR2-DRHO*DRHO/RHO)/RHO)*A*	D2290
	1A/S**4	D2300
	A2=-(E0+AN*E1)/4./(AN+1.)	D2310
	A4=-(E2+AN*E3+A2*(E0+(AN+2.)*E1))/8./(AN+2.)	D2320
	Y(1)=CMPLX(RST1,0.)	D2330
	Y(2)=Y(1)*NORD*(1.+Y(1)*Y(1)*(A2+A4*Y(1)*Y(1)))	D2340

	Y(J)=Y(1)**(NORD-1)*(AN*Y(1)*Y(1)*((AN*2.)*A2*(AN*4.)*A4*Y(1)*Y(1	02350
	1))	02360
300	M=3	02370
C		02380
C	IF IFUNC = 1, EIGENVALUE IS BEING CALCULATED	02390
C	IF IFUNC = 2, DALPHA/DS IS BEING CALCULATED FROM THE	02400
C	SOLVABILITY CONDITION	02410
C		02420
	IF (IFUNC.EQ.1) GO TO 320	02430
	IF (KEY1.EQ.2) GO TO 310	02440
	DUM=ALPHA-OMEGA	02450
	HSUM(1,1,1)=(0.,0.)	02460
	HSUM(2,1,1)=2.*(ALPHA-MACH2*DUM/TJT0)*Y(1)*Y(2)*Y(2)/DUM/DUM	02470
	ISUM(1,1)=(0.,0.)	02480
	ISUM(2,1)=(ALPHA-MACH2*DUM/TJT0)*Y(1)*Y(1)*(I0*I0-I1*I1-2.*AN*I0*I	02490
	11/LAMDAM/Y(1))/DUM/DUM*TJT0	02500
	GO TO 320	02510
310	CALL UEVAL (Y(1),UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	02520S
	DUM=ALPHA*UVAL-OMEGA	02530
	HSUM(1,1,1)=((D2RDRS-DRHO*DRDS/RHO)/RHO/RHO+2.*ALPHA*(D2UDRS-ALPH	02540
	1A*DUVAL*DUDS/DUM)/RHO/DUM)*Y(3)/DUM/DUM-2.*MACH2*(DRDS/RHO*ALPHA*D	02550
	2UDS/DUM)*Y(2))*Y(2)*Y(1)	02560
	HSUM(2,1,1)=2.*(ALPHA-MACH2*DUM*RHO*UVAL)*Y(1)*Y(2)*Y(2)/DUM/DUM-2	02570
	1.*OMEGA*DUVAL*Y(3)*Y(2)*Y(1)/DUM**4/RHO	02580
	ISUM(1,1)=(0.,0.)	02590
	ISUM(2,1)=(0.,0.)	02600
320	INT=0	02610
C		02620
C	DETERMINE THE CONTOUR OF INTEGRATION=	02630
C	LOCATE THE CRITICAL POINT	02640
C		02650
	IND=0	02660
	DO 330 I=1,3	02670
330	DIR(I)=(1.,0.)	02680
	DO 340 I=4,6	02690
340	DIR(I)=(-1.,0.)	02700
	CVAL=OMEGA/ALPHA	02710
	ETAC=CSQRT(-CLOG(CVAL/UCENT)/A)	02720
	IF (KEY1.EQ.2) GO TO 350	02730
	RADC=ETAC*S*HETHETA	02740
	GO TO 360	02750
350	RADC=ETAC*S	02760
360	IF (REAL(RADC).GT.(2.*RST1)) GO TO 370	02770
	RST1=RST1/2.	02780
	GO TO 250	02790
370	TEMP1=AIMAG(RADC)*SIGN(ETA2,AIMAG(RADC))*SIGN(1.,-AIMAG(CVAL))	02800
C		02810
C	DECIDE WHETHER NECESSARY TO INTEGRATE AROUND	02820
C	THE CRITICAL POINT	02830
C		02840
	IF (ABS(AIMAG(RADC)).GT.ETA2.AND.AIMAG(CVAL).GT.0.) GO TO 380	02850
	DIR(2)=CMPLX(0.,SIGN(1.,TEMP1))	02860
	DIR(5)=DIR(2)	02870
C		02880
C	DEFINE THE LIMITS OF THE CONTOUR INTEGRATION	02890
C		02900
	LIM(1)=CMPLX(REAL(RADC)-ETA1,0.)	02910
	LIM(2)=CMPLX(REAL(RADC)-ETA1,TEMP1)	02920
	LIM(5)=CMPLX(REAL(RADC)+ETA1,TEMP1)	02930

LIM(4)=CMPLX(REAL(RADC)+ETA1,0.)	D2940
LIM(3)=CMPLX(REAL(RADC),TEMP1)	D2950
LIM(6)=LIM(3)	D2960
IF (REAL(LIM(1)).GT.REAL(Y(1))) GO TO 400	D2970
LIM(1)=Y(1)	D2980
LIM(2)=CMPLX(REAL(Y(1)),AIMAG(LIM(2)))	D2990
IF (IFLG.EQ.0) GO TO 400	D3000
IF (IFUNC.EQ.2) WRITE (6,840) (LIM(I),I=1,6)	D3010*
GO TO 400	D3020
380 DO 390 I=1,6	D3030
390 LIM(I)=CMPLX(REAL(RADC),0.)	D3040
400 CONTINUE	D3050
C	D3060
C	D3070
C	D3080
IWR=0	D3090
ISTEP=1	D3100
CSTEP=(0.,0.)	D3110
INT=0	D3120
K=1	D3130
H=SMIN*10.	D3140
IFL=1	D3150
410 PY(1)=Y(1)	D3160
PY(2)=Y(2)	D3170
PY(3)=Y(3)	D3180
420 IF (H.LT.SMIN) H=SMIN	D3190
IF (H.GT.SMAX) H=SMAX	D3200
IF (CABS(Y(1)-LIM(ISTEP)).GT.H) GO TO 430	D3210
H=CABS(Y(1)-LIM(ISTEP))	D3220
IF (IFL.EQ.1) IFL=2	D3230
IF (IFL.EQ.3) IFL=4	D3240
430 CSTEP=ABS(H)*DIR(ISTEP)	D3250
CALL PJMRUN (M,CSTEP,Y,DY,P,Q,ERRES)	D3260S
IND=IND+1	D3270
IF (ERRES.LT.ERMIN) GO TO 450	D3280
IF (ERRES.LT.ERMAX) GO TO 460	D3290
IF (H.LE.SMIN) GO TO 440	D3300
H=0.8*H	D3310
Y(1)=PY(1)	D3320
Y(2)=PY(2)	D3330
Y(3)=PY(3)	D3340
IF (IFL.EQ.2) IFL=1	D3350
IF (IFL.EQ.4) IFL=3	D3360
GO TO 420	D3370
440 IWR=1	D3380
GO TO 460	D3390
450 H=1.25*H	D3400
460 IF (IFUNC.EQ.1) GO TO 500	D3410
C	D3420
C	D3430
C	D3440
CALL UEVAL (Y(1),UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	D3450S
DUM=ALPHA*UVAL-OMEGA	D3460
DUM1=Y(1)*Y(2)/DUM/DUM/RHO	D3470
J=2	D3480
IF (INT.EQ.1) J=3	D3490
HSUM(1,J,K)=DUM1*((D2RDRS/RHO-DRHO*DRDS/RHO/RHO+2.*ALPHA*(D2UDRS/D	D3500
1UM-ALPHA*DUVAL*DUDS/DUM/DUM))*Y(3)-2.*MACH2*DUM*(DUM*DRDS*ALPHA*RH	D3510
20*DUDS)*Y(2))	D3520

HSUM(2,J,K)=DUM1*2.*((ALPHA=MACH2*DUM*RHO*UVAL)*Y(2)-OMEGA*DUVAL*Y	D3530
1(3)/DUM/DUM)	D3540
IF (J,EQ.3) GO TO 470	D3550
L1=CSTEP	D3560
IF (K,EQ.2) L1=-L1	D3570
INT=1	D3580
GO TO 500	D3590
470 L2=CSTEP	D3600
IF (K,EQ.2) L2=-L2	D3610
DO 490 J=1,2	D3620
DO 480 I=1,3	D3630
480 DUMH(I)=HSUM(J,I,K)	D3640
DUM1=ISUM(J,K)	D3650
CALL INTEG (DUMH,DUM1,L1,L2)	D3660S
ISUM(J,K)=DUM1	D3670
490 HSUM(J,1,K)=HSUM(J,3,K)	D3680
INT=0	D3690
500 GO TO (410,510,410,550), IFL	D3700
510 Y(1)=LIM(ISTEP)	D3710
IF (IFUNC,EQ.1) GO TO 530	D3720
IF (INT,EQ.0) GO TO 530	D3730
DO 520 I=1,2	D3740
ISUM(I,1)=ISUM(I,1)+0.5*L1*(HSUM(I,1,1)+HSUM(I,2,1))	D3750
520 HSUM(I,1,1)=HSUM(I,2,1)	D3760
INT=0	D3770
GO TO 530	D3780
530 ISTEP=ISTEP+1	D3790
IF (ISTEP,GT.3) GO TO 540	D3800
IF (CABS(Y(1)-LIM(ISTEP)).LT.1.E-10) GO TO 510	D3810
IFL=1	D3820
GO TO 410	D3830
C	D3840
C	D3850
C	D3860
540 PP=Y(2)	D3870
DPP=Y(3)	D3880
GO TO 580	D3890
550 Y(1)=LIM(ISTEP)	D3900
IF (IFUNC,EQ.1) GO TO 570	D3910
IF (INT,EQ.0) GO TO 570	D3920
DO 560 I=1,2	D3930
ISUM(I,2)=ISUM(I,2)+0.5*L1*(HSUM(I,1,2)+HSUM(I,2,2))	D3940
560 HSUM(I,1,2)=HSUM(I,2,2)	D3950
INT=0	D3960
570 ISTEP=ISTEP+1	D3970
IF (ISTEP,GT.6) GO TO 600	D3980
IF (CABS(Y(1)-LIM(ISTEP)).LT.1.E-20) GO TO 550	D3990
IFL=3	D4000
GO TO 410	D4010
C	D4020
C	D4030
C	D4040
580 Y(1)=CMPLX(YMAX,0.)	D4050
LAMDAP=CSQRT(MACH2*OMEGA*OMEGA-ALPHA*ALPHA)	D4060
IF (AIMAG(LAMDAP).GT.0.) GO TO 590	D4070
LAMDAP=-LAMDAP	D4080
590 ARG=LAMDAP*Y(1)	D4090
CALL NCBRTS (ARG,H01,H02,NORD,1)	D4100S
CALL NCBRTS (ARG,H11,H12,NORD1,1)	D4110S

Y(2)=H01	D4120
Y(3)=AN*H01/YMAX=LAMDAP*H11	D4130
IFL=3	D4140
IF (IFUNC.EQ.1) GO TO 410	D4150
MSUM(1,1,2)=(0.,0.)	D4160
MSUM(2,1,2)=2.*ALPHA*Y(1)*Y(2)*Y(2)/OMEGA/OMEGA	D4170
ISUM(1,2)=(0.,0.)	D4180
ISUM(2,2)=-ALPHA*Y(1)*Y(1)*(H01*H01+H11*H11-2.*AN*H01*H11/LAMDAP/Y	D4190
1(1))/OMEGA/OMEGA	D4200
INT=0	D4210
K=2	D4220
GO TO 410	D4230
C	D4240
C	D4250
C	D4260
600 BB4=Y(3)*PP-Y(2)*DpP	D4270
AC=Y(2)/PP	D4280
IF (IFUNC.EQ.1) GO TO 620	D4290
IF (IFLG.EQ.0) GO TO 610	D4300
WRITE (6,810) AC	D4310*
C	D4320
C	D4330
C	D4340
610 ISUM(1,1)=AC*AC*ISUM(1,1)+ISUM(1,2)	D4350
ISUM(2,1)=AC*AC*ISUM(2,1)+ISUM(2,2)	D4360
DKDB=-ISUM(1,1)/ISUM(2,1)	D4370
IF (IFLG.EQ.0) GO TO 10	D4380
WRITE (6,820) DKDB	D4390*
GO TO 10	D4400
620 BB(KK)=BB4	D4410
IF (IFLG.EQ.0) GO TO 630	D4420
WRITE (6,770) IND,ACON(KK),BB(KK)	D4430*
630 IF (KK.LT.NT) GO TO 240	D4440
C	D4450
C	D4460
C	D4470
CALL LAGRAN (KK,ACON,ALPHA,BB)	D4480*
IF (NTT.EQ.0) ALPHA=CMPLX(REAL(ALPHA),-ABS(AIMAG(ALPHA)))	D4490
ACON(KK+1)=ALPHA	D4500
IF (ABS(REAL(ACON(KK+1))).LT.1.E-5) GO TO 640	D4510
IF (ABS(1.-REAL(ACON(KK))/REAL(ACON(KK+1))).GT.0.005) GO TO 680	D4520
GO TO 650	D4530
640 WRITE (6,850)	D4540*
650 IF (ABS(AIMAG(ACON(KK+1))).LT.1.E-5) GO TO 660	D4550
IF (ABS(1.-AIMAG(ACON(KK))/AIMAG(ACON(KK+1))).GT.0.005) GO TO 680	D4560
GO TO 670	D4570
660 WRITE (6,860)	D4580*
GO TO 690	D4590
670 CONTINUE	D4600
GO TO 690	D4610
680 IF (KK.LT.15) GO TO 240	D4620
IEROR=1	D4630
RETURN	D4640
690 IF (IFLG.EQ.0) GO TO 700	D4650
WRITE (6,780) ALPHA	D4660*
700 NTT=NTT+1	D4670
ADAT(NTT)=ALPHA	D4680
SDAT(NTT)=S	D4690
CDAT(NTT)=AC	D4700

IFUNC=2	D4710
GO TO 240	D4720
710 CONTINUE	D4730
IF (IFLG.EQ.0) GO TO 730	D4740
WRITE (6,790) VJAO	D4750*
DO 720 I=1,NTT	D4760
720 WRITE (6,800) SDAT(I),ADAT(I),CDAT(I)	D4770*
730 CONTINUE	D4780
CALL DIRECT (ADAT,NTT,DS,TM,NANG,B0,GAMMA,INF,RADNF,XLAST,RSTART,P	D4790S
1THETA,PDB)	D4800
RETURN	D4810
C	D4820
740 FORMAT (1H1,10X,"INVISCID AXISYMMETRIC JET STABILITY CALCULATION"/	D4830
111X,"*****"/722X,"MODE N	D4840
2UMBER = ",I1//22X,"MACH NUMBER = ",F10.4//22X,"TEMPERATURE RATIO =	D4850
3 ",F10.4//22X,"STROUHAL NUMBER = ",F10.4//22X,"FREQUENCY = ",F10.4	D4860
4//22X,"THICKNESS = ",F10.4//)	D4870
750 FORMAT (22X,"POTENTIAL CORE RADIUS = ",F10.4//)	D4880
760 FORMAT (22X,"JET CENTERLINE VELOCITY = ",F10.4//)	D4890
770 FORMAT (1X,15.4X,"ALPHA = ",2E11.5,2X,"GIVES B4 = ",2E11.5/)	D4900
780 FORMAT (21X,"WAVENUMBER = ",2F14.9//)	D4910
790 FORMAT (1H1,30X,"MACHNO = ",F10.4///3X,"THICKNESS",15X,"ALPHA",25X	D4920
1,"C"//)	D4930
800 FORMAT (1X,E11.5,4(2E11.5))	D4940
810 FORMAT (30X,"C = ",2F14.9/)	D4950
820 FORMAT (25X,"DK/DS = ",2E12.5//)	D4960
830 FORMAT (1X,"BETA1 = ",F10.5,5X,"BETA2 = ",F10.5//)	D4970
840 FORMAT (1X,4(1X,2E14.7))	D4980
850 FORMAT (1X,"REAL PART OF ALPHA TOO SMALL FOR CONVERGENCE TEST"/)	D4990
860 FORMAT (1X,"IMAGINARY PART OF ALPHA TOO SMALL FOR CONVERGENCE ", "T	D5000
EST, ITERATIONS COMPLETED"/)	D5010
END	D5020-

•DECK PJMRUN	
SUBROUTINE PJMRUN (M,H,Y,DY,P,Q,ERRES)	E 10
COMPLEX Y(M),DY(M),P(M),Q(M),RR(8),H	E 20
DO 10 I=1,M	E 30
10 Q(I)=(0.,0.)	E 40
DY(I)=(1.,0.)	E 50
DO 20 I=2,M	E 60
20 DY(I)=(0.,0.)	E 70
CALL DERY (M,Y,DY)	E 80S
DO 30 I=1,M	E 90
P(I)=H*DY(I)*0.5	E 100
RR(I)=(P(I)-Q(I)+Y(I))-Y(I)	E 110
Y(I)=Y(I)+RR(I)	E 120
30 Q(I)=(3.*Q(I))-P(I)+3.*RR(I)	E 130
CALL DERY (M,Y,DY)	E 140S
DO 40 I=1,M	E 150
P(I)=H*DY(I)	E 160
RR(I)=((P(I)-Q(I))*0.5+Y(I))-Y(I)	E 170
Y(I)=Y(I)+RR(I)	E 180
40 Q(I)=(3.*P(I))-(2.*Q(I))-(6.*RR(I))	E 190
CALL DERY (M,Y,DY)	E 200S
ERRES=0.	E 210
DO 60 I=1,M	E 220
IF (CABS(P(I)-Q(I)).LT.1.E-20) GO TO 50	E 230
E=CABS(((H*DY(I))-P(I))/(P(I)-Q(I)))	E 240
IF (E.GT.ERRES) ERRES=E	E 250
50 P(I)=H*DY(I)-0.5*P(I)	E 260
RR(I)=(P(I)+Y(I))-Y(I)	E 270
Y(I)=Y(I)+RR(I)	E 280
60 Q(I)=Q(I)+6.*(P(I)-RR(I))	E 290
CALL DERY (M,Y,DY)	E 300S
DO 70 I=1,M	E 310
P(I)=(-4.*P(I)+H*DY(I)+Q(I))/6.	E 320
RR(I)=(P(I)+Y(I))-Y(I)	E 330
Y(I)=Y(I)+RR(I)	E 340
70 Q(I)=RR(I)-P(I)	E 350
RETURN	E 360
END	E 370-

•DECK DERY	
SUBROUTINE DERY (M,Y,DY)	F 10
COMPLEX Y(M),DY(M),ALPHA,UVAL,DUVAL,RHO,DRHO	F 20
COMPLEX DUDS,D2UDRS,DRDS,D2RDRS,DUM	F 30
COMPLEX DKDB	F 40
REAL MACH2	F 50
COMMON/INFO/ALPHA,OMEGA,MACH2,TJT0,NORD,GM1,DKDB,IFLG,VJA0	F 60
COMMON/SPR/HTHETA,S,KEY1,UCENT,DUCDS,BETA1,BETA2,IFUNC	F 70
AN=NORD	F 80
CALL UEVAL (Y(1),UVAL,DUVAL,DUDS,D2UDRS,RHO,DRHO,DRDS,D2RDRS)	F 90
DUM=ALPHA*UVAL-OMEGA	F 100
DY(2)=Y(3)	F 110
DY(3)=(DRHO/RHO+2.*ALPHA*DUVAL/DUM-1./Y(1))*Y(3)+(ALPHA*ALPHA-MACH	F 120
12*DUM*DUM*RHO*AN*AN/Y(1)/Y(1))*Y(2)	F 130
RETURN	F 140
END	F 150-

*DECK	UEVAL		
	SUBROUTINE UEVAL (X,U,DUDR,DUDS,D2UDRS,R,DRDR,DRDS,D2RDRS)	G	10
	COMPLEX X,U,DUDR,DUDS,D2UDRS,R,DRDR,DRDS,D2RDRS	G	20
	COMPLEX ALPHA,ETA,DRDU,D2RDU2	G	30
	COMPLEX DKDB,D2UDR2	G	40
	REAL MACH2	G	50
	COMMON/INFO/ALPHA,OMEGA,MACH2,TJT0,NORD,GM1,DKDB,IFLG,VJA0	G	60
	COMMON/SPR/HTHETA,S,KEY1,UCENT,UCDS,BETA1,BETA2,IFUNC	G	70
	A=.693147	G	80
	GO TO (10,40,60,60), KEY1	G	90
C		G	100
C	IF KEY1 = 1 WE CALCULATE UVAL IN THE ANNULAR MIXING	G	110
C	REGION FOR A GIVEN VALUE OF RADIUS, X.	G	120
C		G	130
	10 IF (REAL(X),LT,HTHETA) GO TO 70	G	140
	ETA=(X-HTHETA)/S	G	150
	U=CEXP(-A*ETA*ETA)	G	160
	DUDR=-2.*A*ETA*U/S	G	170
	20 R=1./(1.+(TJT0-1.)*U+0.5*GM1*MACH2*U*(1.-U))	G	180
	IF (KEY1,EQ,3) GO TO 80	G	190
	DRDU=-R*R*(TJT0-1.+0.5*GM1*MACH2*(1.-2.*U))	G	200
	DRDR=DRDU*DUDR	G	210
	IF (IFUNC,EQ,1) GO TO 80	G	220
	D2UDR2=(4.*A*A*ETA*ETA-2.*A)*U/S/S	G	230
	IF (KEY1,EQ,2) GO TO 50	G	240
	DHDS=-TJT0*(HTHETA*BETA1+2.*BETA2*S)/(HTHETA+TJT0*BETA1*S)	G	250
	DUDS=-DUDR*(ETA+DHDS)	G	260
	D2UDRS=-D2UDR2*(ETA+DHDS)-DUDR/S	G	270
	30 DRDS=DRDU*DUDS	G	280
	D2RDU2=2.*DRDU*DRDU/R+GM1*MACH2*R*R	G	290
	D2RDRS=D2RDU2*DUDR+DUDS*DRDU+D2UDRS	G	300
	RETURN	G	310
C		G	320
C	IF KEY1 = 2 WE CALCULATE UVAL IN THE DEVELOPED JET	G	330
C	FLOW FOR A GIVEN VALUE OF RADIUS, X.	G	340
C		G	350
	40 ETA=X/S	G	360
	U=UCENT*CEXP(-A*ETA*ETA)	G	370
	DUDR=-2.*A*ETA*U/S	G	380
	GO TO 20	G	390
	50 DUDS=DUCDS*U/UCENT-ETA*DUDR	G	400
	D2UDRS=(DUCDS/UCENT-1./S)*DUDR-ETA*D2UDR2	G	410
	GO TO 30	G	420
C		G	430
C	IF KEY1 = 3 WE CALCULATE THE VALUE OF UVAL FOR A GIVEN	G	440
C	VALUE OF ETA=X.	G	450
C		G	460
	60 ETA=X	G	470
	U=CEXP(-A*ETA*ETA)	G	480
	DUDR=-2.*A*ETA*U	G	490
	IF (KEY1,EQ,4) GO TO 90	G	500
	GO TO 20	G	510
	70 U=(1.,0.)	G	520
	DUDR=(0.,0.)	G	530
	R=1./TJT0	G	540
	DRDR=(0.,0.)	G	550
	80 DUDS=(0.,0.)	G	560
	D2UDRS=(0.,0.)	G	570
	DRDS=(0.,0.)	G	580
	D2RDRS=(0.,0.)	G	590
	RETURN	G	600
	90 R=1./(1.+(TJT0-1.)*U+0.5*GM1*MACH2*U*UCENT*(1.-U*UCENT))	G	610
	RETURN	G	620
	END	G	630-

*DECK LAGRAN	
SUBROUTINE LAGRAN (NUM,C,CVAL,B4)	H 10
COMPLEX C(10),B4(10),CVAL,CONT,CMIN	H 20
DO 20 JJ=1,2	H 30
N=NUM-JJ	H 40
CMIN=B4(N)	H 50
JN=N	H 60
DO 10 I=1,N	H 70
K=NUM-I-JJ+1	H 80
IF (CABS(CMIN).LE.CABS(B4(K))) GO TO 10	H 90
JN=K	H 100
CMIN=B4(K)	H 110
10 CONTINUE	H 120
IF (JN.EQ.N) GO TO 20	H 130
B4(JN)=B4(N)	H 140
B4(N)=CMIN	H 150
CMIN=C(N)	H 160
C(N)=C(JN)	H 170
C(JN)=CMIN	H 180
20 CONTINUE	H 190
CVAL=(0.,0.)	H 200
DO 40 J=N,NUM	H 210
CONT=(1.,0.)	H 220
DO 30 I=N,NUM	H 230
IF (I.EQ.J) GO TO 30	H 240
CONT=CONT*(B4(I)/(B4(J)-B4(I)))	H 250
30 CONTINUE	H 260
40 CVAL=CVAL+C(J)*CONT	H 270
RETURN	H 280
END	H 290-

*DECK NCBRTS	I 10
SUBROUTINE NCBRTS (Z,B1,B2,N,M)	I 20
COMPLEX Z,M1(50),M2(50),B1,B2	I 30
IF (M.EQ.0) GO TO 20	I 40
IF (N.EQ.0.OR.N.EQ.1) GO TO 20	I 50\$
CALL CBRTS (Z,M1(1),M2(1),0,1)	I 60\$
CALL CBRTS (Z,M1(2),M2(2),1,1)	I 70
NP1=N+1	I 80
DO 10 J=3,NP1	I 90
M1(J)=2.*(J-2)*M1(J-1)/Z-M1(J-2)	I 100
10 M2(J)=2.*(J-2)*M2(J-1)/Z-M2(J-2)	I 110
B1=M1(NP1)	I 120
B2=M2(NP1)	I 130
RETURN	I 140\$
20 CALL CBRTS (Z,B1,B2,N,M)	I 150
RETURN	I 160-
END	

•DECK CBRTS	
SUBROUTINE CBRTS (Z,H1,H2,N,M)	J 10
DIMENSION AJ(1000)	J 20
COMPLEX Z,CON,F2,SUM,AJN,AYN,FCT,PCD,H1,H2	J 30
AN=N	J 40
R=CABS(Z)	J 50
IF (R.GT.6.6) GO TO 60	J 60
IF (R.GE..1E-30) GO TO 10	J 70
THETA=0.	J 80
GO TO 20	J 90
10 THETA=ATAN2(AIMAG(Z),REAL(Z))	J 100
20 CONTINUE	J 110
THN=AN*THETA	J 120
CON=CMPLX(COS(THN),SIN(THN))	J 130
F1=-1.	J 140
F2=CMPLX((COS(2.*THETA)-1.),SIN(2.*THETA))	J 150
F3=R/2.	J 160
FAC=1.	J 170
LIM=29-N	J 180
CALL BSSLS (R,AJ,29,IERR)	J 190S
SUM=CMPLX(AJ(N+1),0.)	J 200
PCD=F1*F2*F3	J 210
FCT=(1.,0.)	J 220
DO 30 K=1,LIM	J 230
L=N+K-1	J 240
FAC=K*FAC	J 250
FCT=FCT*PCD	J 260
AJ(L)=AJ(L)/FAC	J 270
30 SUM=SUM+FCT*AJ(L)	J 280
IN=LIM+1	J 290
KN=LIM+1	J 300
DO 40 I=IN,KN	J 310
FAC=I*FAC	J 320
L=I+N	J 330
CALL BELS (R,Y,L)	J 340S
FCT=FCT*PCD	J 350
Y=Y/FAC	J 360
40 SUM=SUM+FCT*Y	J 370
AJN=CON*SUM	J 380
CALL BELZ (Z,AJN,AYN,N)	J 390S
IF (M.NE.0) GO TO 50	J 400
H1=AJN	J 410
H2=AYN	J 420
RETURN	J 430
50 H1=AJN*(0.,1.)*AYN	J 440
H2=AJN*(0.,1.)*AYN	J 450
RETURN	J 460
60 CONTINUE	J 470
CALL HAN (Z,H1,H2,N)	J 480S
IF (M.NE.0) GO TO 70	J 490
H1=(H1+H2)/2.	J 500
H2=(0.,-.5)*(H1-H2)	J 510
70 RETURN	J 520
END	J 530-

•DECK BSSLS	
SUBROUTINE BSSLS (X,F,N,IERR)	K 10
DIMENSION F(1)	K 20
IERR=0	K 30
NMAX=30	K 40
IF (N,LE,NMAX) GO TO 10	K 50
IERR=1	K 60
RETURN	K 70
10 MX=X	K 80
NPP=3*MX+12+10*(IABS(N-1)/10)	K 90
IF (IFIX(X).GT.N) NPP=IFIX(3.*X+12.)	K 100
IF (MOD(NPP,2).EQ.0) NPP=NPP+1	K 110
DO 20 I=1,NPP	K 120
20 F(I)=0.	K 130
IF (X,GE,.1E-34) GO TO 30	K 140
F(1)=1.	K 150
RETURN	K 160
30 IF (X,GE,.14E0) GO TO 80	K 170
Z=X/2.	K 180
F(1)=1.	K 190
LPP=NPP-1	K 200
DO 40 K=1,LPP	K 210
40 F(K+1)=F(K)*Z	K 220
FAC2=-Z*Z	K 230
FAC1=1.	K 240
DO 70 I=1,NPP	K 250
NORD=I-1	K 260
IF (I,EQ,1) GO TO 50	K 270
FAC1=FAC1/FLOAT(NORD)	K 280
50 VAL=FAC1	K 290
SUM=FAC1	K 300
DO 60 J=2,20	K 310
L=J+NORD-1	K 320
K=J-1	K 330
VAL=VAL*FAC2/FLOAT(L*K)	K 340
IF (ABS(VAL).LT.1.E-20) GO TO 70	K 350
60 SUM=SUM+VAL	K 360
70 F(I)=F(I)*SUM	K 370
RETURN	K 380
80 NP=NPP+1	K 390
NPR=NPP-1	K 400
F(NP-1)=.1E-34	K 410
F(NP)=0.	K 420
DO 90 I=1,NPR	K 430
NP=NPP-I	K 440
XN=NP	K 450
90 F(NP)=2.*XN/X*F(NP+1)-F(NP+2)	K 460
XN=F(1)	K 470
DO 100 I=3,NPP,2	K 480
100 XN=2.*F(I)+XN	K 490
XN=1./XN	K 500
DO 110 I=1,NPP	K 510
F(I)=XN*F(I)	K 520
110 CONTINUE	K 530
RETURN	K 540
END	K 550-

*DECK BELS	L 10
SUBROUTINE BELS (X,Y,N)	L 20
AN=N	L 30
FN=1.	L 40
DO 10 I=1,N	L 50
AI=I	L 60
10 FN=FN*AI	L 70
C=(.5*X)**2	L 80
CN=(.5*X)**N/FN	L 90
F=C/(AN+1.)	L 100
AJ=2.	L 110
D=1.	L 120
FN1=1.-F	L 130
20 F=F*C/((AN+AJ)*AJ)	L 140
FN1=FN1+D*F	L 150
AJ=AJ+1.	L 160
D=-D	L 170
IF (ABS(F/FN1)-1.E-10) 30,30,20	L 180
30 Y=FN1*CN	L 190
RETURN	L 200
END	

•DECK BELZ	
SUBROUTINE BELZ (X,Y,XY,N)	M 10
COMPLEX X,Y,XY,SM,CXF,CCN,CC,CF,CFN1,CFN3,CHA,XI	M 20
CHA=(.5,0.)	M 30
AN=N	M 40
IF (CABS(X).GE..1E-30) GO TO 10	M 50
PH=0.	M 60
GO TO 20	M 70
10 PH=ATAN2(AIMAG(X),REAL(X))	M 80
20 CONTINUE	M 90
XI=(0.,1.)	M 100
R=CABS(X)	M 110
FN=1.	M 120
FM=0.	M 130
FQ=0.	M 140
SM=(0.,0.)	M 150
IF (N) 30,60,30	M 160
30 DO 40 I=1,N	M 170
AI=I	M 180
FM=FM+1./AI	M 190
40 FN=FN*AI	M 200
CXF=CHA*CHA*X*X	M 210
CCN=(CHA*X)**(-N)/FN	M 220
FS=FN/AN	M 230
GS=1.	M 240
DO 50 I=1,N	M 250
AI=I	M 260
SM=SM+CCN*FS/GS	M 270
CCN=CCN*CXF	M 280
GS=GS*AI	M 290
IF (N.EQ.I) GO TO 50	M 300
FS=FS/(AN-AI)	M 310
50 CONTINUE	M 320
60 CC=CHA*CHA*X*X	M 330
CCN=(CHA*X)**N	M 340
CCN=CCN/FN	M 350
CF=CC/(AN+1.)	M 360
AJ=2.	M 370
D=1.	M 380
CFN1=1.-CF	M 390
CFN3=CMPLX(FM,0.)	M 400
FQ=FQ+1./(AJ-1.)	M 410
FM=FM+1./(AN+AJ-1.)	M 420
FP=FM+FQ	M 430
CFN3=CFN3-CF*FP	M 440
70 CF=CF*CC/((AN+AJ)*AJ)	M 450
CFN1=CFN1+D*CF	M 460
FQ=FQ+1./AJ	M 470
FM=FM+1./(AN+AJ)	M 480
FP=FM+FQ	M 490
CFN3=CFN3+D*CF*FP	M 500
AJ=AJ+1.	M 510
D=-D	M 520
IF (CABS(CF/CFN1)-1.E-10) 80,80,70	M 530
80 XY=(2.*(1.5772156649*(ALOG(R/2.)*XI*PH))*Y-SM-CFN3*CCN)/3.141592653	M 540
159	M 550
RETURN	M 560
END	M 570-

*DECK HAN	N 10
SUBROUTINE HAN (Z,H1,H2,N)	N 20
COMPLEX Z,H1,H2,SETI,SP,X,CP,CP1	N 30
PI=3.14159265359	N 40
AN=N	N 50
IF (CABS(Z).GE..1E-30) GO TO 10	N 60
PH=0.	N 70
GO TO 20	N 80
10 PH=ATAN2(AIMAG(Z),REAL(Z))	N 90
20 CONTINUE	N 100
R=CABS(Z)	N 110
S1=EXP(-1.*AIMAG(Z))/SQRT(.5*PI*R)	N 120
SIGMA1=2.*REAL(Z)/PI-AN-.5-PH/PI	N 130
SETI=CEXP(.5*(0.,1.)*PI*SIGMA1)	N 140
SP=(1.,0.)	N 150
CP=SP	N 160
CP1=CP	N 170
X=-2.*Z*(0.,1.)	N 180
C1=1.	N 190
30 CP=CP*(4.*AN*AN-C1*C1)/(C1*4.*X)	N 200
C1=C1+2.	N 210
SP=SP*CP	N 220
IF (CABS(CP)-CABS(CP1)) 40,50,50	N 230
40 CP1=CP	N 240
GO TO 30	N 250
50 SP=SP-CP	N 260
H1=S1*SETI*SP	N 270
S1=EXP(AIMAG(Z))/SQRT(.5*PI*R)	N 280
SIGMA1=-2.*REAL(Z)/PI-AN+.5-PH/PI	N 290
SETI=CEXP(.5*(0.,1.)*PI*SIGMA1)	N 300
SP=(1.,0.)	N 310
X=2.*Z*(0.,1.)	N 320
CP=SP	N 330
CP1=CP	N 340
C1=1.	N 350
60 CP=CP*(4.*AN*AN-C1*C1)/(C1*4.*X)	N 360
C1=C1+2.	N 370
SP=SP*CP	N 380
IF (CABS(CP)-CABS(CP1)) 70,80,80	N 390
70 CP1=CP	N 400
GO TO 60	N 410
80 SP=SP-CP	N 420
H2=S1*SETI*SP	N 430
RETURN	N 440-
END	

•DECK INTEG		
SUBROUTINE INTEG (H,SUM,L1,L2)	0	10
COMPLEX H(3),SUM,L1,L2	0	20
SUM=SUM+(L1+L2)*(H(1)*L2*(2.*L1-L2)+H(2)*(L1+L2)**2+H(3)*L1*(2.*L2	0	30
I=L1)/L1/L2/6.	0	40
RETURN	0	50
END	0	60-

*DECK DIRECT		
SUBROUTINE DIRECT (ADAT,NTT,DB,TM,NANG,B0,GAMMA,INF,RADNF,XLAST,RS	P	10
1TART,PTHETA,PDB)	P	20
DIMENSION TM(NANG),PTHETA(NANG),PDB(NANG)	P	30
COMPLEX Y(4),DY(4),P(4),Q(4),XSAVE,PY(4)	P	40
COMPLEX ALPHA,DKDB,ADAT(1),AVAL,DUM	P	50
COMPLEX XVAL(1025),W(1025),W1(1025),BN(1025),CWAVE,CONT	P	60
COMPLEX H01,H02	P	70
REAL NFDB(1025,10)	P	80
INTEGER GAMMA	P	90
REAL MJ,MACH2,KAPPA,M20	P	100
COMMON/DATA/KAPPA,EPSI,POTB,IFLAG	P	110
COMMON/INFO/ALPHA,OMEGA,MACH2,TJT0,NORD,GM1,DKDB,IFLG,VJAO	P	120
ERMIN=0.1	P	130
ERMAX=0.14	P	140
PI=3.14159	P	150
FCT=57.2958	P	160
MJ=VJAO/SQRT(TJT0)	P	170
IF (MJ.GT.2.) GO TO 10	P	180
SIGMA=10.7/(1.-.1163*MJ*MJ)	P	190
GO TO 20	P	200
10 SIGMA=19.4*SQRT(MJ-.0,9418)	P	210
20 EPSI=1.2658/SIGMA	P	220
DELX=0.5/OMEGA	P	230
IF (IFLG.EQ.0) GO TO 30	P	240
WRITE (6,680) NORD,VJAO,TJT0,EPSI,GAMMA	P	250*
C	P	260
C CALCULATION OF WIDTH AT END OF POTENTIAL CORE	P	270
C	P	280
30 M20=MACH2*OMEGA*OMEGA	P	290
A=0.2*MACH2	P	300
B=(1.-TJT0-A)	P	310
IF (A.LT.1.E-10) GO TO 40	P	320
AK=SQRT(B*B+4.*A)	P	330
POTB=-1.38629*A/(ALOG(ABS(A+B-1.))-B*ALOG(ABS((2.*A+B-AK)*(B-AK)/(P	340
12.*A+B-AK)/(B-AK))))/AK)/TJT0	P	350
POTB=SQRT(POTB)	P	360
GO TO 60	P	370
40 IF (ABS(B).LT.1.E-10) GO TO 50	P	380
POTB=-.693147*B*B/(B*ALOG(ABS(1.-B)))/TJT0	P	390
POTB=SQRT(POTB)	P	400
GO TO 70	P	410
50 POTB=1.17741	P	420
GO TO 80	P	430
C	P	440
C CALCULATION OF THE EDDY VISCOSITY CONSTANT	P	450
C	P	460
60 RHOB=1./(1.-0.5*B-0.25*A)	P	470
KAPPA=(1./A-1/(B-A)*ALOG(ABS(A+B-1.))-(B*B+2.*A*A*B)*ALOG(ABS((2.*A	P	480
1+B-AK)*(B-AK)/(2.*A+B-AK)/(B-AK)))/AK)/2./A/A)*2.88539/RHOB	P	490
GO TO 90	P	500
70 RHOB=1./(1.-0.5*B)	P	510
KAPPA=(0.5*TJT0*ALOG(TJT0)/B/B)*2.88539/B/RHOB	P	520
GO TO 90	P	530
80 KAPPA=POTB/2.07944	P	540
90 IFLAG=1	P	550
C	P	560
C CALCULATION OF STARTING CONDITIONS	P	570
C	P	580

	Y(1)=(0.,0.)	P 590
	Y(2)=80	P 600
	Y(3)=(1.,0.)	P 610
	Y(4)=(1.,0.)	P 620
	B=REAL(Y(2))	P 630
	UC=REAL(Y(3))	P 640
	X=REAL(Y(1))	P 650
	DBDX=EPSI	P 660
C		P 670
C	CALCULATE INTEGRAND FOR FOURIER TRANSFORM	P 680
C		P 690
	XVAL(1)=Y(4)	P 700
	IF (NORD.EQ.0) GO TO 110	P 710
	CALL COEFF (ADAT,NTT,B,AVAL,DB)	P 720
	DUM=CSQRT(MACH2*OMEGA*OMEGA-AVAL*AVAL)	P 730
	IF (AIMAG(DUM).GT.0.) GO TO 100	P 740
	DUM=-DUM	P 750
100	DUM=DUM**NORD	P 760
	XVAL(1)=XVAL(1)/DUM	P 770
110	CONTINUE	P 780
	AMP=CABS(XVAL(1))	P 790
	IF (ABS(AIMAG(XVAL(1))).LT.1.E-20) GO TO 120	P 800
	IF (ABS(REAL(XVAL(1))).LT.1.E-20) GO TO 130	P 810
	PHASE=ATAN2(AIMAG(XVAL(1)),REAL(XVAL(1)))*FCT	P 820
	GO TO 140	P 830
120	PHASE=0.	P 840
130	PHASE=90.*SIGN(1.,AIMAG(XVAL(1)))	P 850
140	IF (IFLG.EQ.0) GO TO 150	P 860
	WRITE (6,690) X,B,DBDX,UC,XVAL(1),AMP,PHASE	P 870
C		P 880
C	BEGIN INTEGRATION	P 890
C		P 900
150	N=2**GAMMA	P 910
	ISTEP=1	P 920
	H=DELX	P 930
	SMAX=H	P 940
	SMIN=H/1000.	P 950
	XSAVE=Y(1)	P 960
160	IFL=1	P 970
	XSTOP=REAL(XSAVE)*DELX	P 980
	ISTEP=ISTEP+1	P 990
	IF (ISTEP.GE.(N+2)) GO TO 310	P1000
170	DO 180 I=1,4	P1010
180	PY(I)=Y(I)	P1020
190	IF (H.LT.SMIN) H=SMIN	P1030
	IF (H.GT.SMAX) H=SMAX	P1040
	IF (CABS(Y(1)-XSTOP).GT.H) GO TO 200	P1050
	H=CABS(Y(1)-XSTOP)	P1060
	IFL=2	P1070
200	CALL RUNREL (4,H,Y,DY,P,0,ERRES,ADAT,NTT,DB)	P1080
	IND=IND+1	P1090
	IF (ERRES.LT.ERMIN) GO TO 230	P1100
	IF (ERRES.LT.ERMAX) GO TO 240	P1110
	IF (H.LE.SMIN) GO TO 220	P1120
	H=0.8*H	P1130
	DO 210 I=1,4	P1140
210	Y(I)=PY(I)	P1150
	IFL=1	P1160
	GO TO 190	P1170

220	IWR=1	P1180
	GO TO 240	P1190
230	M=1.25*M	P1200
240	IF (IFL.EQ.1) GO TO 170	P1210
	X=REAL(Y(1))	P1220
	B=REAL(Y(2))	P1230
	UC=REAL(Y(3))	P1240
	DBDX=REAL(DY(2))	P1250
C		P1260
C	CALCULATE INTEGRAND FOR FOURIER TRANSFORM	P1270
C		P1280
	XVAL(ISTEP)=Y(4)	P1290
	IF (NORD.EQ.0) GO TO 260	P1300
	CALL COEFF (ADAT,NIT,B,AVAL,DB)	P1310S
	DUM=CSQRT(MACH2*OMEGA*OMEGA-AVAL*AVAL)	P1320
	IF (AIMAG(DUM).GT.0.) GO TO 250	P1330
	DUM=-DUM	P1340
250	DUM=CSQRT(DUM)	P1350
	XVAL(ISTEP)=XVAL(ISTEP)/DUM	P1360
260	CONTINUE	P1370
	AMP=CABS(XVAL(ISTEP))	P1380
	IF (ABS(AIMAG(XVAL(ISTEP))).LT.1.E-20) GO TO 270	P1390
	IF (ABS(REAL(XVAL(ISTEP))).LT.1.E-20) GO TO 280	P1400
	PHASE=ATAN2(AIMAG(XVAL(ISTEP)),REAL(XVAL(ISTEP)))*FCT	P1410
	GO TO 290	P1420
270	PHASE=0.	P1430
	GO TO 290	P1440
280	PHASE=90.*SIGN(1.,AIMAG(XVAL(ISTEP)))	P1450
290	IF (IFLG.EQ.0) GO TO 300	P1460
	WRITE (6,690) X,B,DBDX,UC,XVAL(ISTEP),AMP,PHASE	P1470*
300	XSAVE=Y(1)	P1480
	GO TO 160	P1490
310	IF (IFLG.EQ.0) GO TO 320	P1500
	WRITE (6,700) IWR,IND	P1510*
C		P1520
C	PERFORM FOURIER TRANSFORM	P1530
C		P1540
320	IGAM=GAMMA+1	P1550
	INUM=2**IGAM	P1560
	N1=N+1	P1570
	N2=N+2	P1580
	DO 360 I=N2,INUM	P1590
	J=I-INUM-1	P1600
	X=FLOAT(J)*DEL X	P1610
	DUM=(0.,1.)*ADAT(1)*X	P1620
	IF (CABS(DUM).GT.30.) GO TO 330	P1630
	XVAL(I)=XVAL(I)*CEXP(DUM)	P1640
	GO TO 340	P1650
330	XVAL(I)=(0.,0.)	P1660
340	IF (NORD.EQ.0) GO TO 360	P1670
	DUM=CSQRT(M20-ADAT(1)*ADAT(1))	P1680
	IF (AIMAG(DUM).GT.0.) GO TO 350	P1690
	DUM=-DUM	P1700
350	DUM=DUM**NORD	P1710
	XVAL(I)=XVAL(I)/DUM	P1720
360	CONTINUE	P1730
	CALL FFT (IGAM,INUM,XVAL,W)	P1740S
	DO 370 I=1,INUM	P1750
370	XVAL(I)=XVAL(I)*DEL X/2./PI	P1760

	DELW=2.*PI/DELX/INUM	P1770
	IF (IFLG.EQ.0) GO TO 380	P1780
	WRITE (6,710)	P1790*
C		P1800
C	CALCULATION OF B(K)	P1810
C		P1820
380	DO 440 I=1,INUM	P1830
	IF (I.GE.N) GO TO 390	P1840
	KK=I-N1	P1850
	W(KK)=DELW*(I-N)	P1860
	GO TO 400	P1870
390	KK=I-N+1	P1880
	W(KK)=DELW*(I-N)	P1890
400	BN(KK)=XVAL(KK)	P1900
	AMP=CABS(BN(KK))	P1910
	IF (ABS(AIMAG(BN(KK))).LT.1.E-20) GO TO 410	P1920
	IF (ABS(REAL(BN(KK))).LT.1.E-20) GO TO 420	P1930
	PHASE=ATAN2(AIMAG(BN(KK)),REAL(BN(KK)))*FCT	P1940
	GO TO 430	P1950
410	PHASE=0.	P1960
	GO TO 430	P1970
420	PHASE=90.*SIGN(1.,AIMAG(BN(KK)))	P1980
430	WAVEN=REAL(W(KK))	P1990
	IF (IFLG.EQ.0) GO TO 440	P2000
	WRITE (6,720) WAVEN,BN(KK),AMP,PHASE	P2010*
440	CONTINUE	P2020
	INP1=INUM+1	P2030
	XVAL(INP1)=XVAL(1)	P2040
	W(INP1)=W(1)	P2050
	BN(INP1)=BN(1)	P2060
C		P2070
C	CALCULATION OF FAR FIELD DIRECTIVITY PATTERN	P2080
C		P2090
	IF (IFLG.EQ.0) GO TO 450	P2100
	WRITE (6,730)	P2110*
450	DO 550 M=1,NANG	P2120
	ANGLE=TM(M)/FCT	P2130
	COST=COS(ANGLE)	P2140
	WAVEN=OMEGA*VJA0*COST	P2150
	IF (WAVEN.LT.0.) GO TO 460	P2160
	IVAL=IFIX(WAVEN/DELW-.001)+1	P2170
	IF (IVAL.LT.3) IVAL=3	P2180
	IF (IVAL.GT.(N-1)) IVAL=N-1	P2190
	GO TO 470	P2200
460	IVAL=IFIX(WAVEN/DELW-.001)+INP1	P2210
	IF (IVAL.LT.(N2+2)) IVAL=N2+2	P2220
	IF (IVAL.GT.(INP1-2)) IVAL=INP1-2	P2230
470	IM2=IVAL-2	P2240
	IP2=IVAL+2	P2250
	CWAVE=(0.,0.)	P2260
	DO 490 J=IM2,IP2	P2270
	CONT=(1.,0.)	P2280
	DO 480 KJ=IM2,IP2	P2290
	IF (J.EQ.KJ) GO TO 480	P2300
	CONT=CONT*(WAVEN-W(KJ))/(W(J)-W(KJ))	P2310
480	CONTINUE	P2320
490	CWAVE=CWAVE+BN(J)*CONT	P2330
	IF (NORD.EQ.0) GO TO 520	P2340
	IF (ABS(ANGLE).LT.1.E-20) GO TO 500	P2350

VAL=(SQRT(M20-WAVEN*WAVEN))*NORD	P2360
GO TO 510	P2370
500 VAL=0.	P2380
510 CWAVE=CWAVE*VAL	P2390
520 PTHETA(M)=2.*REAL(CWAVE*CONJG(CWAVE))	P2400
ANGLE=ANGLE*FCT	P2410
IF (PTHETA(M).LT.1.E-20) GO TO 530	P2420
PDB(M)=10.*ALOG10(PTHETA(M))	P2430
GO TO 540	P2440
530 PDB(M)=0.	P2450
540 IF (IFLG.EQ.0) GO TO 550	P2460
WRITE (6,740) ANGLE,PTHETA(M),PDB(M)	P2470*
550 CONTINUE	P2480
IF (INF.EQ.0) GO TO 670	P2490
C	P2500
C	P2510
C	P2520
IF (NORD.EQ.0) GO TO 580	P2530
DO 570 I=1,INUM	P2540
DUM=CSQRT(M20-W(I)*W(I))	P2550
IF (ABS(AIMAG(DUM)).LT.1.E-10) GO TO 560	P2560
IF (AIMAG(DUM).GT.0.) GO TO 570	P2570
DUM=-DUM	P2580
GO TO 570	P2590
560 IF (REAL(DUM).LT.0.) DUM=-DUM	P2600
570 BN(I)=BN(I)*DUM**NORD	P2610
580 DO 650 I=1,INF	P2620
RAD=RSTART*FLOAT(I)*RADNF	P2630
DO 610 J=1,INUM	P2640
DUM=CSQRT(M20-W(J)*W(J))	P2650
IF (ABS(AIMAG(DUM)).LT.1.E-10) GO TO 590	P2660
IF (AIMAG(DUM).GT.0.) GO TO 600	P2670
DUM=-DUM	P2680
GO TO 600	P2690
590 IF (REAL(DUM).LT.0.) DUM=-DUM	P2700
600 DUM=DUM*RAD	P2710
CALL NCBRTS (DUM,M01,M02,NORD,1)	P2720\$
610 XVAL(J)=BN(J)*M01	P2730
DO 620 J=1,INUM	P2740
620 XVAL(J)=XVAL(J)*SQRT(RAD)	P2750
CALL FFT (IGAM,INUM,XVAL,W1)	P2760\$
DO 630 J=1,INUM	P2770
630 XVAL(J)=XVAL(J)*DEWL	P2780
DO 640 J=2,N	P2790
K=J+N	P2800
640 NFDB(J,I)=10.*ALOG10(0.5*REAL(XVAL(K)*CONJG(XVAL(K)))/RAD)	P2810
650 NFDB(1,I)=10.*ALOG10(0.5*REAL(XVAL(1)*CONJG(XVAL(1)))/RAD)	P2820
WRITE (6,750) RADNF	P2830*
DO 660 J=1,N	P2840
K=N-J+2	P2850
IF (J.EQ.1) K=1	P2860
X=DEWL*FLOAT(J-1)	P2870
IF (X.GT.XLAST) GO TO 660	P2880
WRITE (6,760) X,(NFDB(K,I),I=1,INF)	P2890*
660 CONTINUE	P2900
670 RETURN	P2910
C	P2920
680 FORMAT (1H1,28X,"VARIATION OF FOURIER TRANSFORM INTEGRAND"/29X,40H	P2930
1*****//28X,"MODE NUMBER ",I1/2	P2940

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28X,"MACH NUMBER = ",F10.4/23X,"TEMPERATURE RATIO = ",F10.4/32X,"EP P2950
35ILON = ",F10.4/34X,"GAMMA " ,I2///4X,"AXIAL",3X,"THICKNESS", P2960
44X,"DBDX",3X,"CENTERLINE",2X,"FOURIER TRANSFORM",7X,"AMPLITUDE",2X P2970
5,"PHASE"/3X,"DISTANCE",22X,"VELOCITY",2X,"INTEGRAND, G(S)"/) P2980
690 FORMAT (1X,4F10.4,2E12.4,2X,2F10.4) P2990
700 FORMAT (/1X,"IWR = ",I1,2X,"IND = ",I5//) P3000
710 FORMAT (1H1,25X,"WAVENUMBER SPECTRUM, B(K)"/26X,25H***** P3010
1*****//1X,"WAVENUMBER",4X,"WAVENUMBER SPECTRUM",6X,"AMPLITUDE P3020
2",2X,"PHASE"/21X,"B(K)"/) P3030
720 FORMAT (1X,F10.4,2X,2E12.4,2X,2F10.4) P3040
730 FORMAT (1H1,20X,"FAR-FIELD DIRECTIVITY"/21X,21H***** P3050
1**//9X,"ANGLE",10X,"PTHETA",11X,"P DB"/) P3060
740 FORMAT (6X,F10.4,5X,E12.5,5X,F10.4) P3070
750 FORMAT (1H1,20X,"NEAR FIELD SOUND PRESSURE LEVEL CONTOURS"/21X,40H P3080
1*****//35X,"RADIAL SPACING = ", P3090
2F5.2," RADII"/) P3100
760 FORMAT (1X,F10.4,5X,13F8.2) P3110
END P3120-

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*DECK RUNREL	
SUBROUTINE RUNREL (M,H,Y,DY,P,Q,ERRES,ADAT,NTT,DB)	Q 10
COMPLEX Y(M),DY(M),P(M),Q(M),RR(4)	Q 20
COMPLEX ADAT(1)	Q 30
10 DO 20 I=1,M	Q 40
20 Q(I)=(0.,0.)	Q 50
DY(I)=(1.,0.)	Q 60
DO 30 I=2,M	Q 70
30 DY(I)=(0.,0.)	Q 80
CALL DERY1 (M,Y,DY,ADAT,NTT,DB)	Q 90\$
DO 40 I=1,M	Q 100
P(I)=H*DY(I)*.5	Q 110
RR(I)=(P(I)-Q(I)+Y(I))-Y(I)	Q 120
Y(I)=Y(I)+RR(I)	Q 130
40 Q(I)=(3.*Q(I))-P(I)+(3.*RR(I))	Q 140
CALL DERY1 (M,Y,DY,ADAT,NTT,DB)	Q 150\$
DO 50 I=1,M	Q 160
P(I)=H*DY(I)	Q 170
RR(I)=((P(I)-Q(I))*5+Y(I))-Y(I)	Q 180
Y(I)=Y(I)+RR(I)	Q 190
50 Q(I)=(3.*P(I))-(2.*Q(I))-(6.*RR(I))	Q 200
CALL DERY1 (M,Y,DY,ADAT,NTT,DB)	Q 210\$
ERRES=0.	Q 220
DO 70 I=1,M	Q 230
IF (CABS(P(I)-Q(I)).LT.1.E-20) GO TO 60	Q 240
E=CABS((H*DY(I))-P(I))/(P(I)-Q(I))	Q 250
IF (E.GT.ERRES) ERRES=E	Q 260
60 P(I)=H*DY(I)-.5*P(I)	Q 270
RR(I)=(P(I)+Y(I))-Y(I)	Q 280
Y(I)=Y(I)+RR(I)	Q 290
70 Q(I)=Q(I)+6.*(P(I)-RR(I))	Q 300
CALL DERY1 (M,Y,DY,ADAT,NTT,DB)	Q 310\$
DO 80 I=1,M	Q 320
P(I)=(-4.*P(I)+H*DY(I)+Q(I))/6.	Q 330
RR(I)=(P(I)+Y(I))-Y(I)	Q 340
Y(I)=Y(I)+RR(I)	Q 350
80 Q(I)=RR(I)-P(I)	Q 360
RETURN	Q 370
END	Q 380-

*DECK DERY1		R	10
SUBROUTINE DERY1 (M,Y,DY,ADAT,NTT,DB)		R	20
COMPLEX Y(M),DY(M),ADAT(NTT),AVAL		R	30
COMPLEX ALPHA,DKDB		R	40
COMPLEX YPEAK,APEAK,X0		R	50
REAL KAPPA,KAPB,MACH2,VJAO		R	60
COMMON/DATA/KAPPA,EPSI,POTB,IFLAG		R	70
COMMON/INFO/ALPHA,OMEGA,MACH2,TJTO,NORD,GM1,DKDB,IFLG,VJAO		R	80
COMMON/DECAY/ ID,SD		R	90
C		R	100
C		R	110
C		R	120
B=REAL(Y(2))		R	130
IF (B.LT.POTB) GO TO 40		R	140
IF (IFLAG.EQ.2) GO TO 10		R	150
KAPPA=POTB*(1.-KAPPA*2.0*(EPSI-1./REAL(Y(1)))/0.04)		R	160
IFLAG=2		R	170
10 AA=0.2*MACH2		R	180
AB=(1.-TJTO-AA)		R	190
UC=REAL(Y(3))		R	200
KAPB=0.04*(1.0-KAPPA/B)		R	210
IF (AA.LT.1.E-10) GO TO 20		R	220
AK=SQRT(AB*AB+4.*AA)		R	230
RHOB=1./(1.-0.5*UC*(AB+0.5*UC*AA))		R	240
DBDX=.693147*KAPB*UC**3*RHOB/(UC/AA-((AB+AA*UC)*ALOG(ABS((AA*UC+AB		R	250
1)*UC-1.))-((AB*AB+2.*AA+AA*AB*UC)*ALOG(ABS((2.*AA*UC+AB-AK)*(AB-AK)		R	260
2)/(2.*AA*UC+AB-AK))/(AB-AK))/AK)/2./AA/AA)/2.		R	270
DUCDX=1.38629*(AA*UC+UC*AB*UC-1.)*DBDX/UC/B**3/TJTO		R	280
GO TO 50		R	290
20 IF (AB.LT.1.E-10) GO TO 30		R	300
RHOB=1./(1.-UC*AB)		R	310
DBDX=.693147*KAPB*UC**3*RHOB*AB/(UC*UC/2.+UC*(1.-UC)/AB*(1.-UC*AB)		R	320
1)*ALOG(ABS(1.-AB*UC))/AB/AB)/2.		R	330
DUCDX=-1.38629*(1.-AB*UC)*DBDX/B**3/UC/TJTO		R	340
GO TO 50		R	350
30 DBDX=2.07944*KAPB/B		R	360
DUCDX=-UC*DBDX/B		R	370
GO TO 50		R	380
40 DBDX=EPSI		R	390
DUCDX=0.		R	400
C		R	410
C		R	420
C		R	430
50 DY(2)=CMPLX(DBDX,0.)		R	440
DY(3)=CMPLX(DUCDX,0.)		R	450
IF (B.GT.SD) GO TO 70		R	460
IF (B.GT.(NTT*DB)) GO TO 60		R	470
CALL COEFF (ADAT,NTT,B,AVAL,DB)		R	480
DY(4)=(0.,1.)*AVAL*Y(4)		R	490
RETURN		R	500
60 DY(4)=(0.,1.)*Y(4)*CMPLX(OMEGA/REAL(Y(3)),AIMAG(ADAT(NTT))*NTT*DB/		R	510
1B)		R	520
RETURN		R	530
70 IF (ID.GT.1) GO TO 80		R	540
YPEAK=Y(4)		R	550
CALL COEFF (ADAT,NTT,B,APEAK,DB)		R	560
X0=Y(1)		R	570
SIGMA=ALOG(CABS(YPEAK))/REAL(X0*X0)		R	580
APR=REAL(APEAK)		R	590
ID=2		R	600
80 DY(4)=Y(4)*(-2.0*SIGMA*(Y(1)-X0)*(0.,1.)*APEAK*(2.0*Y(1)/X0-1.0))		R	610
RETURN		R	620
END		R	

*DECK COEFF	
SUBROUTINE COEFF (A,NG,S,AVAL,DB)	S 10
COMPLEX A(1),AVAL,A1,A2,A3	S 20
I=IFIX((S-0.05)/DB)	S 30
IF (I.EQ.1) I=2	S 40
IF (I.EQ.NG) I=NG-1	S 50
IF (I.GT.NG) GO TO 10	S 60
DS=S-0.05-(I-1)*DB	S 70
A1=(A(I-1)-2.*A(I)+A(I+1))/2./DB/DB	S 80
A2=(4.*A(I)-3.*A(I-1)-A(I+1))/2./DB	S 90
A3=A(I-1)	S 100
AVAL=DS*(A1*DS+A2)+A3	S 110
10 RETURN	S 120
END	S 130-

•DECK FFT		
C	SUBROUTINE FFT (IGAM, INUM, XVAL, W)	T 10
C	TO COMPUTE THE FOURIER EXPONENTIAL TRANSFORM OF X(T)	T 20
C	USING THE FFT BY BRIGHAM AND MORROW	T 30
C		T 40
C	IGAM - POWER OF TWO NUMBER OF POINTS	T 50
C	INUM - NUMBER OF POINTS	T 60
C	W - WORKING ARRAY OF DIMENSION INUM DIMENSIONED	T 70
C	IN CALLING ROUTINE	T 80
C	XVAL - DATA POINT ARRAY OF DIMENSION INUM DIMENSIONED	T 90
C	IN CALLING ROUTINE. XVAL IS DEFINED SUCH THAT	T 100
C	XVAL(1) = VALUE AT T=0	T 110
C	XVAL(INUM/2+1) = VALUE AT T=PERIOD/2	T 120
C	XVAL(INUM/2+2) = VALUE AT T=-PERIOD/2	T 130
C	XVAL(INUM) = VALUE AT T=-DELT	T 140
C	XVAL IS RETURNED AS THE FOURIER TRANSFORM S(F)	T 150
C	IN STEPS OF DELF=1/PERIOD. S(F) IS FOLDED ABOUT	T 160
C	F=INUM/2*PERIOD	T 170
C	FOR A WAVENUMBER TRANSFORM THE CALLING PROGRAM	T 180
C	MUST SUBSEQUENTLY DIVIDE BY 2*PI AND MULTIPLY	T 190
C	BY DELX FOR A CONSISTENT TRANSFORM. FOR A FREQUENCY	T 200
C	TRANSFORM THE CALLING ROUTINE MUST MULTIPLY BY DELT	T 210
C	TO OBTAIN TRANSFORM AS DEFINED BY BRIGHAM AND MORROW.	T 220
C		T 230
C	COMPLEX XVAL(INUM), W(INUM), VAL, XDUM	T 240
C	COMPLEX CEXP	T 250
C	PI=3.14159265359	T 260
C	NUM=2**(IGAM-1)	T 270
C	DO 10 I=1, NUM	T 280
C	AI=I-1	T 290
C	ANUM=NUM	T 300
C	10 W(I)=CEXP(-(0.,1.)*PI*AI/ANUM)	T 310
C	DO 20 IOUT=1, IGAM	T 320
C	N2=2**(IOUT-1)	T 330
C	IGM=IGAM-IOUT	T 340
C	IGM2=2**IGM	T 350
C	DO 20 KKK=1, N2	T 360
C	DO 20 KK=1, IGM2	T 370
C	IVAL=KK-1+(KKK-1)*2*IGM2	T 380
C	IF (IVAL.EQ.0) IVAL=0	T 390
C	ISOL1=ISOL(IOUT, IGAM, IVAL)*1	T 400
C	IDASH1=IDASH(IOUT, IGAM, IVAL)*1	T 410
C	K1=IMOVE(IOUT, IGAM, IVAL)*1	T 420
C	IVAL=IVAL+1	T 430
C	KVAL=IVAL+IGM2	T 440
C	XDUM=XVAL(IDASH1)	T 450
C	VAL=W(K1)*XVAL(ISOL1)	T 460
C	XVAL(IVAL)=XDUM*VAL	T 470
C	20 XVAL(KVAL)=XDUM*VAL	T 480
C	NUM1=INUM-1	T 490
C	DO 30 I=1, NUM1	T 500
C	I1=IREV(IGAM, I)*1	T 510
C	IVAL=I+1	T 520
C	IF (IVAL.GT.I1) GO TO 30	T 530
C	XDUM=XVAL(IVAL)	T 540
C	XVAL(IVAL)=XVAL(I1)	T 550
C	XVAL(I1)=XDUM	T 560
C	30 CONTINUE	T 570
C	RETURN	T 580
C	END	T 590
		T 600-

```

*DECK ISOL
  FUNCTION ISOL(IOUT,IGAM,K)
    IB=2** (IGAM-IOUT)
    IW=IB.AND.K
    IF (IW.EQ.0) GO TO 10
    ISOL=K
    RETURN
  10 ISOL=K+IB
    RETURN
  END

```

```

U 10
U 20
U 30
U 40
U 50
U 60
U 70
U 80
U 90-

```

```

•DECK IMOVE
FUNCTION IMOVE(IOUT,IGAM,K)
  I2=1
  IG=IGAM-1
  DO 10 I=1,IG
10  I2=I2+2**I
    I1=K.AND.I2
    I3=IGAM-IOUT
    I4=SHIFT(I1,-I3)
    I1=COMPL(I2)
    I3=I1.AND.K
    I1=I3.OR.I4
    IMOVE=IREV(IGAM,I1)
  RETURN
END

```

```

V 10
V 20
V 30
V 40
V 50
V 60
V 70
V 80
V 90
V 100
V 110
V 120
V 130
V 140-

```



```

*DECK IDASH
FUNCTION IDASH(IOUT,IGAM,K)
  IB=2** (IGAM-IOUT)
  IA=COMPL(IB)
  IDASH=K.AND.IA
  RETURN
END

```

```

W 10
W 20
W 30
W 40
W 50
W 60-

```

```

•DECK IREV
FUNCTION IREV(M,II)
  I2=1
  NG=M-1
  DO 10 I=1,NG
10  I2=I2+2**I
    I1=I1,AND,I2
    I3=I1,AND,1525258
    I4=SHIFT(I3,1)
    I3=I1,AND,1252528
    I5=SHIFT(I3,-1)
    I3=I4,OR,I5
    I4=I3,AND,314638
    I5=SHIFT(I4,2)
    I6=I3,AND,1463148
    I3=SHIFT(I6,-2)
    I4=I3,OR,I5
    I3=I4,AND,74178
    I5=SHIFT(I3,4)
    I3=I4,AND,1703608
    I6=SHIFT(I3,-4)
    I4=I5,OR,I6
    I3=I4,AND,3778
    I5=SHIFT(I3,8)
    I3=I4,AND,1774008
    I6=SHIFT(I3,-8)
    I4=I5,OR,I6
    IM=16-M
    IF (IM.EQ.0) GO TO 20
    I5=SHIFT(I4,-IM)
    GO TO 30
20  I5=I4
30  I3=COMPL(I2)
    I4=I3,AND,II
    IREV=I5,OR,I4
  RETURN
  END

```

```

X 10
X 20
X 30
X 40
X 50
X 60
X 70
X 80
X 90
X 100
X 110
X 120
X 130
X 140
X 150
X 160
X 170
X 180
X 190
X 200
X 210
X 220
X 230
X 240
X 250
X 260
X 270
X 280
X 290
X 300
X 310
X 320
X 330
X 340
X 350
X 360-

```

•DECK	ASTART		
	SUBROUTINE ASTART (VJA0,STRNO,TJT0,ALPHA,NORD,IEROR)		Y 10
	COMPLEX ALPHA,ASTAR0(4,3,8),ASTAR1(4,3,8),A(7,7),B(7)		Y 20
	COMPLEX ALSTAR(4,3,8)		Y 30
	COMMON/ADATA/ASTAR0,ASTAR1		Y 40
C			Y 50
C	LOCATE CLOSEST VALUE IN STARTING VALUE MATRIX		Y 60
C			Y 70
	IF (STRNO.LE.0.065) I=1		Y 80
	IF (STRNO.LE.0.2.AND.STRNO.GT.0.065) I=2		Y 90
	IF (STRNO.LE.0.4.AND.STRNO.GT.0.2) I=3		Y 100
	IF (STRNO.GT.0.4) I=4		Y 110
	IF (TJT0.LE.1.63) J=1		Y 120
	IF (TJT0.LE.2.56.AND.TJT0.GT.1.63) J=2		Y 130
	IF (TJT0.GT.2.56) J=3		Y 140
	K=IFIX((VJA0-0.5)/0.25)+1		Y 150
	IKEY=I		Y 160
	JKEY=J		Y 170
	IF (NORD.EQ.0) GO TO 20		Y 180
	DO 10 II=1,4		Y 190
	DO 10 JJ=1,3		Y 200
	DO 10 KK=1,8		Y 210
10	ALSTAR(II,JJ,KK)=ASTAR1(II,JJ,KK)		Y 220
	GO TO 40		Y 230
20	DO 30 II=1,4		Y 240
	DO 30 JJ=1,3		Y 250
	DO 30 KK=1,8		Y 260
30	ALSTAR(II,JJ,KK)=ASTAR0(II,JJ,KK)		Y 270
C			Y 280
C	CALCULATE STARTING VALUE MATRIX		Y 290
C			Y 300
40	DO 90 IFL=1,7		Y 310
	IF (IFL.EQ.1) GO TO 80		Y 320
	IF (IFL.LT.4) GO TO 60		Y 330
	IF (IFL.LT.6) GO TO 70		Y 340
	IF (IFL.EQ.6) GO TO 50		Y 350
	K=K+2		Y 360
	GO TO 80		Y 370
50	K=K-1		Y 380
	IF (K.EQ.0) K=2		Y 390
	IF (K.EQ.7) K=K-1		Y 400
	I=IKEY		Y 410
	GO TO 80		Y 420
60	J=J+1		Y 430
	IF (J.EQ.4) J=1		Y 440
	GO TO 80		Y 450
70	J=JKEY		Y 460
	I=I+1		Y 470
	IF (I.EQ.5) I=2		Y 480
80	IF (I.EQ.1) S1=0.03		Y 490
	IF (I.EQ.2) S1=0.1		Y 500
	IF (I.EQ.3) S1=0.3		Y 510
	IF (I.EQ.4) S1=0.5		Y 520
	IF (J.EQ.1) T1=1.0		Y 530
	IF (J.EQ.2) T1=2.273		Y 540
	IF (J.EQ.3) T1=2.857		Y 550
	AM1=0.5*(K-1)*0.25		Y 560
	A(IFL,1)=(1.,0.)		Y 570
	A(IFL,2)=S1		Y 580

	A(IFL,3)=S1*S1	Y 590
	A(IFL,4)=T1	Y 600
	A(IFL,5)=T1*T1	Y 610
	A(IFL,6)=AM1	Y 620
	A(IFL,7)=AM1*AM1	Y 630
	90 B(IFL)=ALSTAR(I,J,K)	Y 640
C		Y 650
C	CALL FOR SOLUTION OF SIMULTANEOUS EQUATIONS	Y 660
C		Y 670
	CALL SIMQ (A,B,7,KS)	Y 680S
	IF (KS.EQ.0) GO TO 100	Y 690
	IEROR=2	Y 700
	RETURN	Y 710
C		Y 720
C	CALCULATE STARTING VALUE	Y 730
C		Y 740
	100 ALPHA=B(1)*B(2)*STRNO*B(3)*STRNO*STRNO*B(4)*TJT0*B(5)*TJT0*TJT0*B(Y 750
	16)*VJA0*B(7)*VJA0*VJA0	Y 760
	RETURN	Y 770
	END	Y 780-


```
•DECK ISEQ  
  SUBROUTINE ISEQ (I)  
    GO TO (10,10,20), I  
  10 I=I+1  
    RETURN  
  20 I=1  
    RETURN  
    END
```

```
Z 10  
Z 20  
Z 30  
Z 40  
Z 50  
Z 60  
Z 70-
```

*DECK SIMQ	AA 10
SUBROUTINE SIMQ (A,B,N,KS)	AA 20
COMPLEX A(1),B(1),BIGA,SAVE	AA 30
C FORWARD SOLUTION	AA 40
C	AA 50
TOL=0.0	AA 60
KS=0	AA 70
JJ=-N	AA 80
DO 80 J=1,N	AA 90
JY=J+1	AA 100
JJ=JJ+N+1	AA 110
BIGA=(0.,0.)	AA 120
IT=JJ-J	AA 130
DO 20 I=J,N	AA 140
C	AA 150
C SEARCH FOR MAXIMUM COEFFICIENT IN COLUMN	AA 160
C	AA 170
IJ=IT+I	AA 180
IF (CABS(BIGA)-CABS(A(IJ))) 10,20,20	AA 190
10 BIGA=A(IJ)	AA 200
IMAX=I	AA 210
20 CONTINUE	AA 220
C	AA 230
C TEST FOR PIVOT LESS THAN TOLERANCE (SINGULAR MATRIX)	AA 240
C	AA 250
IF (CABS(BIGA)-TOL) 30,30,40	AA 260
30 KS=1	AA 270
RETURN	AA 280
C	AA 290
C INTERCHANGE ROWS IF NECESSARY	AA 300
C	AA 310
40 I1=J+N*(J-2)	AA 320
IT=IMAX-J	AA 330
DO 50 K=J,N	AA 340
I1=I1+N	AA 350
I2=I1-IT	AA 360
SAVE=A(I1)	AA 370
A(I1)=A(I2)	AA 380
A(I2)=SAVE	AA 390
C	AA 400
C DIVIDE EQUATION BY LEADING COEFFICIENT	AA 410
C	AA 420
50 A(I1)=A(I1)/BIGA	AA 430
SAVE=B(IMAX)	AA 440
B(IMAX)=B(J)	AA 450
B(J)=SAVE/BIGA	AA 460
C	AA 470
C ELIMINATE NEXT VARIABLE	AA 480
C	AA 490
IF (J=N) 60,90,60	AA 500
60 IOS=N*(J-1)	AA 510
DO 80 IX=JY,N	AA 520
IXJ=IOS+IX	AA 530
IT=J-IX	AA 540
DO 70 JX=JY,N	AA 550
IXJX=N*(JX-1)+IX	AA 560
JJX=IXJX+IT	AA 570
70 A(IXJX)=A(IXJX)-(A(IXJ)*A(JJX))	AA 580

```

      80 B(IX)=B(IX)-(B(J)*A(IXJ))
C
C      BACK SOLUTION
C
      90 NY=N-1
        IT=N*N
        DO 100 J=1,NY
          IA=IT-J
          IB=N-J
          IC=N
          DO 100 K=1,J
            B(IB)=B(IB)-A(IA)*B(IC)
            IA=IA-N
          100 IC=IC-1
        RETURN
      END

```

```

AA 590
AA 600
AA 610
AA 620
AA 630
AA 640
AA 650
AA 660
AA 670
AA 680
AA 690
AA 700
AA 710
AA 720
AA 730
AA 740-

```

•DECK BLKLSH

BLOCK DATA LSN

COMPLEX ASTAR0(4,3,8),ASTAR1(4,3,8)

COMMON /ADATA/ ASTAR0,ASTAR1

DATA (((ASTAR0(I,J,K),I=1,4),J=1,3),K=1,4) /

1	(.09358,-.00988),(.3018,-1.0835),(.8303,-.5622),(1.4941,-1.3801),	AB 10
2	(.09268,-.0147),(.2843,-.1235),(.5727,-.83452),(1.5899,-2.4995),	AB 20
3	(.09227,-.0165),(.2762,-.1375),(.4225,-.8857),(1.6951,-2.8943),	AB 30
4	(.09370,-.0104),(.3045,-.0895),(.8813,-.6111),(1.6631,-1.3868),	AB 40
5	(.09282,-.0155),(.2885,-.1312),(.6531,-.9349),(1.7001,-2.3972),	AB 50
6	(.09258,-.0173),(.2806,-.1450),(.4920,-1.0286),(1.7864,-2.8183),	AB 60
7	(.09432,-.0110),(.3118,-.0943),(.9654,-.6463),(1.8513,-1.3641),	AB 70
8	(.09385,-.0163),(.2965,-.1402),(.7901,-1.0089),(1.8762,-2.2768),	AB 80
9	(.09340,-.0183),(.2895,-.1538),(.6586,-1.1550),(1.9302,-2.7002),	AB 90
8	(.09584,-.0109),(.3230,-.0957),(1.0682,-.6527),(2.0507,-1.3039),	AB 100
8	(.09555,-.0164),(.3085,-.1443),(.9465,-1.0326),(2.0944,-2.1508),	AB 110
8	(.09528,-.0183),(.3018,-.1593),(.8603,-1.1941),(2.1292,-2.5534) /	AB 120

DATA (((ASTAR0(I,J,K),I=1,4),J=1,3),K=5,8) /

1	(.09622,-.0102),(.3345,-.0945),(1.1765,-.6259),(2.2561,-1.1935),	AB 130
2	(.09638,-.0156),(.3225,-.1450),(1.0996,-1.0170),(2.3324,-2.0077),	AB 140
3	(.09628,-.0175),(.3162,-.1618),(1.0434,-1.1779),(2.3664,-2.3866),	AB 150
4	(.09656,-.00982),(.3425,-1.0907),(1.2791,-.5613),(2.455,-1.0065),	AB 160
5	(.09696,-.0150),(.3355,-.1430),(1.2449,-.9702),(2.5775,-1.8286),	AB 170
6	(.09700,-.0170),(.3300,-.1610),(1.2092,-1.1304),(2.6217,-2.1918),	AB 180
7	(.09678,-.00947),(.3488,-.0855),(1.3532,-.4552),(2.5695,-0.6875),	AB 190
8	(.09733,-.0145),(.3472,-.1371),(1.3808,-.8920),(2.8178,-1.5880),	AB 200
9	(.09744,-.0165),(.3432,-.1585),(1.3623,-1.0552),(2.8803,-1.9492),	AB 210
8	(.09790,-.00917),(.3540,-.0790),(1.3646,-.3370),(2.7500,0.0000),	AB 220
8	(.09765,-.0141),(.3578,-.1318),(1.4992,-.7761),(3.0192,-1.2388),	AB 230
8	(.09782,-.0160),(.3568,-.1525),(1.5013,-.9476),(3.1223,-1.6252) /	AB 240

DATA (((ASTAR1(I,J,K),I=1,4),J=1,3),K=1,4) /

1	(.1013,-.0930),(.353,-.291),(1.0606,-.7823),(1.7405,-1.3550),	AB 250
2	(.1071,-.1403),(.388,-.427),(1.0934,-1.1439),(1.6609,-2.1340),	AB 260
3	(.1095,-.1573),(.402,-.475),(1.0913,-1.2721),(1.5279,-2.5331),	AB 270
4	(.1015,-.0930),(.357,-.293),(1.0949,-.7973),(1.8407,-1.3815),	AB 280
5	(.1074,-.1405),(.393,-.431),(1.1354,-1.1581),(1.8220,-2.1505),	AB 290
6	(.1098,-.1576),(.407,-.477),(1.1359,-1.2871),(1.7537,-2.5379),	AB 300
7	(.1018,-.0933),(.363,-.297),(1.1461,-.8100),(1.9793,-1.3880),	AB 310
8	(.1078,-.1408),(.401,-.435),(1.1952,-1.1708),(2.0182,-2.1410),	AB 320
9	(.1103,-.1581),(.414,-.479),(1.1990,-1.3006),(1.9946,-2.5056),	AB 330
8	(.1022,-.0938),(.372,-.301),(1.2134,-.8131),(2.1455,-1.3590),	AB 340
8	(.1083,-.1414),(.410,-.437),(1.2715,-1.1754),(2.2342,-2.0963),	AB 350
8	(.1110,-.1585),(.424,-.482),(1.2790,-1.3067),(2.2422,-2.4416) /	AB 360

DATA (((ASTAR1(I,J,K),I=1,4),J=1,3),K=5,8) /

1	(.1027,-.0943),(.381,-.304),(1.2928,-.7999),(2.3276,-1.2818),	AB 370
2	(.1090,-.1420),(.421,-.439),(1.3611,-1.1669),(2.4613,-2.0123),	AB 380
3	(.1117,-.1590),(.436,-.484),(1.3730,-1.3005),(2.4945,-2.3437),	AB 390
4	(.1032,-.0948),(.393,-.307),(1.3790,-.7646),(2.5121,-1.1393),	AB 400
5	(.1099,-.1426),(.434,-.441),(1.4604,-1.1414),(2.6935,-1.8810),	AB 410
6	(.1126,-.1596),(.451,-.486),(1.4774,-1.2776),(2.7490,-2.2042),	AB 420
7	(.1040,-.0953),(.407,-.306),(1.4639,-.7010),(2.6612,-0.8973),	AB 430
8	(.1109,-.1431),(.450,-.441),(1.5657,-1.0942),(2.9228,-1.6878),	AB 440
9	(.1138,-.1603),(.467,-.485),(1.5886,-1.2345),(3.0011,-2.0110),	AB 450
8	(.1049,-.0956),(.422,-.303),(1.5320,-.6039),(2.6335,-0.5950),	AB 460
8	(.1122,-.1438),(.468,-.437),(1.6713,-1.0205),(3.1281,-1.4037),	AB 470
8	(.1151,-.1611),(.484,-.482),(1.7025,-1.1668),(3.2391,-1.7421) /	AB 480

END

AB 560-

•DECK	MXNOISE		
	SUBROUTINE MXNOISE (NU,ILWR,OPNO,BOPNO,IOPT,ROD,DFT,T0F,A0,VJ,VJA0	AC	10
	1,TJT0,I,FREQ,S,ZH,SM,RSW,ALTB,BLTB,SPLB,SPLPD,SPLPG,IND)	AC	20
	DIMENSION SPLB(1),FREQ(1),SMD(20)	AC	30
	DIMENSION T1(6)	AC	40
	REAL KS,KZRZ,LH,LHM	AC	50
	INTEGER OC,BOPNO,OPNO	AC	60
C		AC	70
	COMMON/ONE/ SPLNQ(20),CQ(20),SPLND(20),CD(20),UCLUJ(20),SD(20,6)	AC	80
	COMMON/ELEVEN/X(7)	AC	90
	COMMON/TWELVE/DEC(7)	AC	100
C		AC	110
C		AC	120
	DATA IC,OC,IT/2HIC,2H ,2HIT/	AC	130
C	DATA T1/0.98,1.77,2.209,3.330,0.0,0.0/	AC	140
		AC	150
	IND=OC	AC	160
	TM=ZH*57.2957795	AC	170
	IF (OPNO.EQ.2.OR.OPNO.EQ.5) GO TO 10	AC	180
	S=FREQ(I)*DFT/VJ	AC	190
	SM=0.0	AC	200
	IF ((TM.LE.45.0.AND.VJA0.GE.1.15).AND.(S.GE.0.1.AND.S.LE.0.5)) GO	AC	210
	1 TO 410	AC	220
C		AC	230
C	THIS LOOP CALCULATES SMD FOR A GIVEN TJT0	AC	240
C	FOR ALL 16 VALUES OF SM (PACKAGE B)	AC	250
C		AC	260
	10 DO 60 N=1,20	AC	270
	IF (TJT0.GE.0.98.AND.TJT0.LE.3.33) GO TO 20	AC	280
	IF (TJT0.LT.T1(1)) SMD(N)=SD(N,1)-(T1(1)-TJT0)*(SD(N,2)-SD(N,1))/(AC	290
	T1(2)-T1(1))	AC	300
	IF (TJT0.GT.T1(4)) SMD(N)=SD(N,4)	AC	310
	IF (SMD(N).LT.0.0) SMD(N)=0.0	AC	330
	GO TO 60	AC	340
	20 J=2	AC	350
	30 IF (TJT0-T1(J)) 50,50,40	AC	360
	40 J=J+1	AC	370
	GO TO 30	AC	380
	50 SMD(N)=SD(N,J)+(T1(J)-TJT0)*(SD(N,J-1)-SD(N,J))/(T1(J)-T1(J-1))	AC	390
	60 CONTINUE	AC	400
C		AC	410
C	THIS SECTION ITERATES TO FIND SM ASSOCIATED WITH THE REQUIRED S	AC	420
C		AC	430
	ICOUNT=0	AC	440
	S0=FREQ(I)*DFT/VJ	AC	450
	SM1=0.01	AC	460
	SM=SM1	AC	470
	CALL DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,T0F,VJA0	AC	480S
	1,TJT0,GAMA)	AC	490
	S1=S	AC	500
	SM2=0.63	AC	510
	SM=SM2	AC	520
	CALL DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,T0F,VJA0	AC	530S
	1,TJT0,GAMA)	AC	540
	S2=S	AC	550
	SME=SM1*(S0-S1)*(SM2-SM1)/(S2-S1)	AC	560
	SM=SME	AC	570
	IF (SM.LT.0.0) GO TO 380	AC	580

CALL DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,T0F,VJA0	AC 590S
1,TJT0,GAMA)	AC 600
SOE=S	AC 610
IF (ABS(SOE-S0),LE,0.001) GO TO 80	AC 620
70 SM1=SM2	AC 630
SM2=SME	AC 640
S1=S2	AC 650
S2=SOE	AC 660
SME=SM1*(S0-S1)*(SM2-SM1)/(S2-S1)	AC 670
SM=SME	AC 680
IF (SM,LT,0.0) GO TO 380	AC 690
CALL DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,T0F,VJA0	AC 700S
1,TJT0,GAMA)	AC 710
SOE=S	AC 720
ICOUNT=ICOUNT+1	AC 730
IF (ABS(SOE-S0),LE,0.001) GO TO 80	AC 740
IF (ICOUNT,EQ,50) GO TO 370	AC 750
GO TO 70	AC 760
C THIS SECTION INTERPOLATES VALUES OF SMD,SPLNQ,SPLND,CQ,CD	AC 770
C	AC 780
C	AC 790
80 SM=SME	AC 800
S=SOE	AC 810
SM1000=SM*1000.0	AC 820
Y=ALOG10(SM1000)	AC 830
XX=10.0*Y-14	AC 840
IF (XX,GT,28) GO TO 350	AC 850
IF (XX,LT,1.0) GO TO 350	AC 860
JX=XX	AC 870
J1=JX+1	AC 880
EX=XX-JX	AC 890
SMDI=SMD(JX)+EX*(SMD(J1)-SMD(JX))	AC 900
SPLNQI=SPLNQ(JX)+EX*(SPLNQ(J1)-SPLNQ(JX))	AC 910
SPLNQI=SPLNQI-20.0*ALOG10(RODA/72.0)	AC 920
SPLNDI=SPLND(JX)+EX*(SPLND(J1)-SPLND(JX))	AC 930
SPLNDI=SPLNDI-20.0*ALOG10(RODA/72.0)	AC 940
CQI=CQ(JX)+EX*(CQ(J1)-CQ(JX))	AC 950
CDI=CD(JX)+EX*(CD(J1)-CD(JX))	AC 960
C	AC 970
IF (BOPNO,EQ,1) GO TO 100	AC 980
IF (BOPNO,EQ,2) GO TO 90	AC 990
C	AC1000
90 PI=3.141593	AC1010
KZRZ=PI*FREQ(I)*DFT/A0	AC1020
DELRAD=(SMDI*VJA0)/(DM*KZRZ)	AC1030
UCLUJI=UCLUJ(JX)+EX*(UCLUJ(J1)-UCLUJ(JX))	AC1040
UICZ=VJA0	AC1050
IF (DELRAD,GT,1.818535) UICZ=VJA0*UCLUJI	AC1060
ETAIN=ETAI	AC1070
IF (DELRAD,GT,1.818535) ETAIN=ETAI/UCLUJI	AC1080
GM=(GAMA-1.0)/2.0	AC1090
TITZ=1.0-GM*UICZ*UICZ*(TS-1.0-GM*ETAIN*ETAIN*UICZ*UICZ)/ETAIN	AC1100
GO TO 100	AC1110
C	AC1120
100 KS=(DS*DS)/(TS*GS)-(COS(Z)*COS(Z))	AC1130
DSP2=DS*DS+0.06*0.06*VJA0*VJA0*COS(Z)*COS(Z)	AC1140
IND=OC	AC1150
IF (KS,LT,0.0) GO TO 170	AC1160
C	AC1170

C	**PREDICTION OUTSIDE CONE OF SILENCE**	AC1180
C		AC1190
C	QUADRUPOLE CONTRIBUTION	AC1200
C		AC1210
	LH=80.0*ALOG10(VJA0)	AC1220
	CA=-10.0*(2*NU*3)*ALOG10(DM)	AC1230
	IF (BOPNO,EQ.1) GO TO 110	AC1240
	IF (BOPNO,EQ.2) GO TO 120	AC1250
110	FF=10.0*ALOG10(DS**4*DSP2*(NU-2))-30.0*ALOG10(TS)-20.0*ALOG10(GS)	AC1260
	ZZ=1.0*(CQI*(TS*TS)*(GS*GS)*((1.0/DS)**4)*((COS(Z))**4))	AC1270
	GO TO 130	AC1280
120	CALL LILLEY (NU,IOPT,6,DELRAD,UICZ,TITZ,GAMA,KZRZ,TZ,ETAIN,RSW,ALT	AC1290S
	IB,BLTS,ILWR,FPM,FPD,FPQ,IERL)	AC1300
	IF (IERL,NE.0) GO TO 420	AC1310
	FF=FPQ	AC1320
	ZZ=1.0*CQI*10.0*((FPM-FPQ)/10.0)*COS(Z)**4	AC1330
	GO TO 130	AC1340
130	IF (ZZ,LE.0.0) GO TO 360	AC1350
	DIRECT=10.0*ALOG10(ZZ)	AC1360
	SPLPQ=SPLNQI*LH*CA*FF*DIRECT	AC1370
C		AC1380
C	DIPOLE CONTRIBUTION	AC1390
C		AC1400
	LH=60.0*ALOG10(VJA0)	AC1410
	RTS=1.0/TS	AC1420
	TEMPS=10.0*ALOG10((1.0-RTS)*(1.0-RTS))	AC1430
	CA=-10.0*(2*NU*1)*ALOG10(DM)	AC1440
	IF (BOPNO,EQ.1) GO TO 140	AC1450
	IF (BOPNO,EQ.2) GO TO 150	AC1460
140	FF=10.0*ALOG10(DS*DS*DSP2*(NU-2))-20.0*ALOG10(TS)-10.0*ALOG10(GS)	AC1470
	ZZ=1.0*(CDI*TS*GS*((1.0/DS)**2)*((COS(Z))**2))	AC1480
	GO TO 160	AC1490
150	FF=FPD	AC1500
	ZZ=1.0*CDI*10.0*((FPM-FPD)/10.0)*COS(Z)**2	AC1510
	GO TO 160	AC1520
160	IF (ZZ,LE.0.0) GO TO 360	AC1530
	DIRECT=10.0*ALOG10(ZZ)	AC1540
	SPLPD=SPLNDI*LH*TEMPS*CA*FF*DIRECT	AC1550
C		AC1560
	GO TO 330	AC1570
C		AC1580
C	**PREDICTION INSIDE CONE OF SILENCE**	AC1590
C		AC1600
170	CONTINUE	AC1610
	IND=IC	AC1620
	TZ=Z*57.2957795	AC1630
	IF (TZ,LT.30.0,AND,BOPNO,EQ.1) GO TO 400	AC1640
C		AC1650
	IF (BOPNO,EQ.1) GO TO 180	AC1660
	IF (BOPNO,EQ.2) GO TO 260	AC1670
C		AC1680
C	CALCULATION OF UT/US AND TRANSITION POINT TEMPERATURE RATIO TT	AC1690
C		AC1700
180	ONE=2.0*ETAI*VJA0/COS(Z)+TS-1.0*ETAI*ETAI*VJA0*VJA0*VJA0*0.2	AC1710
	TWO=1.2*ETAI*ETAI*VJA0*VJA0	AC1720
	THREE=(SIN(Z)/COS(Z))**2	AC1730
	FOUR=ONE*ONE-4.0*TWO*THREE	AC1740
	IF (FOUR,LT.0.0) GO TO 190	AC1750
	UTUS=(ONE-SQRT(FOUR))/(2.0*TWO)	AC1760

	GO TO 200	AC1770
190	UTUS=100.0	AC1780
200	CONTINUE	AC1790
C		AC1800
	TT=((1.0/COS(Z))-(VJA0*UTUS*ETAI))**2	AC1810
C		AC1820
C	CALCULATION OF EXPONENTIAL DECAY	AC1830
C		AC1840
	PHI=UTUS*ETAI	AC1850
	DE=((TJT0-1.0)/TT)*(2.0*VJA0/(SQRT(TT)))+(0.2*VJA0*VJA0*(1.0-2.0*P	AC1860
	HI)/TT)	AC1870
	GPHI=GPT(PHI)	AC1880
	IF (GPHI.EQ.0.0) GO TO 340	AC1890
	DEN=-1.0*GPHI*COS(Z)*COS(Z)*DE	AC1900
C		AC1910
	Q=(SQRT(ABS(KS)))**3	AC1920
	Y=(4.0*Q)/(3.0*DEN)	AC1930
	AA3=Y*SMDI*VJA0/DM	AC1940
	IF (AA3.GE.0.6) GO TO 240	AC1950
	IND=IT	AC1960
	IF (AA3.LT.0.0) GO TO 390	AC1970
	II=2	AC1980
210	IF (AA3-X(II)) 230,230,220	AC1990
220	II=II+1	AC2000
	IF (II.GT.7) GO TO 240	AC2010
	GO TO 210	AC2020
230	QQ=DEC(II)*((X(II)-AA3)/(X(II)-X(II-1)))*(DEC(II-1)-DEC(II))	AC2030
	GO TO 250	AC2040
240	QQ=0.39152*EXP(-AA3)/(SQRT(3.0*AA3+1.0))	AC2050
250	DECAY=10.0*ALOG10(QQ)	AC2060
	GO TO 260	AC2070
C		AC2080
C	QUADRUPOLE CONTRIBUTION	AC2090
C		AC2100
260	LH=80.0*ALOG10(VJA0)	AC2110
	CA=-10.0*(2*NU+3)*ALOG10(DM)	AC2120
	IF (BOPNO.EQ.1) GO TO 270	AC2130
	IF (BOPNO.EQ.2) GO TO 280	AC2140
270	CONTINUE	AC2150
	P1=ABS(KS)*COS(Z)*COS(Z)	AC2160
	FFF=10.0*ALOG10(DSP2**(NU-2)*P1*P1/TS)	AC2170
	FFI=FFF*DECAY	AC2180
	ZZ=P1/(COS(Z)*COS(Z))	AC2190
	YY=1.0+CQI/(ZZ*ZZ)	AC2200
	GO TO 290	AC2210
280	CALL LILLEY (NU,IOPT,6,DELRAD,UICZ,TITZ,GAMA,KZRZ,TZ,ETAIN,RSW,ALT	AC2220S
	1B,BLTB,ILWR,FPM,FPD,FPQ,IERL)	AC2230
	IF (IERL.NE.0) GO TO 420	AC2240
	FFI=FPQ	AC2250
	YY=1.0+CQI*10.0**((FPM-FPQ)/10.0)*COS(Z)**4	AC2260
	GO TO 290	AC2270
290	IF (YY.LE.0.0) GO TO 360	AC2280
	DIRECI=10.0*ALOG10(YY)	AC2290
	SPLPQ=SPLNQI*LH+CA*FFI*DIRECI	AC2300
C		AC2310
C	DIPOLE CONTRIBUTION	AC2320
C		AC2330
	LHM=60.0*ALOG10(VJA0)	AC2340
	RTS=1.0/TS	AC2350

TEMP2=10.0*ALOG10((1.0-RTS)*(1.0-RTS))	AC2360
CAH=-10.0*(2*NU+1)*ALOG10(DH)	AC2370
IF (BOPNO,EQ.1) GO TO 300	AC2380
IF (BOPNO,EQ.2) GO TO 310	AC2390
300 FF=10.0*ALOG10(DSP2** (NU-2)*P1/TS)	AC2400
FFH=FF+DECAY	AC2410
YYH=1.0*CDI/ZZ	AC2420
GO TO 320	AC2430
310 FFH=FPD	AC2440
YYH=1.0*CDI*10.0**((FPM-FPD)/10.0)*COS(Z)**2	AC2450
GO TO 320	AC2460
320 IF (YYH,LE.0.0) GO TO 360	AC2470
DIRH=10.0*ALOG10(YYH)	AC2480
SPLPD=SPLNDI+LHM+TEMP2+CAH+FFH+DIRH	AC2490
C	AC2500
C	AC2510
C	AC2520
330 SPLB(I)=10.0*ALOG10(10.0** (SPLPQ/10.0)+10.0** (SPLPD/10.0))	AC2530
GO TO 430	AC2540
C	AC2550
C	AC2560
C	AC2570
340 SPLB(I)=1.0	AC2580
SPLPQ=0.0	AC2590
SPLPD=0.0	AC2600
GO TO 430	AC2610
C	AC2620
350 SPLB(I)=2.0	AC2630
SPLPQ=0.0	AC2640
SPLPD=0.0	AC2650
GO TO 430	AC2660
C	AC2670
360 SPLB(I)=3.0	AC2680
SPLPQ=0.0	AC2690
SPLPD=0.0	AC2700
GO TO 430	AC2710
C	AC2720
370 SPLB(I)=4.0	AC2730
SPLPQ=0.0	AC2740
SPLPD=0.0	AC2750
GO TO 430	AC2760
C	AC2770
380 SPLB(I)=5.0	AC2780
SPLPQ=0.0	AC2790
SPLPD=0.0	AC2800
GO TO 430	AC2810
C	AC2820
390 SPLB(I)=6.0	AC2830
SPLPQ=0.0	AC2840
SPLPD=0.0	AC2850
GO TO 430	AC2860
C	AC2870
400 SPLB(I)=7.0	AC2880
SPLPQ=0.0	AC2890
SPLPD=0.0	AC2900
GO TO 430	AC2910
C	AC2920
410 SPLB(I)=8.0	AC2930
SPLPQ=0.0	AC2940

SPLPD=0.0
GO TO 430
420 CONTINUE
SPLB(I)=FLOAT(IERL)
SPLPQ=0.0
SPLPD=0.0
430 CONTINUE
RETURN
END

AC2950
AC2960
AC2970
AC2980
AC2990
AC3000
AC3010
AC3020
AC3030-

*DECK SELECT		
SUBROUTINE SELECT (NU,ISS)		AD 10
C		AD 20
DIMENSION IRD(8),SM(28),DELRAD(28,6)		AD 30
DIMENSION IWRT(8)		AD 40
COMMON/FOUR/ A(16)		AD 50
COMMON/FIVE/ B(16)		AD 60
COMMON/SIX/ C(16)		AD 70
COMMON/SEVEN/ D(16)		AD 80
COMMON/EIGHT/ E(16)		AD 90
COMMON/NINE/ F(16)		AD 100
COMMON/THIRTN/ R(16)		AD 110
COMMON/EIGHTY/ T1(16),SD(16,6)		AD 120
C		AD 130
COMMON/FOUR1/ A1(28)		AD 140
COMMON/FIVE1/ R1(28)		AD 150
COMMON/SIX1/ C1(28)		AD 160
COMMON/SEVEN1/ D1(28)		AD 170
COMMON/EIGHT1/ E1(28)		AD 180
COMMON/NINE1/ F1(28)		AD 190
COMMON/THIRTN1/ R1(28)		AD 200
COMMON/EIGHTY1/ SD1(28,6),SDT1(28,6)		AD 210
C		AD 220
COMMON/ONE/ SPLNQ(28),CQ(28),SPLND(28),CD(28),UCLUJ(28),XSD(28,6)		AD 230
C		AD 240
COMMON/TWO/ ETA(28),XE(28)		AD 250
DATA PI / 3.141593 /		AD 260
DATA SM / 0.0316,0.04,0.05,0.063,0.08,0.1,0.125,0.16,0.2,0.25,		AD 270
1 0.316,0.4,0.5,0.63,0.8,1.0,1.25,1.6,2.0,2.5,3.16,4.0,5.0,		AD 280
2 6.3,8.0,10.0,12.5,16.0 /		AD 290
C		AD 300
ICOUNT=0		AD 310
C		AD 320
IF (NU.EQ.3) GO TO 40		AD 330
C		AD 340
DO 10 N=1,28		AD 350
ETA(N)=A1(N)		AD 360
SPLNQ(N)=B1(N)		AD 370
CQ(N)=C1(N)		AD 380
SPLND(N)=D1(N)		AD 390
XE(N)=E1(N)		AD 400
CD(N)=F1(N)		AD 410
UCLUJ(N)=R1(N)		AD 420
10 CONTINUE		AD 430
DO 30 I=1,4		AD 440
DO 30 N=1,28		AD 450
IF (ISS.EQ.1) GO TO 20		AD 460
XSD(N,I)=SD1(N,I)		AD 470
GO TO 30		AD 480
20 XSD(N,I)=SDT1(N,I)		AD 490
30 CONTINUE		AD 500
GO TO 90		AD 510
C		AD 520
40 CONTINUE		AD 530
DO 60 N=1,28		AD 540
IF (N.LT.6.OR.N.GT.21) GO TO 50		AD 550
ETA(N)=A(N-5)		AD 560
SPLNQ(N)=B(N-5)		AD 570
CQ(N)=C(N-5)		AD 580

SPLND(N)=D(N-5)	AD 590
XE(N)=E(N-5)	AD 600
CD(N)=F(N-5)	AD 610
UCLUJ(N)=R(N-5)	AD 620
GO TO 60	AD 630
50 CONTINUE	AD 640
ETA(N)=0.0	AD 650
SPLNQ(N)=0.0	AD 660
CQ(N)=0.0	AD 670
SPLND(N)=0.0	AD 680
XE(N)=0.0	AD 690
CD(N)=0.0	AD 700
UCLUJ(N)=1.0	AD 710
60 CONTINUE	AD 720
DO 80 I=1,4	AD 730
DO 80 N=1,28	AD 740
IF (N.LT.6.OR.N.GT.21) GO TO 70	AD 750
XSD(N,I)=SD(N-5,I)	AD 760
GO TO 80	AD 770
70 XSD(N,I)=0.0	AD 780
80 CONTINUE	AD 790
C	AD 800
90 CONTINUE	AD 810
IF (ISS.EQ.0.OR.ISS.EQ.1) GO TO 150	AD 820
READ (5,200) (IRD(I),I=1,8)	AD 830*
DO 100 I=1,8	AD 840
IF (IRD(I).EQ.0) GO TO 100	AD 850
ICOUNT=ICOUNT+1	AD 860
IWRT(ICOUNT)=I	AD 870
100 CONTINUE	AD 880
IF (IRD(1).EQ.1) READ (5,210) (SPLNQ(N),N=1,28)	AD 890*
IF (IRD(2).EQ.1) READ (5,210) (CQ(N),N=1,28)	AD 900*
IF (IRD(3).EQ.1) READ (5,210) (SPLND(N),N=1,28)	AD 910*
IF (IRD(4).EQ.1) READ (5,210) (CD(N),N=1,28)	AD 920*
IF (IRD(5).EQ.1) READ (5,210) (ETA(N),N=1,28)	AD 930*
IF (IRD(6).EQ.1) READ (5,210) (XE(N),N=1,28)	AD 940*
IF (IRD(7).EQ.1) READ (5,210) (UCLUJ(N),N=1,28)	AD 950*
IF (IRD(8).EQ.0) GO TO 150	AD 955
DO 120 JJ=1,4	AD 960
IF (IRD(8).EQ.1) READ (5,210) (DELRAD(N,JJ),N=1,28)	AD 970*
DO 110 N=1,28	AD 980
XSD(N,JJ)=PI*SM(N)*DELRAD(N,JJ)	AD 990
110 CONTINUE	AD1000
120 CONTINUE	AD1010
IF (IRD(8).NE.2) GO TO 150	AD1020
DO 130 N=1,28	AD1030
XSRJ=2.0/SQRT(0.02)*SM(N)*SM(N)+0.057*SM(N)	AD1040
DELRAD(N,1)=XSRJ/7.616559	AD1050
IF (XSRJ.GT.13.85) DELRAD(N,1)=(1.0+0.55*(XSRJ-13.85)/(26.0-13.85)	AD1060
1)*1.818535	AD1070
130 CONTINUE	AD1080
FAC1=0.98**0.25	AD1090
FAC2=1.77**0.25	AD1100
FAC3=2.209**0.25	AD1110
FAC4=3.330**0.25	AD1120
DO 140 N=1,28	AD1130
DELRAD(N,2)=DELRAD(N,1)*FAC2	AD1140
XSD(N,2)=PI*SM(N)*DELRAD(N,2)	AD1150
DELRAD(N,3)=DELRAD(N,1)*FAC3	AD1160

XSD(N,3)=PI*SM(N)*DELRAD(N,3)	AD1170
DELRAD(N,4)=DELRAD(N,1)*FAC4	AD1180
XSD(N,4)=PI*SM(N)*DELRAD(N,4)	AD1190
DELRAD(N,1)=DELRAD(N,1)*FAC1	AD1200
XSD(N,1)=PI*SM(N)*DELRAD(N,1)	AD1210
140 CONTINUE	AD1220
150 CONTINUE	AD1230
IF (IRD(8),NE,0) GO TO 170	AD1240
DO 160 JJ=1,4	AD1250
DO 160 N=1,28	AD1260
DELRAD(N,JJ)=XSD(N,JJ)/(PI*SM(N))	AD1270
160 CONTINUE	AD1280
170 CONTINUE	AD1290
WRITE (6,220)	AD1300*
IF (ICOUNT,EQ,0) WRITE (6,230)	AD1310*
IF (ICOUNT,GT,0) WRITE (6,240) (IWRT(I),I=1,ICOUNT)	AD1320*
IF (IRD(8),EQ,2) WRITE (6,250)	AD1330*
WRITE (6,260) (SM(N),N=1,14)	AD1340*
WRITE (6,270) (SPLNQ(N),N=1,14)	AD1350*
WRITE (6,280) (CQ(N),N=1,14)	AD1360*
WRITE (6,290) (SPLND(N),N=1,14)	AD1370*
WRITE (6,300) (CD(N),N=1,14)	AD1380*
WRITE (6,310) (ETA(N),N=1,14)	AD1390*
WRITE (6,320) (XE(N),N=1,14)	AD1400*
WRITE (6,330) (UCLUJ(N),N=1,14)	AD1410*
DO 180 JJ=1,4	AD1420
WRITE (6,340) (DELRAD(N,JJ),N=1,14)	AD1430*
180 CONTINUE	AD1440
WRITE (6,350) (SM(N),N=15,28)	AD1450*
WRITE (6,270) (SPLNQ(N),N=15,28)	AD1460*
WRITE (6,280) (CQ(N),N=15,28)	AD1470*
WRITE (6,290) (SPLND(N),N=15,28)	AD1480*
WRITE (6,300) (CD(N),N=15,28)	AD1490*
WRITE (6,310) (ETA(N),N=15,28)	AD1500*
WRITE (6,320) (XE(N),N=15,28)	AD1510*
WRITE (6,330) (UCLUJ(N),N=15,28)	AD1520*
DO 190 JJ=1,4	AD1530
WRITE (6,340) (DELRAD(N,JJ),N=15,28)	AD1540*
190 CONTINUE	AD1550
RETURN	AD1560
C	AD1570
200 FORMAT (16I5)	AD1580
210 FORMAT (8F10,1)	AD1590
220 FORMAT (1H1,44X,"MIXING NOISE SOURCE AND MEAN FLOW CONSTANTS")	AD1600
230 FORMAT (/,52X,"* STANDARD DATA VALUES USED *")	AD1610
240 FORMAT (/,44X,"USER INPUT VALUES FOR PARAMETERS",8(1X,11))	AD1620
250 FORMAT (1X,"SOURCE LOCATION MODEL USED , WITH SIGMA = 13.5 , ", "TO	AD1630
1 CALCULATE DELTA/RJ",/,1X,"(TJ/T0)**0.25 DEPENDENCE ", "ASSUMED , A	AD1640
2T STANDARD TEMPERATURES 0.98,1.77,2.209,3.33")	AD1650
260 FORMAT (///,1X,"SM",7X,14F7,3)	AD1660
270 FORMAT (/,1X,"SPLQ",5X,14F7,2)	AD1670
280 FORMAT (/,1X,"AXWTQ",4X,14F7,2)	AD1680
290 FORMAT (/,1X,"SPLD",5X,14F7,2)	AD1690
300 FORMAT (/,1X,"AXWTD",4X,14F7,2)	AD1700
310 FORMAT (/,1X,"VS/VJ",4X,14F7,2)	AD1710
320 FORMAT (/,1X,"VC/VJ",4X,14F7,2)	AD1720
330 FORMAT (/,1X,"VMAX/VJ",2X,14F7,2,/))	AD1730
340 FORMAT (1X,"DELTA/RJ",1X,14F7,2)	AD1740
350 FORMAT (///,1X,"SM",7X,14F7,2)	AD1750
END	AD1760-

*DECK DOPPLER		AE 10
SUBROUTINE DOPPLE (NU,SM,Z,TS,GS,DS,DM,S,TZ,EI,ETAI,RODA,ROD,ZM,TO		AE 20
IF,VJA0,TJT0,G)		AE 30
COMMON/TWO/ETA(28),E(28)		AE 40
C		AE 50
C	CALCULATION OF DM AND S*****	AE 60
C		AE 70
C	EI=INTERPOLATED E	AE 80
C	ETAI=INTERPOLATED ETA	AE 90
C	A=ALPHA	AE 100
C	B=BETA	AE 110
C	GS=GAMMA RATIO GS/G0	AE 120
C	TS=SOURCE TEMPERATURE RATIO TS/T0	AE 130
C		AE 140
	IF (NU,NE.3) GO TO 30	AE 150
	IF (SM,LT.3.16) GO TO 10	AE 160
	EI=0.6	AE 170
	ETAI=0.6	AE 180
	GO TO 70	AE 190
10	IF (SM,GT.0.1) GO TO 20	AE 200
	EI=0.8	AE 210
	ETAI=0.5	AE 220
	GO TO 70	AE 230
20	SM1000=SM*1000	AE 240
	Y=ALOG10(SM1000)	AE 250
	X=10.0*Y-14.0	AE 260
	GO TO 60	AE 270
30	IF (SM,LT.16.0) GO TO 40	AE 280
	EI=0.6	AE 290
	ETAI=0.6	AE 300
	GO TO 70	AE 310
40	IF (SM,GT.0.0316) GO TO 50	AE 320
	EI=1.0	AE 330
	ETAI=0.3	AE 340
	GO TO 70	AE 350
50	SM1000=SM*1000	AE 360
	Y=ALOG10(SM1000)	AE 370
	X=10.0*Y-14.0	AE 380
60	CONTINUE	AE 390
	JX=X	AE 400
	J1=JX+1	AE 410
	EX=X-JX	AE 420
	EI=E(JX)+EX*(E(J1)-E(JX))	AE 430
	ETAI=ETA(JX)+EX*(ETA(J1)-ETA(JX))	AE 440
C	CALCULATION OF RADIATION ANGLE TZ(DEGREES)	AE 450
C		AE 460
	70 POS=1.0/SQRT(0.057*SM+0.021*SM*SM)	AE 470
	RODA=SQRT(ROD*ROD+POS*POS-2.0*ROD*POS*COS(ZM))	AE 480
	XX=(ROD*ROD+RODA*RODA-POS*POS)/(2.0*ROD*RODA)	AE 490
	AA=SQRT(1.0-XX*XX)	AE 500
	W=ATAN2(AA,XX)	AE 510
	Z=W*ZM	AE 520
	TZ=Z*57.2957795	AE 530
C		AE 540
C	CALCULATION OF GAMMAS	AE 550
C		AE 560
	D=0.073	AE 570
	TSM=1.0*(0.6*(TJT0-1.0))+(VJA0-VJA0*(0.6-0.6*0.6)*0.2)	AE 580

IF (TSM.LT.0.999) D=0.034	AE 590
TS=1.0*(TSM-1.0)/((0.98*D/(SM*SM))**0.25)	AE 600
T0C=((T0F-32.0)*5.0)/9.0	AE 610
T0K=T0C+273.0	AE 620
T=TS*T0K	AE 630
G0=1.421-(T0K/11800.0)*(EXP(-ABS(T0K-450.0)/200.0)/80.0)	AE 640
IF (T0K.LE.290.0) G0=1.402	AE 650
G=1.421-(T/11800.0)*(EXP(-ABS(T-450.0)/200.0)/80.0)	AE 660
IF (T.LE.290.0) G=1.402	AE 670
GS=G/G0	AE 680
	AE 690
A=0.2*TS**1.2	AE 700
IF (NU.EQ.3) A=0.2*TS**0.6	AE 710
B=0.55*TS**0.2	AE 720
IF (NU.EQ.3) B=0.4*TS**0.2	AE 730
DS=1.0-ETA1*VJA0*COS(Z)	AE 740
DC=1.0-EI*VJA0*COS(Z)	AE 750
	AE 760
CALCULATION OF MODIFIED DOPPLER FACTOR DM AND STROUHAL NUMBER S	AE 770
	AE 780
*** A NEGATIVE SQUARE ROOT ARGUMENT ERROR CAN OCCUR IN THE NEXT STATEMENT, FOR EXAMPLE, AT HIGH TEMPERATURES. THIS PROBLEM DOES NOT ARISE IF DM IS GIVEN BY	
DM=SQRT(DC*DC+B*B*VJA0*(VJA0*COS(Z)*COS(Z)	
1 +A*A*VJA0*VJA0*ABS(DS*DS/(TS*GS)-COS(Z)*COS(Z)))	
THIS REVISED DEFINITION OF DM WAS SUGGESTED BY THE INVESTIGATION INTO TRANSVERSE NONCOMPACTNESS EFFECTS WITH NUMERICAL LILLEY EQUATION SOLUTIONS, DESCRIBED IN SECTION 2.1.5.2. HOWEVER THE SHEAR LAYER THICKNESS PARAMETER SHOULD BE FIRST RE-OPTIMISED, WITH THE REVISED DM, BEFORE THIS CHANGE IS CONSIDERED FOR GENERAL PREDICTION PURPOSES.	
DM=SQRT(DC*DC+B*B*VJA0*VJA0*COS(Z)*COS(Z)+A*A*VJA0*VJA0*(DS*DS/(TS	AE 790
1*GS)-COS(Z)*COS(Z)))	AE 800
S=SM/DM	AE 810
RETURN	AE 820
END	AE 830-

•DECK	GPT		AF	10
	FUNCTION	GPT(PHI)	AF	20
C			AF	30
C	THIS	FUNCTION CALCULATES THE GRADIENT OF VELOCITY PROFILE*****	AF	40
	DATA	RPI,PI/1.7724539*3.141593/	AF	50
	IF	(PHI.LT.0.0.OR.PHI.GT.1.0) GO TO 10	AF	60
	GPT	=0.0	AF	70
	IF	(PHI.LT.0.0001.OR.PHI.GT.0.9999) RETURN	AF	80
	X	=0.0	AF	90
	DO	10 I=1,20	AF	100
	DEL	=0.5*(1.0-ERF(RPI*X))-PHI	AF	110
	DELP	=-EXP(-X*X*PI)	AF	120
	DIF	=DEL/DELP	AF	130
	X	=X-DIF	AF	140
	IF	(ABS(DIF).LT.0.0001) GO TO 20	AF	150
10	CONTINUE		AF	160
	STOP	7	AF	170
20	CONTINUE		AF	180
	GPT	=DELP	AF	190
	RETURN		AF	200
	END		AF	210-


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C *DECK LILLEY
C ***** AG 10
C SUBROUTINE LILLEY AG 20
C AG 30
C PURPOSE AG 40
C TO SOLVE THE LILLEY EQUATION WITH SPECIFIED MONOPOLE, DIPOLE AG 50
C AND QUADRUPOLE SOURCE DISTRIBUTIONS IN AN AXISYMMETRIC, AG 60
C PARALLEL FLOW FIELD AT A GIVEN FREQUENCY AND OBSERVER ANGLE AG 70
C AG 80
C USAGE AG 90
C CALL LILLEY(NU, IOPT, IW, DELRAD, UICZ, TITZ, GAMMA, KZRZ, THETZ, AG 100
C ETAIN, RSW, ALTB, BLTB, ILWR, FPM, FPD, FPG, IERL) AG 110
C AG 120
C DESCRIPTION OF PARAMETERS AG 130
C ** INPUT AG 140
C IOPT - #1 RING SOURCE, RADIUS SPECIFIED BY ETAIN AG 150
C #2 RADIALLY DISTRIBUTED SOURCE, WIDTH RSW AG 160
C #3 AS FOR IOPT=2 BUT WITH RADIAL-AZIMUTHAL AG 170
C NONCOMPACTNESS SPECIFIED BY ALTB, BLTB AG 180
C IW - OUTPUT FILE INDICATOR AG 190
C DELRAD - VORTICITY THICKNESS OF VELOCITY PROFILE NORMALISED AG 200
C BY JET NOZZLE RADIUS. 0.LT.DELRAD.LE.9 AG 210
C UICZ - CENTER-LINE VELOCITY NORMALISED BY AMBIENT SOUND AG 220
C SPEED. 0.LE.UICZ.LE.3 AG 230
C TITZ - CENTER-LINE STATIC TEMPERATURE NORMALISED BY AG 240
C AMBIENT TEMPERATURE. 0.LT.TITZ.LE.9 AG 250
C GAMMA - RATIO OF SPECIFIC HEATS. 1.LE.GAMMA.LE.1.5 AG 260
C KZRZ - 2*PI*FREQUENCY*NOZZLE RADIUS/AMBIENT SOUND SPEED AG 270
C 0.LT.KZRZ.LE.20 AG 280
C THETZ - FAR-FIELD OBSERVER ANGLE TO DOWNSTREAM JET AXIS AG 290
C 0.LT.THETZ.LT.180 AG 300
C ETAIN - FLOW VELOCITY AT SOURCE RADIUS VS/VMAX AG 310
C STANDARD VALUES ARE TABULATED BELOW AG 320
C ISRL VS/VMAX=ETAIN (ETA=VS/VJ) AG 330
C 1 0.990 AG 340
C 2 0.982 AG 350
C 3 0.969 AG 360
C 4 0.948 AG 370
C 5 0.919 AG 380
C 6 0.877 AG 390
C 7 0.824 AG 400
C 8 0.757 AG 410
C 9 0.679 AG 420
C 10 0.670 AG 430
C 11 0.663 AG 440
C 12 0.600 AG 450
C 13 0.592 AG 460
C 14 0.500 AG 470
C 15 0.408 AG 480
C 16 0.321 AG 490
C 17 0.243 AG 500
C 18 0.176 AG 510
C 19 0.123 AG 520
C 20 0.081 AG 530
C 21 0.052 AG 540
C 22 0.031 AG 550
C 23 0.018 AG 560
C 24 0.010 AG 570
C RSW - TURBULENCE INTENSITY RADIAL HALF WIDTH AG 580

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C			AG 590
C	ALTB	- THESE COEFFICIENTS SPECIFY THE RADIAL-AZIMUTHAL	AG 600
C	BLTB	- COHERENCE LENGTH SCALE $LTB=ALTB \times BLTB$	AG 610
C			AG 620
C			AG 630
C	ILWR	- SET ILWR=1 IF OUTPUT REQUIRED, OTHERWISE ILWR=0	AG 640
C			AG 650
C	IERL	- ERROR FLAG =0 NO ERRORS	AG 660
C		9 CRITICAL RADIUS TOO SMALL	AG 670
C	**OUTPUT		AG 680
C	FPM	- FLOW FACTOR FOR MONOPOLE SOURCE DISTRIBUTION	AG 690
C	FPD	- FLOW FACTOR FOR S.I. DIPOLE SOURCE DISTRIBUTION	AG 700
C	FPQ	- FLOW FACTOR FOR S.I. QUADRUPOLE SOURCE DISTRIBUTION	AG 710
C		(S.I. = STATISTICALLY ISOTROPIC)	AG 720
C			AG 730
C	REMARKS		AG 740
C		AXIAL SOURCE CONVECTION AND COHERENCE EFFECTS ARE NOT	AG 750
C		INCLUDED HERE BUT MAY BE SIMULATED THROUGH A MODIFIED	AG 760
C		DOPPLER FREQUENCY SHIFT WITH ANGLE.	AG 770
C			AG 780
C			AG 790
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED		AG 800
C	DSETUP		AG 810
C	SUB2		AG 820
C	AXIAL		AG 830
C	SLOC		AG 840
C	VELT		AG 850
C	ERF		AG 860
C	CRIT		AG 870
C	RABC		AG 880
C	CBESL1		AG 890
C	CBESL2		AG 900
C	IDERY		AG 910
C	MPCL		AG 920
C	AFCT		AG 930
C	FCT		AG 940
C	OUTP		AG 950
C	COEF		AG 960
C	TRANS		AG 970
C	WRCAL		AG 980
C	TCON		AG 990
C	TSIGN		AG1000
C	RADCSD		AG1010
C	INTRAP		AG1020
C	SRPSD		AG1030
C	BESI		AG1040
C	QTFG		AG1050
C			AG1060
C	ERROR STOPS		AG1070
C	0	- FLOW PARAMETER OUTSIDE ALLOWED RANGE	AG1080
C	1	- FREQUENCY OR ANGLE OUTSIDE ALLOWED RANGE	AG1090
C	2	- INTEGRATION FAILURE IHLF=11	AG1100
C	3	- NUMBER OF INTEGRATION STEPS EXCEEDS DIMENSION	AG1110
C		OF ARRAYS YMI, YPU (EQUIVALENCED) FIRST MPCL CALL	AG1120
C	4	- DITTO THIRD AND FOURTH CALLS	AG1130
C	5	- DITTO FIFTH CALL	AG1140
C	*****		AG1150
C	SUBROUTINE LILLEY (NU, IOPT, IW, DELRAD, UICZ, TITZ, GAMMA, KZRZ, THETZ, ET		AG1160
C	IAIN, RSW, ALTB, BLTB, ILWR, FPM, FPD, FPQ, IERL)		AG1170

DIMENSION D(50),ID(50)	AG1180
COMMON/FOURTN/US(24)	AG1190
REAL KZRZ	AG1200
IERL=0	AG1210
GO TO (10,60,70), IOPT	AG1220
10 CONTINUE	AG1230
C FIND NEAREST STANDARD SOURCE RADIAL POSITION	AG1240
DO 20 I=1,24	AG1250
ISRL=I	AG1260
IF (ETAIN.GT.US(I)) GO TO 30	AG1270
20 CONTINUE	AG1280
30 CONTINUE	AG1290
CALL DSETUP (NU,IOPT,IW,DELRAD,UICZ,TITZ,GAMMA,KZRZ,THETZ,ISRL,ETA	AG1300
1IN,RSW,ALTB,BLTB,D,ID,ILWR)	AG1310S
CALL SUB2 (D,ID)	AG1320
FPM=D(31)	AG1330S
FPD=D(32)	AG1340
FPQ=D(33)	AG1350
IF (ISRL.LE.1) GO TO 40	AG1360
FACL=(ETAIN-US(ISRL-1))/(US(ISRL)-US(ISRL-1))	AG1370
FPM=D(41)+(FPM-D(41))*FACL	AG1380
FPD=D(42)+(FPD-D(42))*FACL	AG1390
FPQ=D(43)+(FPQ-D(43))*FACL	AG1400
40 CONTINUE	AG1410
IERL=ID(41)	AG1420
IF (ILWR.EQ.0) GO TO 50	AG1430
WRITE (IW,90) IERL,FPM,FPD,FPQ	AG1440
50 CONTINUE	AG1450*
RETURN	AG1460
60 CONTINUE	AG1470
70 CONTINUE	AG1480
ISRL=0	AG1490
CALL DSETUP (NU,IOPT,IW,DELRAD,UICZ,TITZ,GAMMA,KZRZ,THETZ,ISRL,ETA	AG1500
1IN,RSW,ALTB,BLTB,D,ID,ILWR)	AG1510S
CALL SUB2 (D,ID)	AG1520
FPM=D(36)	AG1530S
FPD=D(37)	AG1540
FPQ=D(38)	AG1550
IERL=ID(41)	AG1560
IF (ILWR.EQ.0) GO TO 80	AG1570
WRITE (IW,90) IERL,FPM,FPD,FPQ	AG1580
80 CONTINUE	AG1590*
RETURN	AG1600
C 90 FORMAT (1X,I5,3E13,6)	AG1610
END	AG1620
	AG1630
	AG1640-

*DECK DSETUP	
SUBROUTINE DSETUP (NU,IPT,IV,DELRAD,UICZ,TITZ,GAMMA,KZRZ,THETZ,IS	AM 10
JRL,ETAIN,RSW,ALTB,BLTB,D,ID,ILWR)	AM 20
REAL KZRZ	AM 30
DIMENSION D(1),ID(1)	AM 40
DATA RTPI / 2.506628 /	AM 50
ITEST=0	AM 60
PI=3.141593	AM 70
X1=7.616559*DELRAD	AM 80
IF (X1.GT.13.85) X1=13.85*(DELRAD/1.818535-1.0)*(26.0-13.85)/0.55	AM 90
ANG=THETZ*PI/180.0	AM 100
IF (DELRAD.LE.0.0.OR,DELRAD.GT.9.0) GO TO 70	AM 110
IF (UICZ.LT.0.0.OR,UICZ.GT.3.0) GO TO 70	AM 120
IF (TITZ.LE.0.0.OR,TITZ.GT.9.0) GO TO 70	AM 130
IF (GAMMA.LT.1.0.OR,GAMMA.GT.1.5) GO TO 70	AM 140
IF (KZRZ.LE.0.0.OR,KZRZ.GT.20.0) STOP 1	AM 150
IF (THETZ.LE.0.0.OR,THETZ.GE.180.) STOP 1	AM 160
D(1)=0.02*X1/8.0	AM 170
D(2)=.001	AM 180
D(3)=0.0	AM 190
D(4)=0.02	AM 200
D(5)=0.0	AM 210
D(6)=0.12*X1/8.0	AM 220
D(7)=.005	AM 230
D(8)=GAMMA	AM 240
D(9)=0.0	AM 250
D(10)=0.0	AM 260
IF (IPT.EQ.1) GO TO 20	AM 270
RTEST=0.5*X1*RSW/0.832554	AM 280
IF (RTEST.LT.D(1)) ITEST=1	AM 290
IF (RTEST.LT.D(1)) GO TO 20	AM 300
D(9)=RSW	AM 310
RS=0.0	AM 320
IF (ETAIN.LT.0.0001.OR,ETAIN.GT.0.9999) GO TO 10	AM 330
IF (DELRAD.LE.1.818535) RS=1.0*DELRAD*(SQRT(ABS(ALOG(-GPT(ETAIN))))	AM 340
1)+0.022*13.5/SQRT(PI))	AM 350
IF (DELRAD.GT.1.818535) RS=DELRAD*SQRT(2.0*EXP(-1.0)*ABS(ALOG(ETAI	AM 360
1N)))	AM 370
10 CONTINUE	AM 380
RSC=(RS-1.0)/X1	AM 390
D(10)=RSC	AM 400
20 CONTINUE	AM 410
D(11)=KZRZ	AM 420
D(12)=UICZ	AM 430
D(13)=TITZ	AM 440
D(14)=COS(ANG)	AM 450
D(15)=SIN(ANG)	AM 460
D(16)=X1	AM 470
D(17)=0.0	AM 480
D(18)=0.0	AM 490
D(19)=0.0	AM 500
D(20)=0.0	AM 510
D(21)=1.0	AM 520
D(22)=1.0	AM 530
D(23)=0.0	AM 540
D(24)=0.0	AM 550
D(25)=0.0	AM 560
D(26)=0.0	AM 570
GO TO (30,40,50), IPT	AM 580

30	CONTINUE	AH 590
	D(26)=0.0	AH 600
	GO TO 60	AH 610
40	CONTINUE	AH 620
	D(26)=0.0	AH 630
	IF (D(1).GE.10.0*0.5*X1*D(9)/0.832554) ITEST=1	AH 640
	IF (D(1).GE.10.0*0.5*X1*D(9)/0.832554) GO TO 60	AH 650
	D(26)=D(1)	AH 660
	GO TO 60	AH 670
50	CONTINUE	AH 680
	SLTB=(ALTB*X1+BLTB)/RTPI	AH 690
	IF (SLTB.LT.D(1)) ITEST=1	AH 700
	IF (SLTB.LT.D(1)) GO TO 60	AH 710
	D(26)=SLTB	AH 720
60	CONTINUE	AH 730
	ID(1)=5	AH 740
	ID(2)=IW	AH 750
	ID(3)=1	AH 760
	ID(4)=NU	AH 770
	ID(5)=0	AH 780
	ID(6)=0	AH 790
	ID(7)=1	AH 800
	ID(8)=0	AH 810
	ID(9)=0	AH 820
	ID(10)=12	AH 830
	ID(11)=0	AH 840
	ID(12)=0	AH 850
	ID(13)=0	AH 860
	ID(14)=0	AH 870
	ID(15)=0	AH 880
	ID(16)=82	AH 890
	ID(17)=ISRL	AH 900
	ID(18)=0	AH 910
	ID(25)=0	AH 920
	ID(26)=ILWR	AH 930
	IF (IOPT.EQ.2.OR.IOPT.EQ.3.AND.ITEST.EQ.0) ID(25)=1	AH 940
	IF (ITEST.NE.0) WRITE (IW,80) RSW,ALTB,BLTB	AH 950*
	RETURN	AH 960
70	CONTINUE	AH 970
	WRITE (IW,90) DELRAD,UICZ,TITZ,GAMMA	AH 980*
	STOP	AH 990
		AH1000
C	80 FORMAT (1X,"RSW,ALTB,BLTB",3E13.6,"TOO SMALL,OPTION 1 ASSUMED")	AH1010
	90 FORMAT (1X,"FLOW PARAMETERS OUTSIDE ALLOWED RANGE",4E13.6)	AH1020
	END	AH1030-

*DECK SUB2		
SUBROUTINE SUB2 (D,ID)		AI 10
EXTERNAL FCT,AFCT,OUTP		AI 20
DIMENSION D(1),ID(1)		AI 30
DIMENSION PRMT(8),Y(4),DERY(4),AUX(16,4),A(4,4),XOS(40),AMP(3)		AI 40
DIMENSION APLUG(3),IER(2),TIJ(7,40),YMI(450,5),TX(7)		AI 50
DIMENSION PRS(40),PQ(40),PD(40)		AI 60
DIMENSION PA(40)		AI 70
COMPLEX CMPLX,CSORT		AI 80
COMPLEX JSR,CAMP(2),BET1,BET2,STP1,STP2,RADM,BCNS,RPRES		AI 90
COMPLEX KRO,KRD,BCWS,CPLUG(2),TRN,TRRN		AI 100
COMPLEX ST1(40),BE1(40),BET1D		AI 110
COMPLEX ST2(40),BE2(40),BET2D		AI 120
COMPLEX TRFN,TFFN		AI 130
COMPLEX SAV		AI 140
REAL KW,M,M1,KWS		AI 150
COMMON YPU(450,5)		AI 160
C YPU IN OUTP,RADCSD		AI 170
C NMP BELOW IS MAX FIRST DIMENSION		AI 180
C NMP IN YMI ABOVE		AI 190
COMMON/CI/ IR,IW,NOUT,ICHECK		AI 200
COMMON/BJ/ M,KW,CANG,PI,BV,CV,TJR,G		AI 210
COMMON/CRIT/ICC,RC,XMC(16),XTC(16),YCR		AI 220
COMMON/BN/ NGE0,NCJ,NUT		AI 230
COMMON/ER/ IERX		AI 240
C *** FIX STEP SIZE MOD		AI 250
COMMON/FIX/ JFIXSS		AI 260
COMMON/ FJET/IFJ,FJUT,FJTT,FJRT,FJBV,FJCV		AI 270
COMMON/BUG/ IDBUG		AI 280
COMMON/STYPE/ MTPS		AI 290
COMMON /SRDCSD/ SAV(450)		AI 300
EQUIVALENCE (YPU(1,1),YMI(1,1))		AI 310
NDIM=4		AI 320
ICC=3		AI 330
NMP=450		AI 340
PI=3.141593		AI 350
TEMP=.25		AI 360
JSR=(0.,1.)		AI 370
DO 10 JJ=1,8		AI 380
10 PRMT(JJ)=0.		AI 390
DO 20 I=1,16		AI 400
20 AUX(I,1)=0.0		AI 410
C		AI 420
PRMT(3)=-D(1)		AI 430
PRMT(4)=D(2)		AI 440
PRMT(7)=D(3)		AI 450
DFC=D(4)		AI 460
ROX=D(5)		AI 470
RC=D(6)		AI 480
ECON=D(7)		AI 490
G=D(8)		AI 500
RSW=D(9)		AI 510
RSC=D(10)		AI 520
KW=D(11)		AI 530
M=D(12)		AI 540
TJR=D(13)		AI 550
CANG=D(14)		AI 560
SANG=D(15)		AI 570
X1=D(16)		AI 580

BV=D(17)	AI 590
TCOR=D(18)	AI 600
DCOR=D(19)	AI 610
FJUT=D(20)	AI 620
FJTT=D(21)	AI 630
FJRT=D(22)	AI 640
FJBV=D(23)	AI 650
FJCV=D(24)	AI 660
FJFF=D(25)	AI 670
IW=ID(2)	AI 680
NGEO=ID(3)	AI 690
MTYPS=ID(4)	AI 700
NUT=ID(5)	AI 710
IERX=ID(6)	AI 720
IMX=ID(7)	AI 730
IWB=ID(8)	AI 740
JFIXSS=ID(9)	AI 750
JCC=ID(10)	AI 760
ISG=ID(11)	AI 770
IDBUG=ID(12)	AI 780
NSLOX=ID(13)	AI 790
NSLO=ID(14)	AI 800
NCJN=ID(15)	AI 810
NCJM=ID(16)	AI 820
ISRL=ID(17)	AI 830
IFJ=ID(18)	AI 840
IO=ID(26)	AI 850
IF (PRMT(3),EQ,0,0) RETURN	AI 860
NCJMX=NCJM+1	AI 870
NCJNX=NCJN+1	AI 880
	AI 890
	AI 900
CALL AXIAL (X1,BV,CV)	AI 910S
	AI 920
	AI 930
SET UP RADIAL SOURCE LOCATIONS IF REQUIRED	AI 940
IF (NSLOX.GT.0) GO TO 40	AI 950
CALL SLOC (DFC,X1,BV,CV,G,XOS,NSLO)	AI 960S
IF (ISRL.LE.0) GO TO 30	AI 970
IF (CV,EQ,0,0) NSLO=ISRL	AI 980
IF (CV,NE,0,0) NSLO=ISRL+NSLO-24	AI 990
30 CONTINUE	AI1000
40 CONTINUE	AI1010
	AI1020
	AI1030
FJPC=(1.-FJUT)*(1.-FJUT)/FJTT	AI1040
ROI=0.	AI1050
XVS=DFC	AI1060
FJSW=0	AI1070
DO 80 IVS=1,1000	AI1080
RO=XVS	AI1090
CALL VELT (XVS,M,TJR,BV,CV,G,XMC,XTC,3)	AI1100S
IF (IVS,EQ,1) M1=XMC(1)	AI1110
IF (IVS,EQ,1) T1=XTC(1)	AI1120
IF (IO,EQ,0) GO TO 50	AI1130
IF (NUT,GT,0) WRITE (IW,460) XVS,(XMC(I),I=1,3),(XTC(I),I=1,3)	AI1140*
50 CONTINUE	AI1150
IF (XMC(1).GE..99) GO TO 70	AI1160
TPRO=(1.-XMC(1))*(1.-XMC(1))/XTC(1)	AI1170

IF (FJ3W,NE.0.OR,IFJ,EQ.0) GO TO 60	AI1180
IF (ABS(TPRO-FJPC),LT.1,E-04) ROI=XVS	AI1190
IF (ABS(TPRO-FJPC),LT.1,E-04) FJSW=1	AI1200
60 CONTINUE	AI1210
IF (ABS(TPRO-1.),LT.,1E-03) GO TO 90	AI1220
70 CONTINUE	AI1230
XVS=XVS+FJRT*DFC	AI1240
80 CONTINUE	AI1250
90 CONTINUE	AI1260
IF (M,EQ.0.0.AND,TJR,EQ.1.) RO=ROX	AI1270
IF (XOS(1),LT,DFC) DFC=XOS(1)*PRMT(3)/2048.	AI1280
IF (XOS(NSLO),GT,RO) RO=XOS(NSLO)-PRMT(3)/2048.	AI1290
RO=DFC+IFIX(RO/PRMT(3))*PRMT(3)	AI1300
IF (ROX,NE.0.,AND,ROX,GT,XOS(NSLO)) ROI=ROX	AI1310
IF (IFJ,EQ.0.AND,ROI,NE.0.) RO=ROI	AI1320
IF (IFJ,EQ.0.AND,ROI,EQ.0.) ROI=RO	AI1330
IF (IO,EQ.0) GO TO 100	AI1340
IF (NUT,GT.0) WRITE (IW,440) X1,DFC,ROI,RO,RC	AI1350*
100 CONTINUE	AI1360
C	AI1370
C	AI1380
XKW2=KW*KW	AI1390
ICC=2	AI1400
DO 120 MS=1,NSLO	AI1410
CALL VELT (XOS(MS),M,TJR,BV,CV,G,AMP,APLUG,ICC)	AI1420S
PRS(MS)=1.-AMP(1)*CANG	AI1430
ID(41)=0	AI1440
IF (ABS(PRS(MS)),LT.1,E-30) ID(41)=11	AI1450
IF (ABS(PRS(MS)),LT.1,E-30) GO TO 420	AI1460
PRS(MS)=PRS(MS)*PRS(MS)/APLUG(1)	AI1470
PQ(MS)=(CANG*CANG-PRS(MS))*KW*KW	AI1480
PD(MS)=-APLUG(2)/APLUG(1)-2.*AMP(2)*CANG/(1.-AMP(1)*CANG)	AI1490
PA(MS)=-APLUG(2)/APLUG(1)	AI1500
IF (ISG,EQ.1) PA(MS)=0.0	AI1510
IF (ISG,EQ.1) PD(MS)=0.	AI1520
IF (IO,EQ.0) GO TO 110	AI1530
IF (NUT,GT.0) WRITE (IW,440) XOS(MS),AMP(1),APLUG(1),PRS(MS),PQ(MS)	AI1540*
1),PD(MS)	AI1550
110 CONTINUE	AI1560
120 CONTINUE	AI1570
C	AI1580
C	AI1590
ICC=3	AI1600
YCR=0.	AI1610
ICRIT=0	AI1620
CTEST=1.-M1*CANG	AI1630
IF (CTEST,GT.0.0) GO TO 140	AI1640
ICRIT=1	AI1650
YCR=1.	AI1660
CALL CRIT (YCR,M,TJR,BV,CV,G,CANG)	AI1670S
ICC=JCC	AI1680
CALL VELT (YCR,M,TJR,BV,CV,G,XMC,XTC,ICC)	AI1690S
ICC=3	AI1700
IF (IO,EQ.0) GO TO 130	AI1710
IF (NUT,GT.0) WRITE (IW,440) YCR,(XMC(KI),KI=1,JCC)	AI1720*
IF (NUT,GT.0) WRITE (IW,440) YCR,(XTC(KI),KI=1,JCC)	AI1730*
130 CONTINUE	AI1740
ID(41)=0	AI1750
IF (YCR,LT.(DFC-PRMT(3)*RC)) ID(41)=9	AI1760

	IF (YCR,LT,(DFC-PRMT(3)*RC)) GO TO 420	AI1770
160	CONTINUE	AI1780
C		AI1790
C	KRO=CMPLX(KW*SANG,0.0)	AI1800
	DUM=CTEST*CTEST/T1-CANG*CANG	AI1810
	KRD=CMPLX(KW*KW*DUM,0.0)	AI1820
	KRD=CSQRT(KRD)	AI1830
	IF (DUM,LT,0.0) KRD=-KRD	AI1840
	IF (NCJNX,GT,1) GO TO 160	AI1850
	DO 150 NTS=1,7	AI1860
	DO 150 MS=1,NSLO	AI1870
150	TIJ(NTS,MS)=0.	AI1880
160	CONTINUE	AI1890
	MXOS=1	AI1900
C		AI1910
C		AI1920
	DO 370 NCJX=NCJNX,NCJMX	AI1930
	ICHECK=0	AI1940
	NCJ=NCJX-1	AI1950
	SCALE=10.**(-NCJ)	AI1960
C		AI1970
C		AI1980
	BCWS=(0.0,0.0)	AI1990
	IF (NGEO,EQ,1) GO TO 170	AI2000
	RADM=-JSR*KRO	AI2010
	BCNS=JSR*KRD	AI2020
	BCWS=(0.0,0.0)	AI2030
C	ORIGIN AT EDGE OF SINGLE SHEAR LAYER	AI2040
	RPRES=-1./(2.*JSR*KRO)	AI2050
	IERDS=0	AI2060
	GO TO 180	AI2070
170	CONTINUE	AI2080
	CALL RABC (NCJ,RO,DFC,KRO,KRD,RADM,BCNS,BCWS,RPRES,IERDS)	AI2090
180	CONTINUE	AI2100S
	DUM=T1/(CTEST*CTEST)	AI2110
	BCNS=DUM*BCNS	AI2120
	BCWS=DUM*BCWS	AI2130
	IF (IO,EQ,0) GO TO 190	AI2140
	IF (NUT,GT,0) WRITE (IW,440) KRO,KRD,BCWS,RADM,BCNS,RPRES	AI2150
190	CONTINUE	AI2160*
	ID(41)=0	AI2170
	IF (IERDS,NE,0) ID(41)=10	AI2180
	IF (IERDS,NE,0) GO TO 420	AI2190
C		AI2200
C		AI2210
	NOUT=0	AI2220
C	WRONSK = REMOVED	AI2230
	PRMT(3)=-PRMT(3)	AI2240
	PRMT(1)=DFC	AI2250
	PRMT(2)=ROI	AI2260
	IF (ICRIT,EQ,0) GO TO 200	AI2270
	IF (PRMT(2),GT,(YCR-RC)) PRMT(2)=YCR-RC	AI2280
200	CONTINUE	AI2290
	PRMT(6)=XOS(MXOS)-2.*PRMT(3)	AI2300
	IF (MXOS,EQ,1) PRMT(6)=DFC	AI2310
	PRMT(8)=XOS(NSLO)+2.*PRMT(3)	AI2320
	CALL IDERY (DERY,TEMP,NDIM,PRMT,ICC)	AI2330
	Y(1)=SCALE	AI2340S
		AI2350

	Y(2)=0.	AI2360
	Y(3)=REAL(BCNS)*Y(1)	AI2370
	Y(4)=0.	AI2380
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI2390
	IF (NGEO.EQ.0) Y(4)=AIMAG(BCNS)*Y(1)	AI2400
C	USE NEXT CARD FOR COMPLEX ANGLES	AI2410
C	Y(4)=AIMAG(BCNS)	AI2420
	CALL HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,XCU)	AI2430S
	IF (IHLF.GE.11) STOP 2	AI2440
	IF (NOUT.GT.NMP) STOP 3	AI2450
	IF (ICRIT.EQ.0) GO TO 240	AI2460
C		AI2470
C		AI2480
	DO 210 IZ=1,NDIM	AI2490
210	Y(IZ)=Y(IZ)+DERY(IZ)*(PRMT(2)-XCU)	AI2500
	CALL TRANS (Y,ST2,NDIM)	AI2510S
	IF (NOUT.GT.0) NOUT=NOUT-1	AI2520
	PRMT(1)=-PI	AI2530
	PRMT(2)=0.	AI2540
	PRMT(3)=PRMT(3)/(RC*2.**IHX)	AI2550
	PRMT(3)=PRMT(3)*PI	AI2560
	DO 220 IZ=1,NDIM	AI2570
220	DERY(IZ)=TEMP	AI2580
	ICC=JCC	AI2590
	CALL HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,XCU)	AI2600S
	IF (IHLF.GE.11) STOP 2	AI2610
	IF (NOUT.GT.NMP) STOP 3	AI2620
	DO 230 IZ=1,NDIM	AI2630
230	Y(IZ)=Y(IZ)-DERY(IZ)*XCU	AI2640
	CALL TRANS (Y,BE2,NDIM)	AI2650S
C		AI2660
C		AI2670
	ICC=3	AI2680
	PRMT(3)=RC*PRMT(3)*2.**IHX	AI2690
	PRMT(3)=PRMT(3)/PI	AI2700
	IF (NOUT.GT.0) NOUT=NOUT-1	AI2710
C		AI2720
C		AI2730
	PRMT(1)=YCR-RC	AI2740
C	WRONSK	AI2750
	PRMT(2)=ROI	AI2760
	PRMT(6)=XOS(MXOS)-2.*PRMT(3)	AI2770
	IF (PRMT(1).GT.PRMT(2)) PRMT(2)=PRMT(1)+PRMT(3)	AI2780
	CALL IDERY (DERY,TEMP,NDIM,PRMT,ICC)	AI2790S
	CALL HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,XCU)	AI2800S
	IF (IHLF.GE.11) STOP 2	AI2810
240	CONTINUE	AI2820
	NOUTM=NOUT	AI2830
	IF (NOUTM.GT.NMP) STOP 5	AI2840
	IF (IO.EQ.0) GO TO 250	AI2850
	IF (NUT.GT.0) WRITE (IW,450) NCJ,MXOS,NOUTP,NOUTM,ICHECK	AI2860*
250	CONTINUE	AI2870
C		AI2880
C		AI2890
	IF (IFJ.EQ.0) GO TO 260	AI2900
	PRMT(1)=XCU	AI2910
	PRMT(2)=RO	AI2920
	PRMT(3)=PRMT(3)*FIX(FJRT+FJFF)	AI2930
	PRMT(8)=0.	AI2940

CALL IDERY (DERY,TEMP,NDIM,PRMT,ICC)	AI2950S
CALL HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,XCU)	AI2960S
IF (IHLF,GE,11) STOP 2	AI2970
PRMT(3)=PRMT(3)/IFIX(FJRT+FJFF)	AI2980
260 CONTINUE	AI2990
C	AI3000
C	AI3010
NOUT=0	AI3020
PRMT(3)=-PRMT(3)	AI3030
DO 290 MS=MXOS,NSLO	AI3040
STEST=10.	AI3050
DO 270 ISE=1,NOUTM	AI3060
XTEST=ABS(YMI(ISE,1)-XOS(MS))	AI3070
IF (XTEST,GT,STEST) GO TO 280	AI3080
STEST=XTEST	AI3090
MMI=ISE	AI3100
270 CONTINUE	AI3110
280 CONTINUE	AI3120
IF (XOS(MS),LT,YMI(MMI,1)) MMI=MMI-1	AI3130
STP2=CMPLX(YMI(MMI,2),YMI(MMI,3))	AI3140
XINTP=(XOS(MS)-YMI(MMI,1))/(YMI(MMI+1,1)-YMI(MMI,1))	AI3150
STP2=(1.-XINTP)*STP2+XINTP*CMPLX(YMI(MMI+1,2),YMI(MMI+1,3))	AI3160
ST2(MS)=STP2	AI3170
BE1(MS)=(1.-XINTP)*SAV(MMI)+XINTP*SAV(MMI+1)	AI3180
BET2=CMPLX(YMI(MMI,4),YMI(MMI,5))	AI3190
BET2D=CMPLX(YMI(MMI+1,4),YMI(MMI+1,5))	AI3200
BET2=(1.-XINTP)*BET2+XINTP*BET2D	AI3210
BE2(MS)=BET2/ST2(MS)	AI3220
290 CONTINUE	AI3230
C	AI3240
C	AI3250
XN4=FLOAT(NCJ)	AI3260
XN4=XN4*XN4*XN4*XN4	AI3270
NCON=7*(MXOS-1)	AI3280
C	AI3290
WRONSK	AI3300
DO 300 IZ=1,4	AI3310
Y(IZ)=Y(IZ)+DERY(IZ)*(RO-XCU)	AI3320
300 CONTINUE	AI3330S
CALL WRCAL (NGEO,Y,RADM,RPRES,CAMP(1))	AI3340
C	AI3350
C	AI3360
IFLAG=0	AI3370S
IF (ID(25),GT,0) CALL RADCSO (IFLAG,NCJ,CAMP(1),D,ID,NOUTM,BV,CV)	AI3380
C	AI3390
C	AI3400
DO 340 MS=MXOS,NSLO	AI3410
XAV=XOS(MS)	AI3420
C	AI3430
EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI3440
IF (NGEO,EQ,0) XAV=1.	AI3450
CAMP(2)=ST2(MS)*CAMP(1)	AI3460
C	AI3470
THIS RESTRICTS FREQ. TO GT. 10, E-14	AI3480
C	AI3490
IF (ALOG10(CABS(CAMP(2)))-NCJ,LT,-30.) CAMP(2)=(0.,0.)	AI3500*
RCAMP=ABS(REAL(CAMP(2)))	AI3510
AICAMP=ABS(AIMAG(CAMP(2)))	AI3520
IF (IO,EQ,0) GO TO 310	AI3530
IF (RCAMP,LT,1.E-30,AND,AICAMP,LT,1.E-30) WRITE (IW,440) CAMP(2)	
310 CONTINUE	
IF (RCAMP,LT,1.E-30,AND,AICAMP,LT,1.E-30) CAMP(2)=(0.,0.)	
XAV2=XAV*XAV	

	XAV3=XAV*XAV2	AI3540
	XAV4=XAV2*XAV2	AI3550
	TRN=BE2(MS)*PRS(MS)/XAV	AI3560
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI3570
	TRRN=PQ(MS)+NCJ*NCJ/XAV2+TRN*(PD(MS)-NGEO/XAV)	AI3580
	IF (MTYPS,EQ.1) TRRN=PQ(MS)+NCJ*NCJ/XAV2+TRN*(PA(MS)-NGEO/XAV)	AI3590
	IF (MTYPS,EQ.3) GO TO 320	AI3600
C		AI3610
C	EXTRA INFO. FOR MTYPS,NE,3	AI3620
C	ICC=3	AI3630
	CALL VELT (XOS(MS),M,TJR,BV,CV,G,AMP,APLUG,ICC)	AI3640
	AMP(1)=1.-AMP(1)*CANG	AI3650S
	ST1(MS)=-CANG*AMP(2)/BE1(MS)	AI3660
	IF (ISG,EQ.1) ST1(MS)=(0.0,0.0)	AI3670
	IF (ISG,EQ.1) AMP(2)=0.	AI3680
	AMP(3)=-CANG*AMP(3)/AMP(1)	AI3690
	IF (ISG,EQ.1) AMP(3)=0.	AI3700
320	CONTINUE	AI3710
C		AI3720
C		AI3730
	TRC=CABS(TRN)	AI3740
	IF (MTYPS,EQ.1) TRC=CABS(TRN+ST1(MS))	AI3750
	TRC=TRC*TRC	AI3760
	TRRC=CABS(TRRN)	AI3770
	TRRC=TRRC*TRRC	AI3780
	TRR=2.*REAL(TRN)	AI3790
	TRFN=(TRN-1./XAV)/XAV	AI3800
	IF (MTYPS,EQ.1) TRFN=(TRN+ST1(MS)-1.0/XAV)/XAV	AI3810
	TRFC=CABS(TRFN)	AI3820
	TRFC=TRFC*TRFC	AI3830
	TFFN=(TRN-NCJ*NCJ/XAV)/XAV	AI3840
	TFFC=CABS(TFFN)	AI3850
	TFFC=TFFC*TFFC	AI3860
	CN=CABS(CAMP(2))	AI3870
	CN=CN*CN	AI3880
	IF (NCJ,GT.0) CN=2.*CN	AI3940
	TX(1)=CN	AI3950
	TX(2)=TRC*CN	AI3960
	TX(3)=TRRC*CN	AI3970
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI3980
	IF (NGEO,EQ.0) GO TO 330	AI3990
	TX(4)=NCJ*NCJ*CN/XAV2	AI4000
	TX(5)=NCJ*NCJ*TRFC*CN	AI4010
	TX(6)=TFFC*CN	AI4020
	TX(7)=CABS(TRN)*CABS(TRN)*CN	AI4030
330	CONTINUE	AI4040
	CALL TCON (MS,NCJX,NCJNX,TIJ,TX,ECON,NCON,MXOS)	AI4050S
	IF (NCON,EQ.7*NSLO) GO TO 380	AI4060
340	CONTINUE	AI4070
C		AI4080
C		AI4090
	IF (IFIX(PRMT(7)),EQ.0) GO TO 370	AI4100
	IF (IO,EQ.0) GO TO 360	AI4110
	DO 350 MS=1,NSLO	AI4120

	WRITE (IW,440) (TIJ(NTS,MS),NTS=1,7)	AI4130*
350	CONTINUE	AI4140
360	CONTINUE	AI4150
370	CONTINUE	AI4160
C		AI4170
C		AI4180
380	CONTINUE	AI4190
	TX(1)=0.0	AI4200
	SIPD=0.0	AI4210
	TISO=0.0	AI4220
	DO 410 MS=1,NSLO	AI4230
C	SAVE TX(1),SIPD,TISO FOR INTERPOLATION IN S.R. LILLEY	AI4240
	D(41)=TX(1)	AI4250
	D(42)=SIPD	AI4260
	D(43)=TISO	AI4270
	CALL TSIGN (MS,TIJ)	AI4280S
	TX(1)=10.*ALOG10(TIJ(1,MS))	AI4290
	TX(2)=10.*ALOG10(TIJ(2,MS)/(1.5*XKW2))	AI4300
	TX(3)=10.*ALOG10(TIJ(3,MS)/(1.375*XKW2*XKW2))	AI4310
C	EXTRA MOD NEEDED HERE IF 2-D JET CASE TO BE INCLUDED	AI4320
	IF (NGEO,EQ.0) GO TO 390	AI4330
	TX(4)=10.*ALOG10(TIJ(4,MS)/(1.5*XKW2))	AI4340
	TX(5)=10.*ALOG10(TIJ(5,MS)/(1.125*XKW2*XKW2))	AI4350
	TX(6)=10.*ALOG10(TIJ(6,MS)/(1.375*XKW2*XKW2))	AI4360
	TX(7)=10.0*ALOG10(TIJ(7,MS)/(0.5*XKW2))	
390	CONTINUE	AI4370
	TISO=TIJ(3,MS)+TIJ(6,MS)+2.*TIJ(5,MS)	AI4380
	TISO=TISO*XKW2*XKW2*(CANG**4)+TIJ(1,MS)+2.*XKW2*CANG*CANG*(TIJ(2,MS)+TIJ(4,MS))	AI4390
	TISO=10.*ALOG10(TISO/(XKW2*XKW2))	AI4400
	TISO=TISO+TCOR	AI4410
	SIPD=TIJ(7,MS)+TIJ(4,MS)+XKW2*CANG*CANG*TIJ(1,MS)	AI4420
	SIPD=10.*ALOG10(SIPD/XKW2)	AI4430
	SIPD=SIPD+DCOR	AI4440
	ICC=1	AI4450
	SMACH=1.	AI4460
	IF (M,NE.0.) SMACH=M	AI4470
	CALL VELT (XOS(MS),SMACH,TJR,BV,CV,G,AMP,APLUG,ICC)	AI4480
C	VEL. AND TEMP. MUST BE LESS THAN 10. SOURCE POS. LESS THAN 99.	AI4490S
	IF (IO,EQ.0) GO TO 400	AI4500
	WRITE (IW,430) XOS(MS),AMP(1),APLUG(1),(TX(NTS),NTS=1,7),TISO,SIPD	AI4510
400	CONTINUE	AI4520*
C	JAN76	AI4530
410	CONTINUE	AI4540
	D(31)=TX(1)	AI4550
	D(32)=SIPD	AI4560
	D(33)=TISO	AI4570
C		AI4580
C		AI4590
C	OBTAIN NON-COMPACT FLOW FACTORS	AI4600
	IFLAG=1	AI4610
	IF (ID(25),GT.0) CALL RADCSO (IFLAG,NCJ,CAMP(1),D,ID,NOUTH,BV,CV)	AI4620
C		AI4630S
C		AI4640
		AI4650
420	CONTINUE	AI4660
	RETURN	AI4670
C		AI4680
430	FORMAT (1X,F8.4,2F7.4,9F7.2;	AI4690
440	FORMAT (1X,6E13.6)	AI4700
450	FORMAT (1X,3HNCJ,5I5)	AI4710
460	FORMAT (1X,7E11.4)	AI4720
	END	AI4730-

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•DECK AXIAL
SUBROUTINE AXIAL (X1,BV,CV)
IF (X1.GT.13.85) GO TO 10
BV=X1/13.5
CV=-.022*X1
GO TO 20
10 CONTINUE
BV=1.0*(X1-13.85)*0.55/(26.0-13.85)
BV=BV*1.559874
CV=0.
20 CONTINUE
RETURN
END

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AJ 10
AJ 20
AJ 30
AJ 40
AJ 50
AJ 60
AJ 70
AJ 80
AJ 90
AJ 100
AJ 110
AJ 120-

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*DECK SLOC	
SUBROUTINE SLOC (XS,X1,BV,CV,G,XOS,NSLO)	AK 10
DIMENSION XOS(1)	AK 20
DIMENSION U(40)	AK 30
DATA U(1),U(2),U(3),U(4),U(5),U(6),U(7),U(8),U(9),U(10),U(11),	AK 40
1U(12),U(13),U(14),U(15),U(16),U(17),U(18),U(19),U(20),U(21),U(22),	AK 50
2 U(23),U(24)/.99,.98199,.968865,.9481,.91859,.87741,.82377,	AK 60
3 .757455,.67936,.67,.66295,.6,.591905,.5,.408098,.3206435,	AK 70
4 .2425485,.1762325,.1225905,.081409,.051541,.0311374,.0180080,	AK 80
5 .01/	AK 90
IF (CV.EQ.0.) GO TO 70	AK 100
IF (X1.GT.8.01) GO TO 40	AK 110
RMDEL=1.+0.022*X1-.12185*X1	AK 120
XOS(1)=2.*XS	AK 130
RDEL=(RMDEL-XOS(1))/9.	AK 140
DO 10 IDEL=1,9	AK 150
XOS(IDEL+1)=XOS(IDEL)+RDEL	AK 160
10 CONTINUE	AK 170
RDEL=.2437*X1/20.	AK 180
DO 20 IDEL=10,17	AK 190
XOS(IDEL+1)=XOS(IDEL)+RDEL	AK 200
20 CONTINUE	AK 210
XOS(19)=1.-.001007875*X1	AK 220
XOS(20)=1.	AK 230
XOS(21)=1.+0.00872375*X1	AK 240
XOS(22)=XOS(18)+RDEL	AK 250
DO 30 IDEL=22,32	AK 260
XOS(IDEL+1)=XOS(IDEL)+RDEL	AK 270
30 CONTINUE	AK 280
NSLO=33	AK 290
RETURN	AK 300
40 CONTINUE	AK 310
XOS(1)=2.0*XS	AK 320
RDEL=0.2437*X1/20.0	AK 330
NMAX=(1.0+0.022*X1-XOS(1))/RDEL	AK 340
XOS(NMAX+5)=1.0+0.022*X1	AK 350
XOS(2)=XOS(NMAX+5)-NMAX*RDEL	AK 360
NDUM=NMAX-1	AK 370
DO 50 IDUM=2,NDUM	AK 380
XOS(IDUM+1)=XOS(IDUM)+RDEL	AK 390
50 CONTINUE	AK 400
XOS(NMAX+1)=1.0-0.001007875*X1	AK 410
XOS(NMAX+2)=1.0	AK 420
XOS(NMAX+3)=1.0+0.00872375*X1	AK 430
XOS(NMAX+4)=XOS(NMAX)+RDEL	AK 440
NDMIN=NMAX+5	AK 450
NDMAX=NMAX+14	AK 460
DO 60 IDUM=NDMIN,NDMAX	AK 470
XOS(IDUM+1)=XOS(IDUM)+RDEL	AK 480
60 CONTINUE	AK 490
NSLO=NMAX+15	AK 500
RETURN	AK 510
70 CONTINUE	AK 520
NSLO=24	AK 530
DO 80 I=1,NSLO	AK 540
XOS(I)=BV*SQRT(ALOG(1./U(I)))	AK 550
IF (XOS(I).LE.XS) XOS(I)=1.1*XS	AK 560
80 CONTINUE	AK 570
RETURN	AK 580
END	AK 590

*DECK VELT	AL 10
SUBROUTINE VELT (X,M,TJR,BV,CV,G,XMC,XTC,ICC)	AL 20
DIMENSION XMC(1)	AL 30
DIMENSION XTC(1)	AL 40
COMMON/ FJET/IFJ,FJUT,FJTT,FJRT,FJBV,FJCV	AL 50
REAL M	AL 60
DATA SPI/1.7724538/	AL 70
VRT=0.0	AL 80
GMM=(G-1.)/2.	AL 90
TJX=TJR-FJTT+GMM*(M-FJUT)*(M-FJUT)	AL 100
FJTJX=FJTT-(1.-GMM*FJUT*FJUT)	AL 110
IF (CV.EQ.0.) GO TO 180	AL 120
C	AL 130
XN=(ABS(X)-1.*CV)/BV	AL 140
IF (XN.GT.10.) GO TO 10	AL 150
IF (XN.LT.-10.) GO TO 70	AL 160
VR=0.5*(1.-ERF(XN))	AL 170
XMC(1)=(M-FJUT)*VR	AL 180
XTC(1)=FJTT-GMM*XMC(1)*XMC(1)+VR*TJX	AL 190
IF (ICC.EQ.1.AND.IFJ.EQ.0) RETURN	AL 200
IF (IFJ.EQ.0) GO TO 90	AL 210
GO TO 30	AL 220
C	AL 230
10 DO 20 I=1,ICC	AL 240
XTC(I)=0.	AL 250
20 XMC(I)=0.0	AL 260
XTC(I)=1.	AL 270
IF (IFJ.EQ.0) GO TO 60	AL 280
C	AL 290
30 CONTINUE	AL 300
XX=(ABS(X)/FJRT-1.*FJCV)/FJBV	AL 310
IF (XX.GT.10.) GO TO 60	AL 320
IF (XX.LT.-10.) GO TO 50	AL 330
VRT=0.5*(1.-ERF(XX))	AL 340
XMC(1)=FJUT*VRT*XMC(1)	AL 350
IF (XTC(1).EQ.1.0) XTC(1)=1.0-GMM*XMC(1)*XMC(1)+VRT*FJTJX	AL 360
40 CONTINUE	AL 370
IF (ICC.EQ.1) GO TO 60	AL 380
IF (XN.GT.10..AND.CV.NE.0.) GO TO 60	AL 390
IF (XN.GT.4..AND.CV.EQ.0.) GO TO 60	AL 400
IF (CV.EQ.0.) GO TO 210	AL 410
GO TO 90	AL 420
C	AL 430
50 CONTINUE	AL 440
XMC(1)=FJUT*XMC(1)	AL 450
IF (XTC(1).EQ.1.0) XTC(1)=FJTT	AL 460
VRT=1.	AL 470
GO TO 40	AL 480
60 CONTINUE	AL 490
RETURN	AL 500
C	AL 510
70 XMC(1)=M	AL 520
XTC(1)=TJR	AL 530
IF (ICC.EQ.1) RETURN	AL 540
C	AL 550
	AL 560
	AL 570
	AL 580

DO 80 I=2,ICC	AL 590
XTC(I)=0.	AL 600
80 XMC(I)=0.0	AL 610
RETURN	AL 620
C	AL 630
C	AL 640
90 CONTINUE	AL 650
XMC(1)=VR	AL 660
XMC(2)=1.	AL 670
IF (ICC.GT.2) XMC(3)=2.*XN	AL 680
N=ICC-1	AL 690
IF (N=2) 120,120,100	AL 700
100 DO 110 I=3,N	AL 710
110 XMC(I+1)=2.*XN*XMC(I)-2.*(I-2)*XMC(I-1)	AL 720
120 EP=EXP(-XN*XN)	AL 730
FACT=EP/SPI	AL 740
DO 130 I=2,ICC	AL 750
FACT=-FACT/BV	AL 760
130 XMC(I)=FACT*XMC(I)	AL 770
FORM DER. OF VEL. RATIO	AL 780
DO 150 ND=2,ICC	AL 790
XTC(ND)=0.	AL 800
AFAC=1.	AL 810
DO 140 NDR=1,ND	AL 820
INDR=ND-NDR+1	AL 830
XTC(ND)=XTC(ND)+AFAC*XMC(INDR)*XMC(NDR)	AL 840
AFAC=AFAC*(ND-NDR)/NDR	AL 850
140 CONTINUE	AL 860
150 CONTINUE	AL 870
DO 160 ND=2,ICC	AL 880
XTC(ND)=-GMM*(M-FJUT)*(M-FJUT)*XTC(ND)+XMC(ND)*TJX	AL 890
160 CONTINUE	AL 900
DO 170 I=1,ICC	AL 910
XMC(I)=(M-FJUT)*XMC(I)	AL 920
170 CONTINUE	AL 930
XMC(1)=FJUT*VRT*XMC(1)	AL 940
C FJ GRADIENTS NOT INCLUDED	AL 950
RETURN	AL 960
C	AL 970
C	AL 980
C	AL 990
180 CONTINUE	AL1000
XN=X/BV	AL1010
IF (XN.GT.4.) GO TO 190	AL1020
VR=EXP(-XN*XN)	AL1030
XMC(1)=(M-FJUT)*VR	AL1040
XTC(1)=FJUT-GMM*XMC(1)*XMC(1)+VR*TJX	AL1050
IF (ICC.EQ.1.AND. IFJ.EQ.0) RETURN	AL1060
IF (IFJ.EQ.0) GO TO 210	AL1070
GO TO 30	AL1080
C	AL1090
C	AL1100
190 DO 200 I=1,ICC	AL1110
XTC(I)=0.	AL1120
200 XMC(I)=0.	AL1130
XTC(1)=1.	AL1140
IF (IFJ.EQ.0) RETURN	AL1150
GO TO 30	AL1160
C	AL1170
C	

210	CONTINUE	AL1180
	XMC(1)=1.	AL1190
	XMC(2)=2.*XN	AL1200
	IF (ICC-2) 240,240,220	AL1210
220	DO 230 I=3,ICC	AL1220
230	XMC(I)=2.*XN*XMC(I-1)-2.*(I-2)*XMC(I-2)	AL1230
240	FACT=VR	AL1240
	DO 250 I=1,ICC	AL1250
	XMC(I)=FACT*XMC(I)	AL1260
250	FACT=-FACT/BV	AL1270
	DO 270 ND=2,ICC	AL1280
	XTC(ND)=0.	AL1290
	AFAC=1.	AL1300
	DO 260 NDR=1,ND	AL1310
	INDR=ND-NDR+1	AL1320
	XTC(ND)=XTC(ND)+AFAC*XMC(INDR)*XMC(NDR)	AL1330
	AFAC=AFAC*(ND-NDR)/NDR	AL1340
260	CONTINUE	AL1350
270	CONTINUE	AL1360
	DO 280 ND=2,ICC	AL1370
	XTC(ND)=-GMM*(M-FJUT)*(M-FJUT)*XTC(ND)+XMC(ND)*TJX	AL1380
280	CONTINUE	AL1390
	DO 290 I=1,ICC	AL1400
	XMC(I)=(M-FJUT)*XMC(I)	AL1410
290	CONTINUE	AL1420
	XMC(1)=FJUT*VRT+XMC(1)	AL1430
C	FJ GRADIENTS NOT INCLUDED	AL1440
	RETURN	AL1450
	END	AL1460-

•DECK ERF		
FUNCTION ERF(XN)		AM 10
C ERROR FUNCTION RATIONAL APPROXIMATION 7.1.27 OF NBS(ABRAMOWITZ)		AM 20
DATA SPI,A1,A2,A3,A4/1.7724538,.278393,.230389,.000972,.078108/		AM 30
XA=ABS(XN)		AM 40
X1=XA		AM 50
X2=XA*X1		AM 60
X3=XA*X2		AM 70
X4=XA*X3		AM 80
XRF=1.+A1*X1+A2*X2+A3*X3+A4*X4		AM 90
ERF=1.-1./(XRF*XRF*XRF*XRF)		AM 100
IF (XN.LT.0.) ERF=-ERF		AM 110
RETURN		AM 120
END		AM 130-

*DECK CRIT	
SUBROUTINE CRIT (Y,M,TJR,BV,CV,G,CANG)	AN 10
DIMENSION YMC(3)	AN 20
DIMENSION YTC(3)	AN 30
ICC=3	AN 40
DO 10 N=1,10	AN 50
CALL VELT (Y,M,TJR,BV,CV,G,YMC,YTC,ICC)	AN 60\$
YX=Y*(1.-YMC(1)*CANG)/(YMC(2)*CANG)	AN 70
IF (ABS((YX-Y)/YX).LT..001) GO TO 20	AN 80
Y=YX	AN 90
10 CONTINUE	AN 100
Y=0.	AN 110
20 RETURN	AN 120
END	AN 130-

*DECK RABC	
SUBROUTINE RABC (N,RO,DFC,KRO,KRD,RADM,BCNS,BCWS,RPRES,IERDS)	AO 10
COMPLEX CMPLX	AO 20
COMPLEX J,HND,JND	AO 30
COMPLEX KRO,KRD,RADM,BCNS,BCWS,RPRES	AO 40
COMPLEX Z,BJ,Y	AO 50
COMMON/ER/ IERX	AO 60
COMMON/BUG/ IDBUG	AO 70
IERDS=0	AO 80
J=(0.,1.)	AO 90
Z=RO*KRO	AO 100
D=.001	AO 110
CALL CBESL1 (Z,N,BJ,D,IERDS)	AO 120\$
IF (IERDS,NE.0) RETURN	AO 130
CALL CBESL2 (Z,N,Y,IERDS)	AO 140\$
IF (IERDS,NE.0) RETURN	AO 150
RPRES=BJ-J*Y	AO 160
CALL CBESL1 (Z,N+1,BJ,D,IERDS)	AO 170\$
IF (IERDS,NE.0) RETURN	AO 180
CALL CBESL2 (Z,N+1,Y,IERDS)	AO 190\$
IF (IERDS,NE.0) RETURN	AO 200
HND=-(BJ-J*Y)*N*RPRES/Z	AO 210
RADM=Z*HND/RPRES	AO 220
Z=DFC*KRD	AO 230
IF (FLOAT(N+1).GT.250.*CABS(Z*Z)) GO TO 10	AO 240
CALL CBESL1 (Z,N,BJ,D,IERDS)	AO 250\$
IF (IERDS,NE.0) RETURN	AO 260
BCNS=BJ	AO 270
CALL CBESL1 (Z,N+1,BJ,D,IERDS)	AO 280\$
IF (IERDS,NE.0) RETURN	AO 290
JND=-BJ*N*BCNS/Z	AO 300
BCNS=Z*JND/BCNS	AO 310
RETURN	AO 320
10 BCNS=N-Z*Z/(2.*(N+1))	AO 330
RETURN	AO 340
END	AO 350-

*DECK CBESL1		AP 10
C *****		AP 10
C BESSEL FUNCTION OF COMPLEX VARIABLES *		AP 20
C *****		AP 30
C		AP 40
SUBROUTINE CBESL1 (CX,N,CBJ,D,IER)		AP 50
COMPLEX CX,CALPHA,CBJ,CFM1,CBPREV,CFM,CBMK,CS		AP 60
COMMON/BUG/ IDBUG		AP 70
IF (IDBUG.EQ.1) WRITE (6,80)		AP 80*
CBJ=(0.,0.)		AP 90
IF (N.LT.0) IER=1		AP 100
IF (N.LT.0) RETURN		AP 110
X=CABS(CX)		AP 120
Y=AIMAG(CX)		AP 130
IF (X.EQ.0.0.AND.Y.EQ.0.0) IER=2		AP 140
IF (X.EQ.0.0.AND.Y.EQ.0.0) RETURN		AP 150
IF (X.LE.15.) NTEST=20.+10.*X-X**2/3.		AP 160
IF (X.LE.15.) GO TO 10		AP 170
NTEST=90.*X/2.		AP 180
10 IF (N.GE.NTEST) IER=4		AP 190
IF (N.GE.NTEST) RETURN		AP 200
IER=0		AP 210
N1=N+1		AP 220
CBPREV=(0.,0.)		AP 230
IF (X.LT.5.) MA=X+6.		AP 240
IF (X.LT.5.) GO TO 20		AP 250
MA=1.4*X+60./X		AP 260
20 MB=N*X/4+2		AP 270
MZERO=MAX0(MA,MB)		AP 280
MMAX=NTEST		AP 290
IF (MZERO.GE.MMAX-2) MMAX=MZERO+3		AP 300
DO 70 M=MZERO,MMAX,3		AP 310
CFM1=(1.E-28,1.E-28)		AP 320
CFM=(0.,0.)		AP 330
CALPHA=(0.,0.)		AP 340
IF (M.EQ.(M/2)*2) JT=-1		AP 350
IF (M.EQ.(M/2)*2) GO TO 30		AP 360
JT=1		AP 370
30 M2=M-2		AP 380
DO 60 K=1,M2		AP 390
MK=M-K		AP 400
CBMK=2.*MK*CFM1/CX-CFM		AP 410
CFM=CFM1		AP 420
CFM1=CBMK		AP 430
IF (MK-N-1) 50,40,50		AP 440
40 CBJ=CBMK		AP 450
50 JT=-JT		AP 460
CS=1+JT		AP 470
60 CALPHA=CALPHA+CBMK*CS		AP 480
CBMK=2.*CFM1/CX-CFM		AP 490
IF (N.EQ.0) CBJ=CBMK		AP 500
CALPHA=CALPHA+CBMK		AP 510
CBJ=CBJ/CALPHA		AP 520
ACBJ=CABS(CBJ)		AP 530
ER1=(REAL(CBJ)-REAL(CBPREV))/ACBJ		AP 540
ER2=(AIMAG(CBJ)-AIMAG(CBPREV))/ACBJ		AP 550
C ER1 = (REAL(CBJ) - REAL(CBPREV)) / REAL(CBJ)		AP 560
C ER2 = (AIMAG(CBJ) - AIMAG(CBPREV)) / AIMAG(CBJ)		AP 570
IF (ABS(ER1).GT.D) GO TO 70		AP 580
IF (ABS(ER2).GT.D) GO TO 70		AP 590
RETURN		AP 600
70 CBPREV=CBJ		AP 610
IER=3		AP 620
RETURN		AP 630
C		AP 640
80 FORMAT (1X,4HCBE1)		AP 650
END		AP 660-

•DECK CBESL2		
C	*****	AQ 10
C	C B E S L 2	AQ 20
C	*****	AQ 30
C		AQ 40
	SUBROUTINE CBESL2 (X,N,BY,IER)	AQ 50
C	COMPLEX CSQRT,CSIN,CCOS,CLOG	AQ 60
	COMPLEX T, P0, Q0, P1, Q1, A, B, Y0, Y1, XX, X2, TERM,	AQ 70
1	TS, YA, YB, YC	AQ 80
	COMPLEX X, BY	AQ 90
	COMMON/BUG/ IDBUG	AQ 100
	IF (IDBUG,EQ.1) WRITE (6,200)	AQ 110*
	IF (N) 180,10,10	AQ 120
10	IER=0	AQ 130
	IF (CABS(X)) 190,190,20	AQ 140
20	P1=3.141592653	AQ 150
	IF (CABS(X)-4.) 40,40,30	AQ 160
30	T=4./X	AQ 170
	IF (IDBUG,EQ.1) WRITE (6,200)	AQ 180*
	P0=.3989422793	AQ 190
	Q0=-.0124669441	AQ 200
	P1=.3989422819	AQ 210
	Q1=.0374008364	AQ 220
	A=T*T	AQ 230
	B=A	AQ 240
	P0=P0-.0017530620*A	AQ 250
	Q0=Q0+.0004564324*A	AQ 260
	P1=P1+.0029218256*A	AQ 270
	Q1=Q1-.00063904*A	AQ 280
	A=A*A	AQ 290
	P0=P0+.00017343*A	AQ 300
	Q0=Q0-.0000869791*A	AQ 310
	P1=P1-.000223203*A	AQ 320
	Q1=Q1+.0001064741*A	AQ 330
	A=A*B	AQ 340
	P0=P0-.0000487613*A	AQ 350
	Q0=Q0+.0000342468*A	AQ 360
	P1=P1+.0000580759*A	AQ 370
	Q1=Q1-.0000398708*A	AQ 380
	A=A*B	AQ 390
	P0=P0+.0000173565*A	AQ 400
	Q0=Q0-.0000142078*A	AQ 410
	P1=P1-.000020092*A	AQ 420
	Q1=Q1+.00001622*A	AQ 430
	A=A*B	AQ 440
	P0=P0-.0000037043*A	AQ 450
	Q0=Q0+.0000032312*A	AQ 460
	P1=P1+.0000042414*A	AQ 470
	Q1=Q1-.0000036594*A	AQ 480
	A=SQRT(2.*PI)	AQ 490
	B=4.*A	AQ 500
	P0=A*P0	AQ 510
	Q0=B*Q0/X	AQ 520
	P1=A*P1	AQ 530
	Q1=B*Q1/X	AQ 540
	A=X-PI/4.	AQ 550
	B=CSQRT(2./(PI*X))	AQ 560
	Y0=B*(P0*CSIN(A)+Q0*CCOS(A))	AQ 570
	Y1=B*(-P1*CCOS(A)+Q1*CSIN(A))	AQ 580

IF (IDBUG.EQ.1) WRITE (6,200)	AQ 590*
GO TO 90	AQ 600
40 XX=X/2.	AQ 610
X2=XX*XX	AQ 620
T=CLOG(XX)+.5772156649	AQ 630
SUM=0.	AQ 640
TERM=T	AQ 650
Y0=T	AQ 660
DO 70 L=1,15	AQ 670
IF (L-1) 50,60,50	AQ 680
50 SUM=SUM+1./FLOAT(L-1)	AQ 690
60 FL=L	AQ 700
TS=T-SUM	AQ 710
TERM=(TERM*(-X2)/FL**2)*(1.-1./(FL*TS))	AQ 720
70 Y0=Y0+TERM	AQ 730
TERM=XX*(T-.5)	AQ 740
SUM=0.	AQ 750
Y1=TERM	AQ 760
DO 80 L=2,16	AQ 770
SUM=SUM+1./FLOAT(L-1)	AQ 780
FL=L	AQ 790
FL1=FL-1.	AQ 800
TS=T-SUM	AQ 810
TERM=(TERM*(-X2)/(FL1*FL))*((TS-.5/FL)/(TS+.5/FL1))	AQ 820
80 Y1=Y1+TERM	AQ 830
PI2=2./PI	AQ 840
Y0=PI2*Y0	AQ 850
Y1=-PI2/X*PI2*Y1	AQ 860
90 IF (N-1) 100,100,130	AQ 870
100 IF (N) 110,120,110	AQ 880
110 BY=Y1	AQ 890
GO TO 170	AQ 900
120 BY=Y0	AQ 910
GO TO 170	AQ 920
130 YA=Y0	AQ 930
YB=Y1	AQ 940
K=1	AQ 950
140 T=FLOAT(2*K)/X	AQ 960
YC=T*YB-YA	AQ 970
K=K+1	AQ 980
IF (K-N) 150,160,150	AQ 990
150 YA=YB	AQ1000
YB=YC	AQ1010
GO TO 140	AQ1020
160 BY=YC	AQ1030
170 RETURN	AQ1040
180 IER=1	AQ1050
RETURN	AQ1060
190 IER=2	AQ1070
RETURN	AQ1080
C	AQ1090
200 FORMAT (1X,4HCBE2)	AQ1100
END	AQ1110-

AD-A064 685

LOCKHEED-GEORGIA CO MARIETTA
THE GENERATION, RADIATION AND PREDICTION OF SUPERSONIC JET NOIS--ETC(U)
OCT 78 B J TESTER, P J MORRIS, H K TANNA F33615-76-C-2021
LG78ER0262-VOL-2 AFAPL-TR-78-85-VOL-2 NL

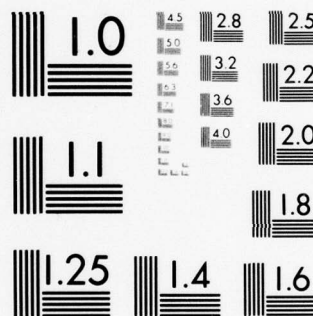
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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

•DECK IDERY

SUBROUTINE IDERY (DERY,TEMP,NDIM,PRMT,ICC)

DIMENSION DERY(1),PRMT(1)

DO 10 I=1,NDIM

DERY(I)=TEMP

10 CONTINUE

ICC=3

IF (IFIX(PRMT(7)).EQ.0) ICC=1

RETURN

END

AR 10

AR 20

AR 30

AR 40

AR 50

AR 60

AR 70

AR 80

AR 90-

*DECK HPCL	A 10
SUBROUTINE HPCL (PRMT,Y,DERY,NDIM,IHLF,AFCT,FCT,OUTP,AUX,A,X)	A 20
DIMENSION PRMT(1),Y(1),DERY(1),AUX(16,1),A(1),BT(6)	A 30
GO TO 40	A 40
C THIS PART OF SUBROUTINE HPCL COMPUTES THE RIGHT HAND SIDE DERY OF	A 50
C THE GIVEN SYSTEM OF LINEAR DIFFERENTIAL EQUATIONS.	A 60
10 CALL AFCT (X,A,Y)	A 70S
CALL FCT (X,DERY)	A 80S
DO 30 M=1,NDIM	A 90
LL=M-NDIM	A 100
HS=0.	A 110
DO 20 L=1,NDIM	A 120
LL=LL+NDIM	A 130
20 HS=HS+A(LL)*Y(L)	A 140
30 DERY(M)=HS+DERY(M)	A 150
GO TO (90,420,440,460,190,260,290,560,600,750,770,320), ISW2	A 160
C POSSIBLE BREAK-POINT FOR LINKAGE	A 170
C	A 180
C	A 190
40 N=1	A 200
IJ=1	A 210
IHLF=0	A 220
X=PRMT(1)	A 230
H=PRMT(3)	A 240
PRMT(5)=0.	A 250
DO 50 I=1,NDIM	A 260
AUX(16,I)=0.	A 270
AUX(15,I)=DERY(I)	A 280
50 AUX(1,I)=Y(I)	A 290
IF (H*(PRMT(2)-X)) 70,60,80	A 300
C	A 310
C ERROR RETURNS	A 320
60 IHLF=12	A 330
GO TO 80	A 340
70 IHLF=13	A 350
C COMPUTATION OF DERY FOR STARTING VALUES	A 360
C	A 370
80 ISW2=1	A 380
GO TO 10	A 390
C RECORDING OF STARTING VALUES	A 400
C	A 410
90 CALL OUTP (X,Y,DERY,IHLF,NDIM,PRMT)	A 420S
IF (PRMT(5)) 110,160,110	A 430
100 IF (IHLF) 120,120,110	A 440
110 RETURN	A 450
120 DO 130 I=1,NDIM	A 460
130 AUX(8,I)=DERY(I)	A 470
C COMPUTATION OF AUX(2,I)	A 480
C	A 490
ISW1=1	A 500
GO TO 400	A 510
C	A 520
140 X=X+H	A 530
DO 150 I=1,NDIM	A 540
150 AUX(2,I)=Y(I)	A 550
C INCREMENT H IS TESTED BY MEANS OF BISECTION	A 560
C	A 570
160 IHLF=IHLF+1	A 580

X=X-H	A 590
DO 170 I=1,NDIM	A 600
170 AUX(4,I)=AUX(2,I)	A 610
H=.5*M	A 620
N=1	A 630
ISW1=2	A 640
GO TO 400	A 650
C	A 660
180 X=X+H	A 670
ISW2=5	A 680
GO TO 10	A 690
190 N=2	A 700
DO 200 I=1,NDIM	A 710
AUX(2,I)=Y(I)	A 720
200 AUX(9,I)=DERY(I)	A 730
ISW1=3	A 740
GO TO 400	A 750
C	A 760
C COMPUTATION OF TEST VALUE DELT	A 770
210 DELT=0.	A 780
DO 220 I=1,NDIM	A 790
118 DELT=DELT+AUX(15,I)*ABS(Y(I)-AUX(4,I))	A 800
IF (Y(I).EQ.0.0) GO TO 220	A 810
DELT=DELT+AUX(15,I)*ABS((Y(I)-AUX(4,I))/Y(I))	A 820
220 CONTINUE	A 830
DELT=.06666667*DELT	A 840
IF (ABS(DELT)-PRMT(4)) 250,250,230	A 850
230 IF (IMLF-10) 160,240,240	A 860
C	A 870
C NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.	A 880
240 IMLF=11	A 890
X=X+H	A 900
GO TO 80	A 910
C	A 920
C SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS	A 930
250 X=X+H	A 940
ISW2=6	A 950
GO TO 10	A 960
260 DO 270 I=1,NDIM	A 970
AUX(3,I)=Y(I)	A 980
270 AUX(10,I)=DERY(I)	A 990
N=3	A1000
ISW1=4	A1010
GO TO 400	A1020
C	A1030
280 N=1	A1040
X=X+H	A1050
ISW2=7	A1060
GO TO 10	A1070
290 X=PRMT(1)	A1080
DO 300 I=1,NDIM	A1090
AUX(11,I)=DERY(I)	A1100
300 Y(I)=AUX(1,I)+H*(.375*AUX(8,I)+.7916667*AUX(9,I)-.2083333*AUX(10,I)	A1110
1)+.04166667*DERY(I))	A1120
310 X=X+H	A1130
N=N+1	A1140
ISW2=12	A1150
GO TO 10	A1160
320 CALL OUTP (X,Y,DERY,IMLF,NDIM,PRMT)	A1170S

	IF (PRMT(5)) 110,330,110	A1180
330	IF (N=4) 340,480,480	A1190
340	DO 350 I=1,NDIM	A1200
	AUX(N,I)=Y(I)	A1210
350	AUX(N+7,I)=DERY(I)	A1220
	IF (N=3) 360,380,480	A1230
C		A1240
360	DO 370 I=1,NDIM	A1250
	DELT=AUX(9,I)+AUX(9,I)	A1260
	DELT=DELT*DELT	A1270
370	Y(I)=AUX(1,I)+.3333333*H*(AUX(8,I)+DELT*AUX(10,I))	A1280
	GO TO 310	A1290
C		A1300
380	DO 390 I=1,NDIM	A1310
	DELT=AUX(9,I)+AUX(10,I)	A1320
	DELT=DELT*DELT*DELT	A1330
390	Y(I)=AUX(1,I)+.375*H*(AUX(8,I)+DELT*AUX(11,I))	A1340
	GO TO 310	A1350
C		A1360
C	THE FOLLOWING PART OF SUBROUTINE HPCL COMPUTES BY MEANS OF	A1370
C	RUNGE-KUTTA METHOD STARTING VALUES FOR THE NOT SELF-STARTING	A1380
C	PREDICTOR-CORRECTOR METHOD.	A1390
400	Z=X	A1400
	DO 410 I=1,NDIM	A1410
	XX=H*AUX(N+7,I)	A1420
	AUX(5,I)=XX	A1430
410	Y(I)=AUX(N,I)+.4*XX	A1440
C	XX IS AN AUXILIARY STORAGE LOCATION	A1450
C		A1460
	X=Z+.4*H	A1470
	ISW2=2	A1480
	GO TO 10	A1490
420	DO 430 I=1,NDIM	A1500
	XX=H*DERY(I)	A1510
	AUX(6,I)=XX	A1520
430	Y(I)=AUX(N,I)+.2969776*AUX(5,I)+.1587596*XX	A1530
C		A1540
	X=Z+.4557372*H	A1550
	ISW2=3	A1560
	GO TO 10	A1570
440	DO 450 I=1,NDIM	A1580
	XX=H*DERY(I)	A1590
	AUX(7,I)=XX	A1600
450	Y(I)=AUX(N,I)+.2181004*AUX(5,I)-3.050965*AUX(6,I)+3.832865*XX	A1610
C		A1620
	X=Z+H	A1630
	ISW2=4	A1640
	GO TO 10	A1650
460	DO 470 I=1,NDIM	A1660
470	Y(I)=AUX(N,I)+.1747603*AUX(5,I)-.5514807*AUX(6,I)+1.205536*AUX(7,I)	A1670
	+1.1711848*H*DERY(I)	A1680
	X=Z	A1690
	GO TO (140,180,210,280), ISW1	A1700
C		A1710
C	POSSIBLE BREAK-POINT FOR LINKAGE	A1720
C		A1730
C	STARTING VALUES ARE COMPUTED.	A1740
C	NOW START HAMMINGS MODIFIED PREDICTOR-CORRECTOR METHOD.	A1750
480	ISTEP=3	A1760

490 IF (N=8) 520,500,520	A1770
C	A1780
C N=8 CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS	A1790
500 DO 510 I=1,NDIM	A1800
DO 510 I=1,NDIM	A1810
AUX(N-1,I)=AUX(N,I)	A1820
510 AUX(N+6,I)=AUX(N+7,I)	A1830
N=7	A1840
C	A1850
C N LESS THAN 8 CAUSES N+1 TO GET N	A1860
520 N=N+1	A1870
C	A1880
C COMPUTATION OF NEXT VECTOR Y	A1890
DO 530 I=1,NDIM	A1900
AUX(N-1,I)=Y(I)	A1910
530 AUX(N+6,I)=DERY(I)	A1920
X=X+H	A1930
540 ISTEP=ISTEP+1	A1940
DO 550 I=1,NDIM	A1950
DELT=AUX(N-4,I)+1.333333*H*(AUX(N+6,I)+AUX(N+6,I)-AUX(N+5,I)+AUX(N	A1960
1+4,I)+AUX(N+4,I))	A1970
Y(I)=DELT-.9256198*AUX(16,I)	A1980
550 AUX(16,I)=DELT	A1990
C PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX, MODIFIED PREDICTOR	A2000
C IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.	A2010
ISW2=8	A2020
GO TO 10	A2030
C DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY	A2040
C	A2050
560 DO 570 I=1,NDIM	A2060
DELT=.125*(9*AUX(N-1,I)-AUX(N-3,I)+3.*H*(DERY(I)+AUX(N+6,I)+AUX(N	A2070
1+6,I)-AUX(N+5,I)))	A2080
AUX(16,I)=AUX(16,I)-DELT	A2090
570 Y(I)=DELT+.07438017*AUX(16,I)	A2100
C	A2110
C TEST WHETHER H MUST BE HALVED OR DOUBLED	A2120
DELT=0.	A2130
DO 580 I=1,NDIM	A2140
IF (Y(I).EQ.0.0) GO TO 580	A2150
C 310 DELT=DELT+AUX(15,I)*ABS(AUX(16,I))	A2160
DELT=DELT+AUX(15,I)*ABS(AUX(16,I)/Y(I))	A2170
580 CONTINUE	A2180
IF (ABS(DELT)-PRMT(4)) 590,720,720	A2190
C	A2200
C H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.	A2210
590 ISW2=9	A2220
GO TO 10	A2230
600 CALL OUTP (X,Y,DERY,IHLF,NDIM,PRMT)	A2240\$
IF (PRMT(5)) 620,610,620	A2250
610 IF (IHLF-11) 630,620,620	A2260
620 RETURN	A2270
630 IF (H*(X-PRMT(2))) 640,620,620	A2280
640 IF (ABS(X-PRMT(2))-1*ABS(H)) 620,650,650	A2290
650 IF (ABS(DELT)-.02*PRMT(4)) 660,660,490	A2300
C	A2310
C	A2320
C H COULD BE DOUBLED IF ALL NECESSARY PRECEEDING VALUES ARE	A2330
C AVAILABLE	A2340
660 IF (IHLF) 490,490,670	A2350

670	IF (N-7) 490,680,680	A2360
680	IF (ISTEP-4) 490,690,690	A2370
690	IMOD=ISTEP/2	A2380
	IF (ISTEP-IMOD-IMOD) 490,700,490	A2390
700	H=H+H	A2400
	IHLF=IHLF-1	A2410
	ISTEP=0	A2420
	DO 710 I=1,NDIM	A2430
	AUX(N-1,I)=AUX(N-2,I)	A2440
	AUX(N-2,I)=AUX(N-4,I)	A2450
	AUX(N-3,I)=AUX(N-6,I)	A2460
	AUX(N+6,I)=AUX(N+5,I)	A2470
	AUX(N+5,I)=AUX(N+3,I)	A2480
	AUX(N+4,I)=AUX(N+1,I)	A2490
	DELT=AUX(N+6,I)+AUX(N+5,I)	A2500
	DELT=DELT+DELT+DELT	A2510
710	AUX(16,I)=8.962963*(Y(I)-AUX(N-3,I))-3.361111*H*(DERY(I)+DELT+AUX(A2520
	1N+4,I))	A2530
	GO TO 490	A2540
		A2550
C		A2560
C	H MUST BE HALVED	A2570
720	IHLF=IHLF+1	A2580
	IF (IHLF-10) 730,730,590	A2590
730	H=.5*H	A2600
	ISTEP=0	A2610
	DO 740 I=1,NDIM	A2620
	Y(I)=.00390625*(80.*AUX(N-1,I)+135.*AUX(N-2,I)+40.*AUX(N-3,I)+AUX(A2630
	1N-4,I))-1171875*(AUX(N+6,I)-6.*AUX(N+5,I)-AUX(N+4,I))*H	A2640
	AUX(N+4,I)=.00390625*(12.*AUX(N-1,I)+135.*AUX(N-2,I)+108.*AUX(N-3,	A2650
	1I)+AUX(N-4,I))-0.234375*(AUX(N+6,I)+18.*AUX(N+5,I)-9.*AUX(N+4,I))*	A2660
	2H	A2670
	AUX(N-3,I)=AUX(N-2,I)	A2680
740	AUX(N+4,I)=AUX(N+5,I)	A2690
	DEL=X-H	A2700
	X=DEL-(H+H)	A2710
	ISW2=10	A2720
	GO TO 10	A2730
750	DO 760 I=1,NDIM	A2740
	AUX(N-2,I)=Y(I)	A2750
	AUX(N+5,I)=DERY(I)	A2760
760	Y(I)=AUX(N-4,I)	A2770
	X=X-(H+H)	A2780
	ISW2=11	A2790
	GO TO 10	A2800
770	X=DEL	A2810
	DO 780 I=1,NDIM	A2820
	DELT=AUX(N+5,I)+AUX(N+4,I)	A2830
	DELT=DELT+DELT+DELT	A2840
	AUX(16,I)=8.962963*(AUX(N-1,I)-Y(I))-3.361111*H*(AUX(N+6,I)+DELT+D	A2850
	1ERY(I))	A2860
780	AUX(N+3,I)=DERY(I)	A2870
	GO TO 540	A2880
	END	A2890-


```

•DECK AFCT
  SUBROUTINE AFCT (X,A,Y)
  DIMENSION A(1),Y(1)
    COMPLEX ACF,BCF,CCF,DCF
  DO 10 I=1,16
10  A(I)=0.0
    CALL COEF (X,ACF,BCF,CCF,DCF)
    A(3)=REAL (ACF)
    A(3)=-A(3)
    A(8)=A(3)
    A(9)=REAL (BCF)
    A(14)=A(9)
    A(10)=AIMAG (BCF)
    A(13)=-A(10)
    A(7)=AIMAG (ACF)
    A(4)=-A(7)
  RETURN
  END

```

```

B 10
B 20
B 30
B 40
B 50
B 60$
B 70
B 80
B 90
B 100
B 110
B 120
B 130
B 140
B 150
B 160
B 170-

```

```
*DECK FCT
SUBROUTINE FCT (X,F)
DIMENSION F(1)
F(1)=0.
F(2)=0.
F(3)=0.
F(4)=0.
RETURN
END
```

```
C 10
C 20
C 30
C 40
C 50
C 60
C 70
C 80-
```

*DECK OUTP	
SUBROUTINE OUTP (X,Y,DERY,IHLF,NDIM,PRMT)	D 10
DIMENSION Y(1),DERY(1),PRMT(1)	D 20
COMMON YPU(450,5)	D 30
COMPLEX ZDUM,SAVF,SAVFM	D 40
COMPLEX SAV	D 50
COMMON/CRIT/ ICC,RC,XMC(16),XTC(16),YCR	D 60
COMMON/SF/ SAVF	D 70
COMMON/STYPE/ MTYPS	D 80
COMMON/CI/ IR,IW,NOUT,ICHECK	D 90
COMMON/BJ/ M,KW,CANG,PI,BV,CV,TJR,G	D 100
COMMON/JB/ M1,M1D,M1DD,TR,TRD,TRDD	D 110
COMMON/BN/ NGE0,NCJ,NUT	D 120
COMMON /SRDCSD/ SAV(450)	D 130
REAL M,KW,M1,M1D,M1DD	D 140
XDUM=X	D 150
IF (ICC.GT.3) XDUM=YCR*RC*COS(X)	D 160
IF (XDUM.LT.PRMT(6).OR.XDUM.GT.PRMT(8)) GO TO 20	D 170
NOUT=NOUT+1	D 180
IF (NOUT.GT.450) WRITE (IW,50) X	D 190*
IF (NOUT.GT.450) RETURN	D 200
IF (ICC.GT.3) GO TO 30	D 210
YPU(NOUT,1)=X	D 220
DO 10 I=1,NDIM	D 230
10 YPU(NOUT,I+1)=Y(I)*(1.0-M1*CANG)**(MTYPS-3)	D 240
SAV(NOUT)=SAVF	D 250
20 CONTINUE	D 260
IF (IFIX(PRMT(7)).EQ.0) RETURN	D 270
IF (NOUT.GT.450) WRITE (6,40) X	D 280*
WRITE (IW,50) X,Y(1),Y(3),M1,M1D,TR,TRD,IHLF	D 290*
RETURN	D 300
30 CONTINUE	D 310
SAVFM=SAVF**(3-MTYPS)	D 320
YPU(NOUT,1)=XDUM	D 330
ZDUM=CMPLX(Y(1),Y(2))/SAVFM	D 340
YPU(NOUT,2)=REAL(ZDUM)	D 350
YPU(NOUT,3)=AIMAG(ZDUM)	D 360
ZDUM=CMPLX(Y(3),Y(4))/SAVFM	D 370
YPU(NOUT,4)=REAL(ZDUM)	D 380
YPU(NOUT,5)=AIMAG(ZDUM)	D 390
SAV(NOUT)=SAVF	D 400
GO TO 20	D 410
C	D 420
40 FORMAT (1X,"STORAGE OVERFLOW - TRY LARGER STEP SIZE. X = ",E13.6)	D 430
50 FORMAT (1X,7E11.4,11)	D 440
END	D 450-

*DECK COEF		
	SUBROUTINE COEF (X,ACF,BCF,CCF,DCF)	E 10
C	CHECK FOR 2-D CASE	E 20
	REAL M,KW,M1,M1D,M1DD	E 30
	COMMON/CI/ IR,IW,NOUT,ICHECK	E 40
	COMMON/BJ/ M,KW,CANG,PI,BV,CV,TJR,G	E 50
	COMMON/JB/ M1,M1D,M1DD,TR,TRD,TRDD	E 60
	COMMON/CRIT/ICC,RC,XMC(16),XTC(16),YCR	E 70
	COMMON/BN/ NGE0,NCJ,NUT	E 80
	COMMON/SF/ SAVF	E 90
	COMPLEX SAVF	E 100
	COMPLEX CMPLX,CEXP	E 110
	COMPLEX ACF,BCF,CCF,DCF,ZERO,FAC,J,WUN,MPHI,CXJJ	E 120
	COMPLEX MPHIX	E 130
	COMPLEX TPHI,TPHIX,CSIG	E 140
	DIMENSION YMC(3)	E 150
	DIMENSION YTC(3)	E 160
	ZERO=(0.0,0.0)	E 170
	J=(0.0,1.0)	E 180
	WUN=(1.0,0.0)	E 190
	IF (ICC.GT.3) GO TO 20	E 200
	CALL VELT (X,M,TJR,BV,CV,G,YMC,YTC,ICC)	E 210
	M1=YMC(1)	E 220
	TR=YTC(1)	E 230
	IF (ICC.EQ.1) GO TO 10	E 240
	IF (X.LT.0.) YMC(2)=-YMC(2)	E 250
	IF (X.LT.0.) YTC(2)=-YTC(2)	E 260
	M1D=YMC(2)	E 270
	TRD=YTC(2)	E 280
	M1DD=YMC(3)	E 290
	TRDD=YTC(3)	E 300
10	CONTINUE	E 310
	V=1.0-M1*CANG	E 320
	SAVF=CMPLX(V,0.0)	E 330
	P=V*V/TR	E 340
	ACF=CMPLX(KW*KW*(P-CANG*CANG)/P,0.0)	E 350
	IF (NGE0.GT.0) ACF=X*ACF-NCJ*NCJ/(X*P)	E 360
	BCF=CMPLX(P,0.0)	E 370
	IF (NGE0.GT.0) BCF=BCF/X	E 380
	CCF=ZERO	E 390
	DCF=ZERO	E 400
	RETURN	E 410
20	CONTINUE	E 420
	MPHI=ZERO	E 430
	TPHI=ZERO	E 440
	MPHIX=ZERO	E 450
	TPHIX=ZERO	E 460
	CSIG=RC*CEXP(J*X)	E 470
	CXJJ=WUN	E 480
	FAC=WUN	E 490
	DO 40 JJ=1,ICC	E 500
	MPHI=MPHI+XMC(JJ)*FAC/CXJJ	E 510
	TPHI=TPHI+XTC(JJ)*FAC/CXJJ	E 520
	IF (CABS((MPHI-MPHIX)/MPHI).GT..0001) GO TO 30	E 530
	IF (CABS((TPHI-TPHIX)/TPHI).LT..0001) GO TO 50	E 540
30	CONTINUE	E 550
	MPHIX=MPHI	E 560
	TPHIX=TPHI	E 570
	FAC=FAC*CSIG	E 580

	XJJ=JJ	E 590
	CXJJ=CMPLX(XJJ,0.0)*CXJJ	E 600
40	CONTINUE	E 610
	STOP 7	E 620
50	CONTINUE	E 630
	FAC=WUN*MPHI*CANG	E 640
	SAVF=FAC	E 650
	FAC=FAC*FAC/TPHI	E 660
	ACF=J*CSIG*KW*KW*(WUN=CANG*CANG/FAC)	E 670
	IF (NGEO.EQ.1) ACF=(YCR*CSIG)*ACF=NCJ*NCJ/(FAC*(YCR*CSIG))*J*CSIG	E 680
	BCF=J*CSIG*FAC	E 690
	IF (NGEO.EQ.1) BCF=BCF/(YCR*CSIG)	E 700
	CCF=ZERO	E 710
	DCF=ZERO	E 720
	IF (JJ.EQ.ICC) ICHECK=1	E 730
C	WRITE(IW,400) MPHI,TPHI,ACF,JJ,ICC	E 740
C	400 FORMAT(1X,6E13.6/1X,2I5)	E 750
	M1=REAL(MPHI)	E 760
	TR=REAL(TPHI)	E 770
	M1D=XMC(2)	E 780
	TRD=XTC(2)	E 790
	M1DD=XMC(3)	E 800
	TRDD=XTC(3)	E 810
	RETURN	E 820
	END	E 830-

```
•DECK TRANS
  SUBROUTINE TRANS (ST2,Y,NDIM)
    DIMENSION ST2(1),Y(1)
    DO 10 I=1,NDIM
      Y(I)=ST2(I)
10  CONTINUE
    RETURN
  END
```

```
F 10
F 20
F 30
F 40
F 50
F 60
F 70-
```

•DECK WRCAL	
SUBROUTINE WRCAL (NGEO,Y,RADM,RPRES,FWRONS)	G 10
COMPLEX CMPLX	G 20
COMPLEX RADM,RPRES,FWRONS ,WRONSK	G 30
DIMENSION Y(1)	G 40
PI=3.141593	G 50
WRONSK=(1.,0.)	G 60
IF (NGEO.EQ.1) WRONSK=CMPLX(0.,-2./PI)	G 70
FWRONS=(CMPLX(Y(1),Y(2))*RADM-CMPLX(Y(3),Y(4)))*RPRES	G 80
FWRONS=WRONSK/FWRONS	G 90
RETURN	G 100
END	G 110-

*DECK TCON	
SUBROUTINE TCON (MS,NCJX,NCJNX,TIJ,TX,ECON,NCON,MXOS)	H 10
DIMENSION TIJ(7,1),TX(1)	H 20
IF (NCJX.EQ.NCJNX) GO TO 20	H 30
IF (NCJX.LT.3) GO TO 20	H 40
ICT=0	H 50
DO 10 I=1,7	H 60
IF (TIJ(I,MS).EQ.0.) GO TO 10	H 70
IF (TX(I)/TIJ(I,MS).LT.ECON) NCON=NCON+1	H 80
IF (TX(I)/TIJ(I,MS).LT.ECON/100.) ICT=ICT+1	H 90
10 CONTINUE	H 100
IF (ICT.EQ.7) MXOS=MXOS+1	H 110
20 DO 30 I=1,7	H 120
TIJ(I,MS)=TIJ(I,MS)+TX(I)	H 130
30 CONTINUE	H 140
RETURN	H 150
END	H 160-

*DECK TSIGN	
SUBROUTINE TSIGN (MS,TIJ)	I 10
DIMENSION TIJ(6,1)	I 20
COMMON/CI/ IR,IW,NOUT,ICHECK	I 30
DO 20 I=1,6	I 40
IF (TIJ(I,MS).GT.0.) GO TO 10	I 50
WRITE (IW,30) I,TIJ(I,MS)	I 60*
TIJ(I,MS)=-TIJ(I,MS)	I 70
IF (TIJ(I,MS).EQ.0.) TIJ(I,MS)=1.	I 80
10 CONTINUE	I 90
20 CONTINUE	I 100
RETURN	I 110
C	I 120
30 FORMAT (1X,13H**SOURCE TYPE,I5,2HIS,E13.6)	I 130
END	I 140-

*DECK RADCSO		
SUBROUTINE RADCSO (IFLAG,NCJ,WINV,D,ID,NOUTM,BV,CV)		J 10
DIMENSION D(1),ID(1),XM(2),XT(2),SLTB(5),A(5,7),TIJ(7,5)		J 20
DIMENSION SSIM(5),SSID(5),SSIQ(5)		J 30
COMPLEX C(450,7)		J 40
COMPLEX WINV,TRRN,RES		J 50
COMPLEX SAV		J 60
REAL M,KW		J 70
COMMON YPU(450,5)		J 80
COMMON /SRDCSD/ SAV(450)		J 90
COMMON/PSD/ RC,BLTB,CVD		J 100
C		J 110
RPI=1.772424		J 120
CVD=CV		J 130
G=D(8)		J 140
RSW=D(9)		J 150
RSC=D(10)		J 160
KW=D(11)		J 170
XKW2=KW*KW		J 180
M=D(12)		J 190
TJR=D(13)		J 200
CANG=D(14)		J 210
X1=D(16)		J 220
TCOR=D(18)		J 230
DCOR=D(19)		J 240
C		J 250
IW=ID(2)		J 260
NGEO=ID(3)		J 270
MTYPS=ID(4)		J 280
IWB=ID(8)		J 290
NCL=ID(25)		J 300
IO=ID(26)		J 310
C	GO AND FORM SIO,SID IF THIS IS FINAL CALL	J 320
	IF (IFLAG.GT.0) GO TO 70	J 330
	DO 10 IT=1,NCL	J 340
C	SLTB(IT)=D(IT+24)*X1	J 350
	SLTB(IT)=D(IT+25)	J 360
10	CONTINUE	J 370
	AWINV=CABS(WINV)	J 380
	RC=RSC*X1+1.0	J 390
	R99=BV*SQRT(ALOG(1.0/0.99))	J 400
	IF (CV.EQ.0.0.AND.RC.LT.R99) RC=R99	J 410
	IF (RC.LE.2.0*D(4)) RC=2.0*D(4)	J 420
	BLTB=0.5*X1*RSW/0.832554611	J 430
	IF (BLTB.LE.0.0) RETURN	J 440
	RCB=RC/BLTB	J 450
	REF=BLTB*BLTB/2.0*(EXP(-RCB*RCB)+RCB*RPI*(1.0+ERF(RCB)))	J 460
	ICC=1	J 470
	CALL VELT (RC,M,TJR,BV,CV,G,XM,XT,ICC)	J 480
	XKAPS2=(1.0-XM(1)*CANG)*(1.0-XM(1)*CANG)/XT(1)-CANG*CANG	J 490
	XKAPS2=ABS(XKAPS2)	J 500
	IF (NCJ.NE.0) GO TO 30	J 510
	DO 20 IT=1,5	J 520
	DO 20 JS=1,7	J 530
20	TIJ(JS,IT)=0.0	J 540
30	CONTINUE	J 550
C	SET UP CNAB FOR ALL SOURCE TYPES	J 560
	ICC=2	J 570
	DO 40 I=1,NOUTM	J 580

R=YPU(I,1)	J 590
CALL VELT (R,M,TJR,BV,CV,G,XM,XT,ICC)	J 6005
PRS=1.0-XM(1)*CANG	J 610
PRS=PRS*PRS/XT(1)	J 620
PQ=(CANG*CANG-PRS)*KW*KW	J 630
PD=-XT(2)/XT(1)-2.0*XM(2)*CANG/(1.0-XM(1)*CANG)	J 640
C(I,1)=CMPLX(YPU(I,2),YPU(I,3))	J 650
C(I,2)=CMPLX(YPU(I,4),YPU(I,5))	J 660
C(I,2)=C(I,2)*PRS/R	J 670
TRRN=(PQ+NCJ*NCJ/(R*R))*C(I,1)+(PD-NGEO/R)*C(I,2)	J 680
C(I,3)=TRRN-(MTYPS-3)*XM(2)*CANG/(1.0-XM(1)*CANG)*C(I,2)	J 690
C(I,4)=NCJ*C(I,1)/R	J 700
C(I,6)=(C(I,2)-NCJ*NCJ*C(I,1)/R)/R	J 710
C(I,7)=C(I,2)	
C(I,2)=C(I,2)-XM(2)*CANG*C(I,1)/SAV(I)	J 720
C(I,5)=NCJ*(C(I,2)-C(I,1)/R)/R	J 730
40 CONTINUE	J 740
DO 60 IT=1,NCL	J 750
IF (SLTB(IT),LT,D(1),OR,BLTB,LT,D(1)) GO TO 60	J 760
DO 50 JS=1,7	J 770
CALL INTRAP (NCJ,YPU(I,1),C(I,JS),NOUTH,SLTB(IT),RES,IERS)	J 7805
IF (CABS(RES),LE,0,0) RES=(1.E-99,0,0)	J 790
C(IT,JS)=RES	J 800
C(IT,JS)=C(IT,JS)*AWINV*AWINV	J 810
ARG=KW*SLTB(IT)/2.0	J 820
IF (SLTB(IT),LT,BLTB/10,0) ARG=0.0	J 830
C(IT,JS)=EXP(ARG*ARG*XKAPS2)*C(IT,JS)	J 840
C(IT,JS)=C(IT,JS)/(REF*SLTB(IT)*SLTB(IT)/2.0)	J 850
TIJ(JS,IT)=TIJ(JS,IT)+CABS(C(IT,JS))	J 860
IF (NCJ,NE,0) TIJ(JS,IT)=TIJ(JS,IT)+CABS(C(IT,JS))	J 870
50 CONTINUE	J 880
SIM=10.0*ALOG10(CABS(C(IT,1)))	J 890
IF (NCJ,EQ,0) SSIM(IT)=SIM	J 900
SIM=SIM-SSIM(IT)	J 910
SID=CABS(C(IT,7))+CABS(C(IT,4))+XKW2*CANG*CANG*CABS(C(IT,1))	J 920
SID=10.0*ALOG10(SID/XKW2)	J 930
IF (NCJ,EQ,0) SSID(IT)=SID	J 940
SID=SID-SSID(IT)	J 950
SIO=CABS(C(IT,3))+CABS(C(IT,6))+2.0*CABS(C(IT,5))	J 960
SIO=SIO*XKW2*XKW2*CANG**4+CABS(C(IT,1))+2.0*CANG**2*XKW2*(CABS(C(I	J 970
IT,2))+CABS(C(IT,4)))	J 980
SIO=10.0*ALOG10(SIO/(XKW2*XKW2))	J 990
IF (NCJ,EQ,0) SSIO(IT)=SIO	J1000
SIO=SIO-SSIO(IT)	J1010
IF (IO,EQ,0) GO TO 60	J1020
IF (IWB,NE,0) WRITE (IW,100) IERS,SLTB(IT),(TIJ(JS,IT)+JS=1,7),SIM	J1030*
1,SID,SIO,NCJ	J1040
60 CONTINUE	J1050
GO TO 90	J1060
70 CONTINUE	J1070
DO 80 IT=1,NCL	J1080
IF (SLTB(IT),LT,D(1),OR,BLTB,LT,D(1)) GO TO 80	J1090
A(IT,1)=10.0*ALOG10(TIJ(1,IT))	J1100
A(IT,2)=10.0*ALOG10(TIJ(2,IT)/(0.5*XKW2))	J1110
A(IT,3)=10.0*ALOG10(TIJ(3,IT)/(0.375*XKW2*XKW2))	J1120
A(IT,4)=10.0*ALOG10(TIJ(4,IT)/(0.5*XKW2))	J1130
A(IT,5)=10.0*ALOG10(TIJ(5,IT)/(0.125*XKW2*XKW2))	J1140
A(IT,6)=10.0*ALOG10(TIJ(6,IT)/(0.375*XKW2*XKW2))	J1150
A(IT,7)=10.0*ALOG10(TIJ(7,IT)/(0.5*XKW2))	
SIO=TIJ(3,IT)+TIJ(6,IT)+2.0*TIJ(5,IT)	J1160
SIO=SIO*XKW2*XKW2*(CANG**4)+TIJ(1,IT)+2.0*CANG*CANG*XKW2*(TIJ(2,IT	J1170

1)*TIJ(4,IT)	J1180
SIQ=10.0*ALOG10(SIQ/(XKW2*XKW2))	J1190
SIQ=SIQ+TCOR	J1200
SID=TIJ(7,IT)+TIJ(4,IT)*XKW2*CANG*CANG*TIJ(1,IT)	J1210
SID=10.0*ALOG10(SID/XKW2)	J1220
SID=SID+DCOR	J1230
IF (IO.EQ.0) GO TO 80	J1240
IF (IWB.NE.0) WRITE (IW,110) SLTB(IT),(A(IT,JS),JS=1,7),SIQ,SID	J1250
80 CONTINUE	J1260
D(36)=A(IT,1)	J1270
D(37)=SID	J1280
D(38)=SIQ	J1290
90 CONTINUE	J1300
RETURN	J1310
C	J1320
100 FORMAT (1X,I1.11F14.4,I5)	J1330
110 FORMAT (1X,F3.4,14X,9F7.2)	J1340
END	J1350

*DECK INTRAP	
SUBROUTINE INTRAP (NCJ,R,CNAB,NOUTM,SLTB,RES, IERS)	K 10
COMMON/PSD/ RC,BLTB,CVD	K 20
DIMENSION R(1)	K 30
COMPLEX CNAB(1),YIN(450),YOUT(450),RES	K 40
IERS=0	K 50
RMIN=RC-1.96*BLTB*1.414	K 60
RMAX=RC+1.96*BLTB*1.414	K 70
SLTB2=SLTB*SLTB/2.0	K 80
IZC=0	K 90
IF (SLTB.LT,BLTB/10.0) IZC=1	K 100
DO 40 JOUT=1,NOUTM	K 110
RFIX=R(JOUT)	K 120
YOUT(JOUT)=(0.0,0.0)	K 130
IF (RFIX.LT,RMIN.OR,RFIX.GT,RMAX) GO TO 40	K 140
RFB=RFIX/SLTB	K 150
IF (IZC.EQ,0) GO TO 10	K 160
YIN(NOUTM)=CNAB(JOUT)*SRPSD(RFIX)*SLTB2	K 170
GO TO 30	K 180
10 CONTINUE	K 190
DO 20 JIN=1,NOUTM	K 200
YIN(JIN)=(0.0,0.0)	K 210
RVAR=R(JIN)	K 220
IF (RVAR.LT,RMIN.OR,RVAR.GT,RMAX) GO TO 20	K 230
RVB=RVAR/SLTB	K 240
ARG=2.0*RFB*RVB	K 250
DR2=(RVB-RFB)*(RVB-RFB)	K 260
C -675.84,X.741.67 FOR EXP(X) ON CDC 7600	K 270
IF (DR2.GT,3.84) GO TO 20	K 280
CALL BESI (ARG,NCJ,ANS,IER)	K 290
IF (IER.NE,0) IERS=1	K 300
YIN(JIN)=RVAR*CNAB(JIN)*SRPSD(RVAR)*ANS*EXP(-DR2)	K 310
20 CONTINUE	K 320
CALL QTFG (R,YIN,YIN,NOUTM)	K 330
30 CONTINUE	K 340
YOUT(JOUT)=RFIX*CONJG(CNAB(JOUT))*SRPSD(RFIX)*YIN(NOUTM)	K 350
40 CONTINUE	K 360
CALL QTFG (R,YOUT,YOUT,NOUTM)	K 370
RES=YOUT(NOUTM)	K 380
RETURN	K 390
END	K 400-

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•DECK SRPSD
      FUNCTION SRPSD(R)
      COMMON/PSD/ RC,BLTB,CVD
      SRPSD=0.0
      DR=(R-RC)/BLTB
      DR2=DR*DR
      IF (DR2.GT.78.0) GO TO 10
      SRPSD=EXP(-DR2/2.0)
10  CONTINUE
      RETURN
      END

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L 10
L 20
L 30
L 40
L 50
L 60
L 70
L 80
L 90
L 100-

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*DECK	BESI		
	SUBROUTINE BESI (X,N,BI,IER)		M 10
C	BESI MODIFIED TO COMPUTE EXP(-X)*ORIGINAL		M 20
	IER=0		M 30
	BI=1.0		M 40
	IF (N) 210,20,10		M 50
10	IF (X) 220,40,40		M 60
20	IF (X) 220,30,40		M 70
30	RETURN		M 80
40	TOL=1.0E-2		M 90
	IF (X-12.0) 60,60,50		M 100
50	IF (X-FLOAT(N)) 60,60,170		M 110
60	XX=X/2.0		M 120
	TERM=1.0		M 130
	IF (N) 100,100,70		M 140
70	DO 90 I=1,N		M 150
	FI=I		M 160
	IF (ABS(TERM)-1.0E-68) 80,90,90		M 170
80	IER=3		M 180
	BI=0.0		M 190
	RETURN		M 200
90	TERM=TERM*XX/FI		M 210
100	BI=TERM		M 220
	XX=XX*XX		M 230
	DO 120 K=1,1000		M 240
C	IF (ABS(TERM) - ABS(BI*TOL)) 100,100,80		M 250
	IF (ABS(TERM)-ABS(BI*TOL)) 130,130,110		M 260
C	80 FK=K*(N+K)		M 270
110	FK=FLOAT(K)*FLOAT(N+K)		M 280
	TERM=TERM*(XX/FK)		M 290
120	BI=BI+TERM		M 300
	IER=5		M 310
	GO TO 160		M 320
130	CONTINUE		M 330
	IF (X-170.0) 150,150,140		M 340
140	IER=4		M 350
	GO TO 160		M 360
150	BI=EXP(-X)*BI		M 370
160	RETURN		M 380
170	FN=4*N*N		M 390
C	IF (X-170.0) 115,111,111		M 400
C	111 IER=4		M 410
C	RETURN		M 420
	XX=1.0/(8.0*X)		M 430
	TERM=1.0		M 440
	BI=1.0		M 450
	DO 190 K=1,30		M 460
	IF (ABS(TERM)-ABS(TOL*BI)) 200,200,180		M 470
180	FK=(2*K-1)**2		M 480
	TERM=TERM*XX*(FK-FN)/FLOAT(K)		M 490
190	BI=BI+TERM		M 500
	GO TO 60		M 510
200	PI=3.141592653		M 520
C	BI=BI*EXP(X)/SQRT(2.0*PI*X)		M 530
	BI=BI/SQRT(2.0*PI*X)		M 540
	GO TO 160		M 550
210	IER=1		M 560
	GO TO 160		M 570
220	IER=2		M 580
	GO TO 160		M 590
	END		M 600-

*DECK QTFG		N 10
C *****		
C SUBROUTINE QTFG		N 20
C		N 30
C PURPOSE		N 40
C TO COMPUTE THE VECTOR OF INTEGRAL VALUES FOR A GIVEN		N 50
C GENERAL TABLE OF ARGUMENT AND FUNCTION VALUES.		N 60
C		N 70
C DESCRIPTION IS ON PAGE 86 OF IBM-SSP MANUAL		N 80
C *****		N 90
C *****		N 100
C SUBROUTINE QTFG (X,Y,Z,NDIM)		N 110
C		N 120
C DIMENSION X(1)		N 130
C COMPLEX Y(1),Z(1),SUM1,SUM2		N 140
C		N 150
C SUM2=0.0		N 160
C IF (NDIM-1) 40,30,i0		N 170
C		N 180
C INTEGRATION LOOP		N 190
10 DO 20 I=2,NDIM		N 200
SUM1=SUM2		N 210
SUM2=SUM2+.5*(X(I)-X(I-1))*(Y(I)+Y(I-1))		N 220
20 Z(I-1)=SUM1		N 230
30 Z(NDIM)=SUM2		N 240
40 RETURN		N 250
END		N 260
		N 270-


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*DECK BLKTMN
      BLOCK DATA TMN
C
C      INPUT DATA*****
C      A=ETA(SM)
C      B=SPLNQ(SM)
C      C=CQ(SM)
C      D=SPLND(SM)
C      E=E(SM)
C      F=CD(SM)
C      H=ARGUMENT X IN EXPONENTIAL DECAY FACTOR
C      P=EXPONENTIAL DECAY FACTOR DEC(X) FOR ARGUMENT X
C
C      R=RATIO OF CENTER-LINE VELOCITY TO JET EXIT VELOCITY AT EACH
C      STROUHAL NUMBER
C      U=RATIO OF MEAN VELOCITY TO CENTER-LINE VELOCITY AT EACH
C      STANDARD SOURCE POSITION
C
C      COMMON/FOUR/A(16)
C      COMMON/FIVE/B(16)
C      COMMON/SIX/C(16)
C      COMMON/SEVEN/D(16)
C      COMMON/EIGHT/E(16)
C      COMMON/NINE/F(16)
C      COMMON/ELEVEN/H(7)
C      COMMON/TWELVE/P(7)
C
C      COMMON/FOUR1/ A1(28)
C      COMMON /FIVE1/ B1(28)
C      COMMON /SIX1/ C1(28)
C      COMMON /SEVEN1/ D1(28)
C      COMMON /EIGHT1/ E1(28)
C      COMMON /NINE1/ F1(28)
C      COMMON /EIGHTY1/ SD1(28,6),SDT1(28,6)
C
C      COMMON/THIRTN1/ R1(28)
C      COMMON/THIRTN/R(16)
C      COMMON/FOURTN/U(24)
C
C      COMMON/EIGHTY/T1(6),SD(16,6)
C
C      DATA (T1(I),I=1,4) / 0.980, 1.770, 2.209, 3.330 /
C      DATA ((SD(N,K),N=1,16),K=1,4) / 0.67,0.80,0.95,1.18,1.31,1.70,
1 2.00,2.30,2.62,2.92,3.23,3.50,3.75,4.00,4.25,4.45,0.67,0.80,
2 0.95,1.18,1.43,1.70,2.00,2.30,2.70,3.10,3.40,3.80,4.18,4.50,
3 4.80,5.15,0.67,0.80,0.95,1.15,1.50,1.90,2.30,2.72,3.14,3.55,
4 3.95,4.38,4.75,5.12,5.40,5.60,0.67,0.80,0.95,1.20,1.55,2.00,
5 2.50,2.90,3.45,3.90,4.35,4.75,5.10,5.35,5.60,5.80 /
C
C      DATA ((SDT1(N,I),N=1,28),I=1,4) /
10.01,0.01,0.01,0.01,0.01,0.01,0.05,0.13,0.30,0.52,0.80,1.05,1.30,
21.50,1.75,1.90,2.05,2.18,2.30,2.40,2.50,2.60,2.69,2.79,2.89,2.96,
33.03,3.09,
40.08,0.09,0.11,0.12,0.15,0.23,0.32,0.45,0.65,0.90,1.20,1.50,1.80,
52.10,2.35,2.55,2.70,2.90,3.03,3.17,3.30,3.43,3.55,3.67,3.79,3.89,
63.98,4.06,
70.20,0.22,0.25,0.28,0.31,0.39,0.53,0.70,0.95,1.25,1.60,1.95,2.25,
82.55,2.85,3.05,3.30,3.50,3.70,3.90,4.06,4.23,4.39,4.56,4.71,4.84,

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	94.94,5.04,	0 590
	\$0.25,0.28,0.32,0.36,0.45,0.57,0.75,0.95,1.25,1.60,2.00,2.35,2.70,	0 600
	\$3.00,3.30,3.60,3.85,4.10,4.30,4.50,4.70,4.80,5.10,5.24,5.42,5.56,	0 610
	\$5.68,5.80/	0 620
C		0 630
	DATA ((SD1(N,I),N=1,28),I=1,4)/	0 640
	1 0.11,0.14,0.18,0.23,0.31,0.45,0.65,0.85,1.10,1.35,1.60,1.85,2.20,	0 650
	2 2.55,3.00,3.30,3.60,3.85,4.10,4.45,4.75,5.10,5.32,5.53,5.71,5.86,	0 660
	3 5.99,6.11,	0 670
	4 0.11,0.14,0.18,0.23,0.31,0.45,0.65,0.85,1.10,1.35,1.60,1.85,2.25,	0 680
	5 2.70,3.15,3.50,3.95,4.30,4.70,5.00,5.30,5.58,5.82,6.04,6.24,6.41,	0 690
	6 6.55,6.68,	0 700
	7 0.11,0.14,0.18,0.25,0.35,0.50,0.70,0.95,1.25,1.55,1.90,2.25,2.75,	0 710
	8 3.25,3.75,4.20,4.60,5.00,5.35,5.65,5.95,6.26,6.53,6.78,7.01,7.19,	0 720
	9 7.35,7.50,	0 730
	\$ 0.11,0.14,0.18,0.25,0.35,0.50,0.77,1.10,1.50,1.85,2.25,2.75,3.25,	0 740
	\$ 3.80,4.30,4.75,5.20,5.55,5.85,6.13,6.40,6.74,7.03,7.29,7.54,7.74,	0 750
	\$ 7.91,8.07 /	0 760
C		0 770
	DATA A(1),A(2),A(3),A(4),A(5),A(6),A(7),A(8),A(9),A(10),A(11),	0 780
	1 A(12),A(13),A(14),A(15),A(16)/0.5,0.52,0.54,0.56,0.57,0.58,0.585,	0 790
	2 0.59,0.595,0.598,0.6,0.6,0.6,0.6,0.6,0.6/	0 800
C		0 810
	DATA A1/ 0.32,0.36,0.40,0.44,0.47,0.5,0.52,0.54,0.56,0.57,0.58,	0 820
	1 0.585,0.59,0.595,0.598,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,	0 830
	2 0.6,0.6,0.6 /	0 840
C		0 850
	DATA B(1),B(2),B(3),B(4),B(5),B(6),B(7),B(8),B(9),B(10),B(11),	0 860
	1 B(12),B(13),B(14),B(15),B(16)/81.5,83.5,85.2,86.9,88.2,89.4,90.4,	0 870
	2 91.2,91.8,92.1,92.2,92.2,92.1,92.0,91.9,91.6/	0 880
C		0 890
	DATA B1/ 70.5,73.5,75.5,78.0,79.9,81.5,83.1,84.6,86.2,87.7,89.0,	0 900
	1 90.0,90.7,91.3,91.8,92.1,92.1,92.0,91.9,91.7,91.4,90.8,90.3,	0 910
	2 89.7,89.2,88.6,88.1,87.5 /	0 920
C		0 930
	DATA C(1),C(2),C(3),C(4),C(5),C(6),C(7),C(8),C(9),C(10),C(11),	0 940
	1 C(12),C(13),C(14),C(15),C(16)/0.75,0.75,0.75,1.1,1.0,1.0,1.0,1.1,	0 950
	2 0.75,0.5,0.3,0.1,0.0,-0.2,-0.4,-0.5/	0 960
C		0 970
	DATA C1/ 7.0,5.0,4.0,3.0,3.0,2.3,1.5,1.0,1.0,1.2,1.2,1.0,0.9,0.7,	0 980
	1 0.6,0.3,0.1,0.0,-0.15,-0.25,-0.4,-0.4,-0.5,-0.55,-0.6,-0.65,	0 990
	2 -0.7,-0.7 /	01000
C		01010
	DATA D(1),D(2),D(3),D(4),D(5),D(6),D(7),D(8),D(9),D(10),D(11),	01020
	1 D(12),D(13),D(14),D(15),D(16)/93.2,95.3,97.0,98.4,99.4,100.1,	01030
	2 100.7,100.9,100.9,100.8,100.6,100.1,99.5,98.7,97.8,96.9/	01040
C		01050
	DATA D1/ 82.0,84.4,86.6,88.8,91.0,93.1,95.2,97.0,98.3,99.4,100.1,	01060
	1 100.6,101.0,101.1,101.0,100.6,100.0,99.3,98.5,97.6,96.6,95.8,	01070
	2 94.9,94.0,93.0,92.0,91.0,90.0 /	01080
C		01090
	DATA E(1),E(2),E(3),E(4),E(5),E(6),E(7),E(8),E(9),E(10),E(11),	01100
	1 E(12),E(13),E(14),E(15),E(16)/0.8,0.77,0.75,0.7,0.68,0.66,0.63,	01110
	2 0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6/	01120
C		01130
	DATA E1/ 1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,0.9,0.8,0.73,0.68,0.65,	01140
	1 0.63,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6,0.6 /	01150
C		01160
	DATA F(1),F(2),F(3),F(4),F(5),F(6),F(7),F(8),F(9),F(10),F(11),	01170

	1 F(12),F(13),F(14),F(15),F(16)/2.3,2.0,1.5,1.3,1.0,0.8,0.6,0.5,	01180
	2 0.3,0.1,-0.15,-0.2,-0.35,-0.4,-0.4,-0.4/	01190
C		01200
	DATA F1/ 15.0,10.0,10.0,7.5,6.0,4.5,3.0,1.7,1.3,1.0,0.8,0.6,0.3,	01210
	1 0.2,0.0,-0.15,-0.2,-0.3,-0.3,-0.4,-0.4,-0.5,-0.55,-0.6,-0.62,	01220
	2 -0.62,-0.65,-0.7 /	01230
C		01240
	DATA H(1),H(2),H(3),H(4),H(5),H(6),H(7)/0.0,0.1,0.2,0.3,0.4,0.5,	01250
	1 0.6/	01260
C		01270
	DATA P(1),P(2),P(3),P(4),P(5),P(6),P(7)/1.0,0.59,0.4,0.28,0.2,	01280
	1 0.158,0.128/	01290
C		01300
	DATA R/ 0.58,0.65,0.74,0.82,0.9,0.95,0.99,1.0,1.0,1.0,1.0,1.0,1.0,	01310
	1 1.0,1.0,1.0 /	01320
C		01330
	DATA R1 / 0.32,0.36,0.4,0.46,0.52,0.58,0.65,0.74,0.82,0.90,0.96,	01340
	1 1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,	01350
	2 1.0,1.0 /	01360
C		01370
	DATA U(1),U(2),U(3),U(4),U(5),U(6),U(7),U(8),U(9),U(10),U(11),	01380
	1 U(12),U(13),U(14),U(15),U(16),U(17),U(18),U(19),U(20),U(21),	01390
	2 U(22),U(23),U(24)/0.99,0.98199,0.968865,0.9481,0.91859,0.87741,	01400
	3 0.82377,0.757455,0.67936,0.67,0.66295,0.6,0.591905,0.5,0.408098,	01410
	4 0.3206435,0.2425485,0.1762325,0.1225905,0.081409,0.051541,	01420
	5 0.0311374,0.018008,0.01/	01430
C		01440
	END	01450-

*DECK SANOISE	P 10
SUBROUTINE SANOISE (BETA,TJTO,ROD,BC,DFT,A0,NFREQ,FREQ,I,J,TM,L0,M	P 20
1J,DF,WORK2,NS,SPLC,HXX,HYY,CYY,A3,A2)	P 30
DIMENSION TM(20),FREQ(20),SPLC(30),HVX(30),HVV(30),CVX(30),	P 40
1 CVY(30),ANS3DB(30)	P 50
COMMON / THIRTY / HX(20)	P 60
COMMON / FORTY / HY(20)	P 70
COMMON / FIFTY / CX(20)	P 80
COMMON / SIXTY / CY(20)	P 90
REAL MJ,K0,K1,L0,L1,MC	P 100
IF (J,NE,1,OR,I,NE,1) GO TO 50	P 110
C CALCULATION OF OASPLC (PACKAGE C)	P 120
C	P 130
C	P 140
IF (BETA.GT.1.0) GO TO 20	P 150
IF (TJTO.LT.0.9) GO TO 10	P 160
ANS1DB=(40.0*ALOG10(BETA))-(20.0*ALOG10(ROD))	P 170
OASPLC=157.5+ANS1DB	P 180
GO TO 40	P 190
10 ANS1DB=(40.0*ALOG10(BETA))-(20.0*ALOG10(ROD))	P 200
OASPLC=155.5+ANS1DB	P 210
GO TO 40	P 220
20 IF (TJTO.LT.0.9) GO TO 30	P 230
ANS1DB=(20.0*ALOG10(BETA))-(20.0*ALOG10(ROD))	P 240
OASPLC=157.5+ANS1DB	P 250
GO TO 40	P 260
30 ANS1DB=(10.0*ALOG10(BETA))-(20.0*ALOG10(ROD))	P 270
OASPLC=155.5+ANS1DB	P 280
GO TO 40	P 290
40 CONTINUE	P 300
50 IF (J,NE,1) GO TO 70	P 310
C CALCULATION OF ANS3DB AND INTERPOLATED VALUES OF H0 AND C1	P 320
C FOR ALL SPECIFIED FREQUENCIES (PACKAGE C)	P 330
C	P 340
WORK1=((6.2832*RC*DFT*BETA)/A0)	P 350
HVX(I)=((6.283*FREQ(I)*L0)/(12.0*A0))	P 360
CVX(I)=HVX(I)	P 370
IF (HVX(I).LT.0.2) GO TO 60	P 380
IF (HVX(I).GT.70.0) GO TO 60	P 390
CALL LAGRNG (HX,HY,20,HVX(I),HVV(I))	P 400
IF (TJTO.LT.0.9) HVY(I)=HVV(I)-2.0	P 410
CALL LAGRNG (CX,CY,20,CVX(I),CVY(I))	P 420
ANS3DB(I)=10.0*ALOG10(WORK1*FREQ(I))	P 430
60 CONTINUE	P 440
70 CONTINUE	P 450
IF (MJ,LE,1.0) GO TO 110	P 460
C SHOCK NOISE CONTRIBUTION CAN BE AND IS NEGLECTED	P 470
C FOR THE FOLLOWING CONDITIONS	P 480
C (1) TJTO LESS THAN 0.9 AND TM(J) LESS THAN 50 DEG.	P 490
C (2) TJTO GREATER THAN 0.9 AND TM(J) LESS THAN 30 DEG.	P 500
C	P 510
C	P 520
IF (TJTO.LT.0.9.AND.TM(J).LT.50.0.OR.TJTO.GE.0.9.AND.TM(J).LT.30.0	P 530
1) GO TO 120	P 540
C	P 550
IF (HVX(I).LT.0.2) GO TO 100	P 560
IF (HVX(I).GT.70.0) GO TO 100	P 570
C	P 580

WC=6.283*FREQ(I)	P 590
IIEND=NS-1	P 600
SUMI=0.0	P 610
DO 90 II=1,IIEND	P 620
CI2=CVY(I)**(II+1),	P 630
ISEND=NS-II	P 640
SUMS=0.0	P 650
DO 80 ISN=1,ISEND	P 660
IS=ISN-1	P 670
QIS=WORK2*II*(1.0-(0.06*(IS+((II+1.0)/2.0))))	P 680
QCOS=COS(QIS*WC)	P 690
QSIN=SIN((QIS*WC*BC)/2.0)	P 700
WORK3=(QCOS*QSIN)/QIS	P 710
SUMS=SUMS+WORK3	P 720
80 CONTINUE	P 730
WORK4=CI2*SUMS	P 740
SUMI=SUMI+WORK4	P 750
90 CONTINUE	P 760
C WORK5=(4.0*SUMI)/(NS*BC*WC)	P 770
ANS2=1.0*WORK5	P 780
ANS2DB=10.0*ALOG10(ABS(ANS2))	P 790
C	P 800
SPL=HVV(I)+ANS1DB+ANS3DB(I)+ANS2DB	P 810
SPLC(I)=SPL	P 820
HXX=HVX(I)	P 830
HYY=HVV(I)	P 840
CYY=CVY(I)	P 850
A3=ANS3DB(I)	P 860
A2=ANS2DB	P 870
GO TO 130	P 880
C	P 890
C	P 900
C	P 910
FAILURE CODE STATEMENTS (PACKAGE C)	P 920
100 HYY=0.0	P 930
HXX=HVX(I)	P 940
CYY=0.0	P 950
A3=0.0	P 960
A2=0.0	P 970
SPLC(I)=2.0	P 980
GO TO 130	P 990
C	P1000
110 HXX=0.0	P1010
HYY=0.0	P1020
CYY=0.0	P1030
A3=0.0	P1040
A2=0.0	P1050
SPLC(I)=1.0	P1060
GO TO 130	P1070
C	P1080
120 HXX=0.0	P1090
HYY=0.0	P1100
CYY=0.0	P1110
A3=0.0	P1120
A2=0.0	P1130
SPLC(I)=3.0	P1140
GO TO 130	P1150
130 RETURN	P1160
END	P1170-

•DECK LAGRNG	
SUBROUTINE LAGRNG (X,Y,N,VALX,VALY)	Q 10
C	Q 20
C THIS SUBROUTINE CONDUCTS LAGRANGIAN INTERPOLATION*****	Q 30
C	Q 40
C X=X-COORDINATES OF H0 OR C1 MASTER INPUT SPECTRUM	Q 50
C Y=Y-COORDINATES OF H0 OR C1 MASTER INPUT SPECTRUM	Q 60
C N=NUMBER OF POINTS DESCRIBING H0 OR C1 MASTER INPUT SPECTRUM	Q 70
C VALX=ARGUMENT SIGMA	Q 80
C VALY=INTERPOLATED VALUE OF H0 OR C1 AT ARGUMENT SIGMA	Q 90
C	Q 100
DIMENSION X(20),Y(20)	Q 110
C	Q 120
N1=N-1	Q 130
DO 10 I=2,N1	Q 140
IF (VALX.LE.X(I)) GO TO 20	Q 150
10 CONTINUE	Q 160
I=N1	Q 170
20 IS1=I-1	Q 180
IS2=I+1	Q 190
VALY=0.0	Q 200
DO 40 I=IS1,IS2	Q 210
P=1.0	Q 220
DO 30 J=IS1,IS2	Q 230
IF (I.EQ.J) GO TO 30	Q 240
A=(VALX-X(J))/(X(I)-X(J))	Q 250
P=P*A	Q 260
30 CONTINUE	Q 270
B=P*Y(I)	Q 280
VALY=VALY+B	Q 290
40 CONTINUE	Q 300
RETURN	Q 310
END	Q 320-

•DECK	BLKSAN	
	BLOCK DATA SAN	R 10
C		R 20
C	INPUT DATA*****	R 30
C		R 40
C	HX=ARGUMENT SIGMA IN SOURCE STRENGTH SPECTRUM	R 50
C	HY=SOURCE STRENGTH H0(SIGMA) FOR ARGUMENT SIGMA	R 60
C	CX=ARGUMENT SIGMA IN CORRELATION COEFFICIENT SPECTRUM	R 70
C	CY=CORRELATION COEFFICIENT C1(SIGMA) FOR ARGUMENT SIGMA	R 80
C		R 90
	COMMON/THIRTY/HX(20)	R 100
	COMMON/FORTY/HY(20)	R 110
	COMMON/FIFTY/CX(20)	R 120
	COMMON/SIXTY/CY(20)	R 130
C		R 140
	DATA HX/ 0.2,0.3,0.4,0.7,1.0,1.5,2.0,3.0,3.5,4.0,4.5,5.0,6.0,7.0,	R 150
	1 8.0,10.0,20.0,40.0,68.0,70.0 /	R 160
C		R 170
	DATA HY/ 116.0,121.6,125.5,132.5,137.7,142.7,145.7,148.5,149.1,	R 180
	1 149.2,149.1,148.8,147.4,146.7,145.7,143.7,137.4,130.5,125.4,	R 190
	2 125.2 /	R 200
C		R 210
	DATA CX/ 0.2,0.3,0.4,0.7,1.0,1.5,2.0,3.0,3.5,4.0,4.5,5.0,6.0,7.0,	R 220
	1 8.0,10.0,20.0,40.0,68.0,70.0 /	R 230
C		R 240
	DATA CY/ 0.70,0.71,0.71,0.72,0.73,0.74,0.74,0.71,0.69,0.67,0.64,	R 250
	1 0.62,0.58,0.54,0.50,0.45,0.28,0.12,0.02,0.02 /	R 260
C		R 270
	END	R 280-

*DECK INTEG		
PROGRAM INTEG(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT)		S 10
EXTERNAL FCT,FCD,FQA6		S 20
REAL I1,I2,K		S 30
REAL MJ		S 40
DIMENSION W(24),FREQ(24),WI1(24),WI2(24),XU(24),XX(21),ENT1(21),		S 50
1 ENT2(21),DBU(24),OBD(24),DB(24)		S 60
2 ,SN(24),SPLM(24),IL(3)		S 70
COMMON/CON/ A0,VJ,XC,K,A1,B1,C1,A2,B2,C2,D2,A3,B3,RJ,WP,		S 80
1 A4,A5,XLIMIT,INTFLG		S 90
PI=3.141593		S 100
C		S 110
C READ INPUT CONSTANTS		S 120
C		S 130
READ (5,140) RUNNO		S 140*
READ (5,170) (FREQ(I),I=1,24)		S 150*
10 READ (5,140) TP		S 160*
IF (TP.LT.1.0) GO TO 130		S 170
READ (5,180) (SPLM(I),I=1,24)		S 180*
READ (5,160) IOUT		S 190*
READ (5,160) INTFLG		S 200*
READ (5,140) MJ		S 210*
READ (5,140) VJF		S 220*
READ (5,140) XC		S 230*
READ (5,140) T0F		S 240*
READ (5,150) K		S 250*
READ (5,140) A1		S 260*
READ (5,140) B1		S 270*
READ (5,140) C1		S 280*
READ (5,150) A2		S 290*
READ (5,150) B2		S 300*
READ (5,140) C2		S 310*
READ (5,150) D2		S 320*
READ (5,150) A3		S 330*
READ (5,150) B3		S 340*
READ (5,150) A4		S 350*
READ (5,150) A5		S 360*
READ (5,150) XLIMIT		S 370*
READ (5,140) RJ		S 380*
READ (5,140) R		S 390*
READ (5,150) PAMB		S 400*
C		S 410
A0F=49.02*SQRT(T0F+459.67)		S 420
PAMB=PAMB*6894.7572		S 430
VJ=VJF*12.0		S 440
AJ=VJ/MJ		S 450
A0=A0F*12.0		S 460
XC=XC*2.0*RJ*(4.3+1.1*MJ*MJ)		S 470
VJA0=VJ/A0		S 480
TJT0=(AJ/A0)**2		S 490
THETA=90.0		S 500
C		S 510
K=K/(0.63*AJ*2.0*MJ*(1.1+0.9*MJ))		S 520
C BEGIN FREQUENCY LOOP		S 530
C		S 540
XLOWER=0.0		S 550
XUPER2=1.0/XC		S 560
TURB=0.6667*0.179*MJ*(-.1028)		S 570
CONST=20.0*ALOG10(1.4*PAMB/2.0E-5)-20.0*ALOG10(R)+10.0*ALOG10(0.23)		S 580

116)	40.0*ALOG10(VJ/A0*TURB/A0)-10.0*ALOG10(64.0*PI*SQR(PI))+10.0*	S 590
2	ALOG10(2.0)	S 600
DO 80	I=1,24	S 610
W(I)	=2.0*PI*FREQ(I)	S 620
SN(I)	=FREQ(I)*2.0*RJ/VJ	S 630
WP	=W(I)	S 640
XMAX	=5.99402199/(FREQ(I)*K)	S 650
IF (INTFLG.EQ.1)	GO TO 20	S 660
IF (XC.LT.XMAX)	GO TO 20	S 670
XUPPER	=XMAX	S 680
CALL QA6	(FQA6,I1)	S 690S
GO TO 30		S 700
20	XUPPER=XC	S 710
CALL DQG32	(XLOWER,XUPPER,FCT,I1)	S 720S
30	XU(I)=XUPPER	S 730
W1(I)	=I1*W(I)**5*(1.0/SQR(C1))	S 740
W1(I)	=W1(I)*SQR(PI)/2.0	S 750
IF (W1(I).GT.0.0)	GO TO 40	S 760
DBU(I)	=0.0	S 770
GO TO 50		S 780
40	DBU(I)=10.0*ALOG10(W1(I))	S 790
50	CALL DQG32 (XLOWER,XUPER2,FCD,I2)	S 800S
W12(I)	=I2*W(I)**5/(2.0*C2)	S 810
W12(I)	=W12(I)/4.0	S 820
IF (W12(I).GT.0.0)	GO TO 60	S 830
DBD(I)	=0.0	S 840
GO TO 70		S 850
60	DBD(I)=10.0*ALOG10(W12(I))	S 860
70	DB(I)=10.0*ALOG10(10.0**((DBU(I)/10.0)+10.0**((DBD(I)/10.0)))	S 870
DBU(I)	=DBU(I)+CONST	S 880
DBD(I)	=DBD(I)+CONST	S 890
DB(I)	=DB(I)+CONST	S 900
80	CONTINUE	S 910
WRITE (6,190)	INTFLG,MJ,T0F,A0,VJF,XC,RJ,A1,A2,B1,B2,C1,C2,K,D2,A3	S 920*
1,B3,A4,A5,R,PAMB,XLIMIT		S 930
DO 90	I=1,24	S 940
WRITE (6,200)	FREQ(I),SN(I),DBU(I),DBD(I),DB(I)	S 950*
90	CONTINUE	S 960
IF (IOUT.EQ.0)	GO TO 120	S 970
WRITE (6,210)		S 980*
ENT2(I)	=0.0	S 990
DO 110	I=1,24	S1000
WP	=W(I)	S1010
WRITE (6,220)	FREQ(I),W(I)	S1020*
DO 100	J=1,21	S1030
XX(J)	=FLOAT(J-1)	S1040
ENT1(J)	=FCT(XX(J))*W(I)**5*(1.0/SQR(C1))	S1050
IF (J.EQ.1)	GO TO 100	S1060
ENT2(J)	=FCD(1.0/XX(J))*W(I)**5/(2.0*C2)/XX(J)**2	S1070
100	CONTINUE	S1080
WRITE (6,230)	XX(1),ENT1(1)	S1090*
WRITE (6,230)	(XX(J),ENT1(J),ENT2(J),J=2,21)	S1100*
110	CONTINUE	S1110
120	CONTINUE	S1120
C		S1130
C	RETURN FOR NEXT COMPUTATION	S1140
C		S1150
C	GO TO 10	S1160
C		S1170

130 STOP	S1180
C	S1190
C	S1200
C	S1210
C	S1220
140 FORMAT (F15.1)	S1230
150 FORMAT (E10.4)	S1240
160 FORMAT (I1)	S1250
170 FORMAT (8F10.1)	S1260
180 FORMAT (12F6.1)	S1270
190 FORMAT (1H1,T8,"INPUT PARAMETERS FOR INTEGRATION ARE -",//,T2,"INT	S1280
1FLG = ",I2,/,T5,"MJ = ",E15.8,T40,"T0 = ",E15.8,/,T5,"A0 = ",E15.	S1290
28,T40,"VJ = ",E15.8,/,T5,"XC = ",E15.8,T40,"RJ = ",E15.8,/,T5,"A	S1300
31 = ",E15.8,T40,"A2 = ",E15.8,/,T5,"B1 = ",E15.8,T40,"B2 = ",E15.	S1310
48,/,T5,"C1 = ",E15.8,T40,"C2 = ",E15.8,/,T5," K = ",E15.8,T40,"D	S1320
52 = ",E15.8,/,T5,"A3 = ",E15.8,T40,"B3 = ",E15.8,/,T5,"A4 = ",E1	S1330
65.8,T40,"A5 = ",E15.8,/,T5," R = ",E15.8,T40,"P0 = ",E15.8,/,T5,	S1340
7"XLIMIT = ",F6.2,/,/,T2,"FREQUENCY",T18,"SN",T29,"DBU",T40,"DBD",	S1350
BT51,"DB",/)	S1360
200 FORMAT (T3,F8.2,T15,F7.3,3(4X,F7.2))	S1370
210 FORMAT (1H1,T24,"VALUES OF INTEGRAND FOR VARIOUS VALUES OF X",/)	S1380
220 FORMAT (/5X,"FREQUENCY = ",F8.2,5X,"OMEGA = ",E15.7,/,T15,"X",T2	S1390
18,"INTEGRAND 1",T48,"INTEGRAND 2",/)	S1400
230 FORMAT (11X,F10.6,5X,E15.7,5X,E15.7)	S1410
END	S1420-

*DECK FCT	
FUNCTION FCT(X)	T 10
REAL L1,LT,K	T 20
COMMON/CON/ A0,VJ,XC,K,A1,B1,C1,A2,B2,C2,D2,A3,B3,RJ,WP,	T 30
1 A4,A5,XLIMIT,INTFLG	T 40
DATA PI,RTP / 3.141593,0.797885 /	T 50
R12=RJ	T 60
IF (X.LE.XLIMIT) GO TO 10	T 70
L1=A1*X+B1	T 80
LT=A3*X+B3	T 90
GO TO 20	T 100
10 L1=A4*X	T 110
LT=A5*X	T 120
20 CONTINUE	T 130
D1=1.0	T 140
T0=K*X**D1	T 150
IF (INTFLG.EQ.1) GO TO 50	T 160
PART1=R12*X*L1*LT**2*T0	T 170
PART=- (WP*T0) / 8.0	T 180
IF (PART.LT.147.5.AND.PART.GT.-146.5) GO TO 30	T 190
PART2=0.0	T 200
GO TO 40	T 210
30 PART2=EXP(PART)	T 220
40 FCT=PART1*PART2*EXP(-.0016*X*X)	T 230
RETURN	T 240
50 PART1=R12*X*L1*LT**2*T0	T 250
PART=- (L1*WP)**2/(8.0*PI*0.63*0.63*VJ*VJ)	T 260
IF (PART.LT.147.5.AND.PART.GT.-146.5) GO TO 60	T 270
PART2=0.0	T 280
GO TO 70	T 290
60 PART2=EXP(PART)	T 300
70 PART3=RTP*PI/4.0/(1.0+(WP*T0)**2/4.0)**1.5	T 310
FCT=PART1*PART2*PART3*EXP(-.0016*X*X)	T 320
RETURN	T 330
END	T 340-

•DECK QG10

SUBROUTINE QG10 (XL,XU,FCT,Y)

A=0.5*(XU+XL)

B=XU-XL

C=0.4869533*B

Y=0.03333567*(FCT(A+C)+FCT(A-C))

C=0.4325317*B

Y=Y+0.07472567*(FCT(A+C)+FCT(A-C))

C=0.3397048*B

Y=Y+0.1095432*(FCT(A+C)+FCT(A-C))

C=0.2166977*B

Y=Y+0.1346334*(FCT(A+C)+FCT(A-C))

C=0.07443717*B

Y=B*(Y+0.1477621*(FCT(A+C)+FCT(A-C)))

RETURN

END

U 10
U 20
U 30
U 40
U 50
U 60
U 70
U 80
U 90
U 100
U 110
U 120
U 130
U 140
U 150-

•DECK FQA6

FUNCTION FQA6(XP)	V 10
REAL L1,LT,K	V 20
COMMON/CON/ A0,VJ,XC,K,A1,B1,C1,A2,B2,C2,D2,A3,B3,RJ,WP,	V 30
1 A4,A5,XLIMIT,INTFLG	V 40
X=SQRT(8.0*XP/(WP**2*K**2))	V 50
R12=RJ	V 60
IF (X.LE.XLIMIT) GO TO 10	V 70
L1=A1*X*B1	V 80
LT=A3*X*B3	V 90
GO TO 20	V 100
10 L1=A4*X	V 110
LT=A5*X	V 120
20 CONTINUE	V 130
T0=K*X	V 140
PART1=SQRT(XP)*R12*L1*LT*LT*T0	V 150
PART2=(WP**2*K**2)/4.0	V 160
FQA6=PART1/PART2*EXP(-.0016*X*X)	V 170
RETURN	V 180
END	V 190-

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*DECK QA6
SUBROUTINE QA6 (FCT,Y)
X=15.12996
Y=.5317103E-6*FCT(X)
X=9.124248
Y=Y+.0001714737*FCT(X)
X=5.196153
Y=Y+.007810781*FCT(X)
X=2.552590
Y=Y+.1032160*FCT(X)
X=.8983028
Y=Y+.5209846*FCT(X)
X=.09874701
Y=Y+1.140270*FCT(X)
RETURN
END

```

```

W 10
W 20
W 30
W 40
W 50
W 60
W 70
W 80
W 90
W 100
W 110
W 120
W 130
W 140
W 150-

```

*DECK FCD

FUNCTION FCD(X)	X 10
REAL L2,LT,K	X 20
COMMON/CON/ A0,VJ,XC,K,A1,B1,C1,A2,B2,C2,D2,A3,B3,RJ,WP,	X 30
1 A4,A5,XLIMIT,INTFLG	X 40
DATA PI,RTP / 3.141593,0.797885 /	X 50
L2=(A2/X+B2)**D2	X 60
LT=(A3/X+B3)**D2	X 70
T0=K/X	X 80
IF (INTFLG.EQ.1) GO TO 30	X 90
PART1=L2*LT*LT*XC**4*EXP(-.0016*XC*XC)*T0	X 100
PART=- (WP*T0)**2/8.0	X 110
IF (PART.LT.147.5.AND.PART.GT.-146.5) GO TO 10	X 120
PART2=0.0	X 130
GO TO 20	X 140
10 PART2=EXP(PART)	X 150
20 FCD=PART1*PART2	X 160
RETURN	X 170
30 PART1=L2*LT**2*XC**4*EXP(-.0016*XC*XC)*T0	X 180
VC=0.63*VJ	X 190
PART=- (L2*WP)**2/(8.0*PI*VC*VC)	X 200
IF (PART.LT.147.5.AND.PART.GT.-146.5) GO TO 40	X 210
PART2=0.0	X 220
GO TO 50	X 230
40 PART2=EXP(PART)	X 240
50 PART3=RTP*PI/4.0/(1.0+(WP*T0)**2/4.0)**1.5	X 250
FCD=PART1*PART2*PART3	X 260
RETURN	X 270
END	X 280-

*DECK DQG32	
SUBROUTINE DQG32 (XL,XU,FCT,Y)	Y 10
A=.5*(XU+XL)	Y 20
B=XU-XL	Y 30
C=.49863193092474078*B	Y 40
Y=.003509305004735048*(FCT(A+C)+FCT(A-C))	Y 50
C=.4928057557726341*B	Y 60
Y=Y+.008137197365452835*(FCT(A+C)+FCT(A-C))	Y 70
C=.48238112779375322*B	Y 80
Y=Y+.012696032654631030*(FCT(A+C)+FCT(A-C))	Y 90
C=.46745303796886984*B	Y 100
Y=Y+.017136931456510717*(FCT(A+C)+FCT(A-C))	Y 110
C=.44816057788302606*B	Y 120
Y=Y+.021417949011113340*(FCT(A+C)+FCT(A-C))	Y 130
C=.42468380686628499*B	Y 140
Y=Y+.025499029631188088*(FCT(A+C)+FCT(A-C))	Y 150
C=.39724189798397120*B	Y 160
Y=Y+.029342046739267774*(FCT(A+C)+FCT(A-C))	Y 170
C=.36609105937014484*B	Y 180
Y=Y+.032911111388180923*(FCT(A+C)+FCT(A-C))	Y 190
C=.33152213346510760*B	Y 200
Y=Y+.036172897054424253*(FCT(A+C)+FCT(A-C))	Y 210
C=.29385787862038116*B	Y 220
Y=Y+.039096947893535153*(FCT(A+C)+FCT(A-C))	Y 230
C=.25344995446611470*B	Y 240
Y=Y+.041655962113473378*(FCT(A+C)+FCT(A-C))	Y 250
C=.21067563806531767*B	Y 260
Y=Y+.043826046502201906*(FCT(A+C)+FCT(A-C))	Y 270
C=.16593430114106382*B	Y 280
Y=Y+.045586939347881942*(FCT(A+C)+FCT(A-C))	Y 290
C=.11964368112606854*B	Y 300
Y=Y+.046922199540402283*(FCT(A+C)+FCT(A-C))	Y 310
C=.07223598079139825*B	Y 320
Y=Y+.047819360039637430*(FCT(A+C)+FCT(A-C))	Y 330
C=.024153832843869158*B	Y 340
Y=B*(Y+.048270044257363900*(FCT(A+C)+FCT(A-C)))	Y 350
RETURN	Y 360
END	Y 370-